

Hardware and Operating Condition Impacts on SPI

SOUTHWEST RESEARCH INSTITUTE®

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POWERTRAIN ENGINEERING

Preamble

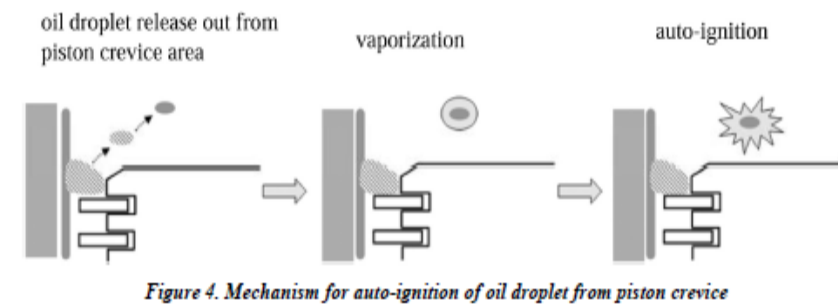
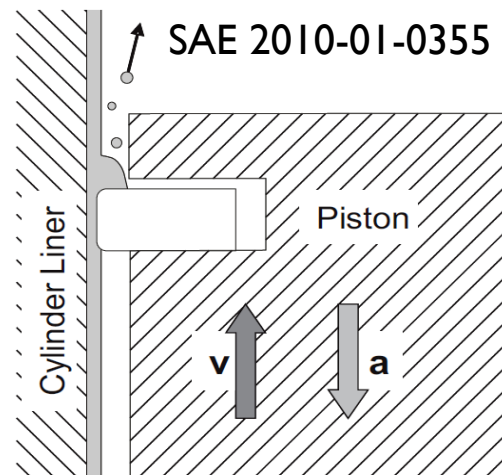
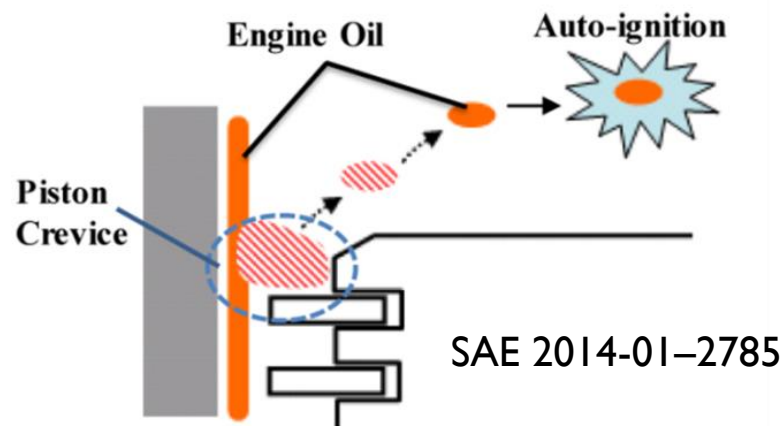
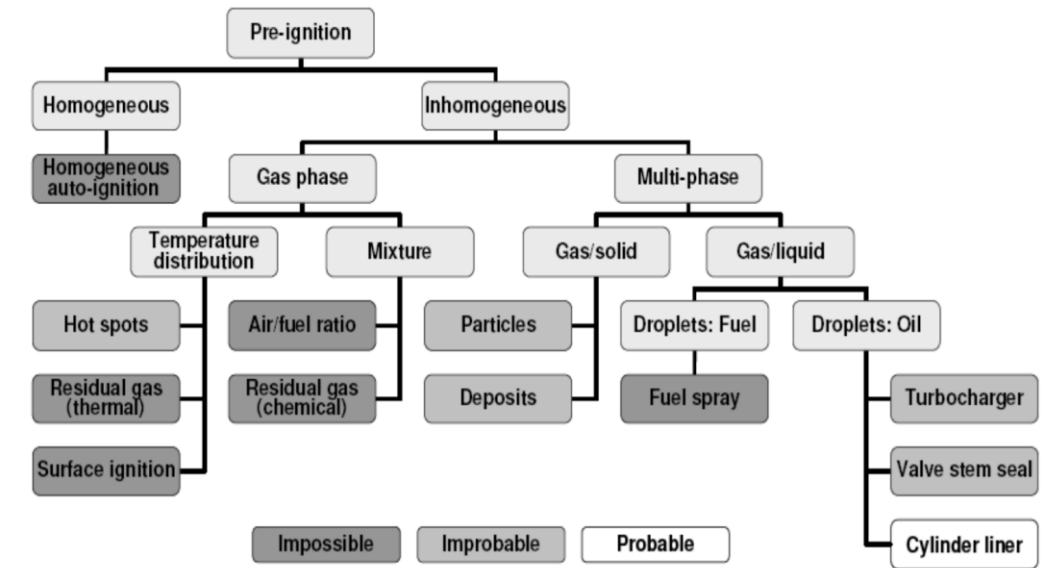
- This presentation will attempt to cover “everything else” related to the frequency of (L)SPI with *all else being equal*
 - May still not be exhaustive and omissions were not intentional
 - There may be contradictory observations, but a general view is presented
- It is a collection of observations from literature and the various authors are fully acknowledged
 - Additional sources are SwRI Internal Research and P3 Consortium
- Much of our understanding of LSPI is based on steady-state testing
 - Please accept *for now* that it is a reasonable representation of real-world behavior

Contents

- Overview of hypothesis
- Factors contributing to LSPI
 - Operating conditions
 - User demands
 - Calibration
 - Transients
 - Hardware
 - Design
 - Engine condition
- Conclusion
- Recommendations

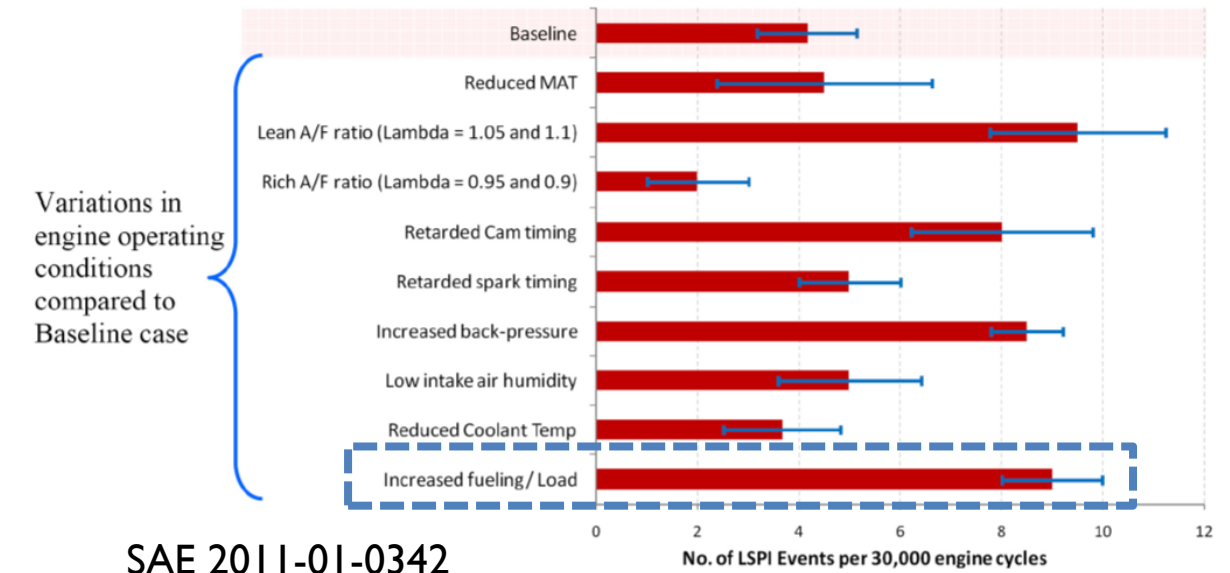
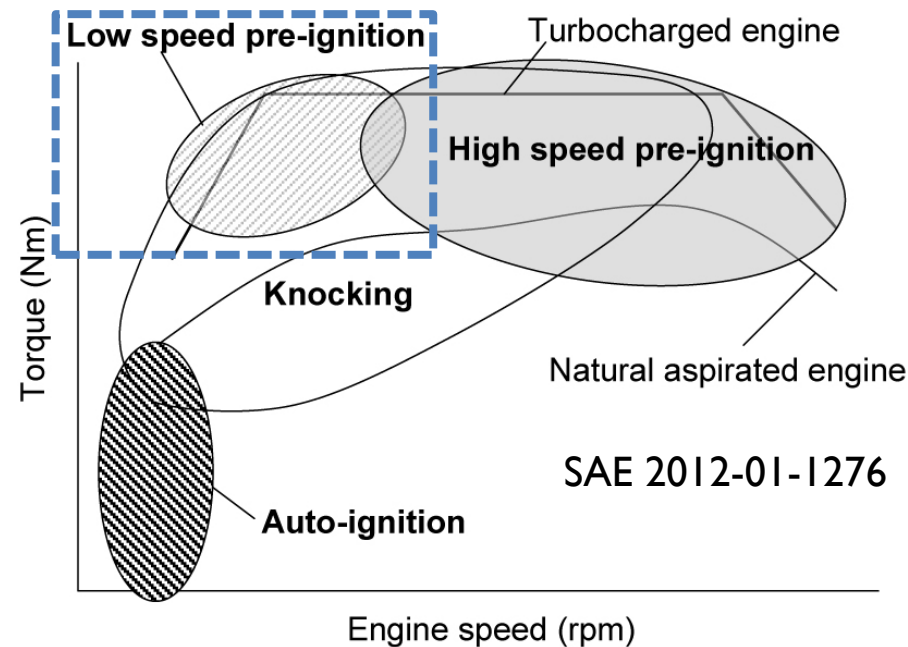
Working Hypothesis

- There are numerous publications that point to the crevice fluid as a likely cause of LSPI
 - Mixture of fuel and oil in right proportion
- Combustion related soot and/or particulates appear to have a contributing/complementary impact, as do engine deposits



Speed / Load Demands

- LSPI encountered in low speed, high load parts of the engine map
 - Typical of forced induction, direct injection spark ignition engines with retarded spark



SAE 2012-01-1141	Low	Frequency of SuperKnock	High
Intake air Pressure	Low	□ □ →	High
Lambda	Rich	□ □ →	Lean
Intake air Temperature	No Influence (26~42degC)		
Ignition Timing	Retard	□ □ →	Advance
Injection Timing	Advance	□ □ →	Retard
Intake Open Timing	Retard	□ □ →	Advance
Blow-by Oil	Little	□ □ →	Much

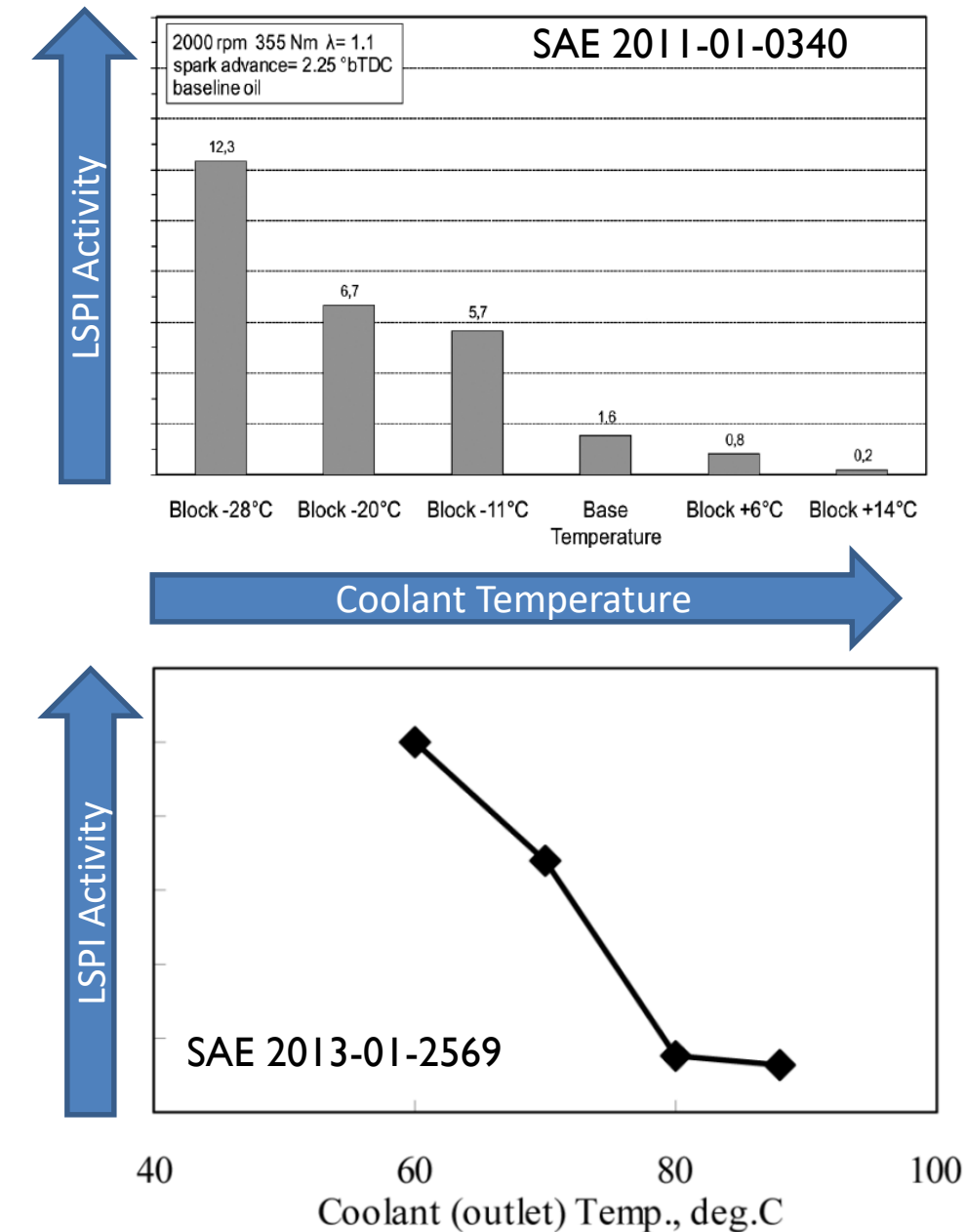
Calibration - Engine Coolant Temperature

- Multiple papers have shown that LSPI increases with lower coolant temperatures
 - This is engine / design specific
 - Correlation between wall temperatures and fuel evaporation (EXX) that corresponds to LSPI frequency

Coolant temp.	◎
Inj. start timing	◎
Fuel pressure	○
Ig. timing	×
A/F (Exhaust)	×
Blow-by gas	△
Deposit	○
Top ring gap location	◎
Low oil cetane number (and w/o Ca)	◎
Oil w/ & w/o Ca	◎

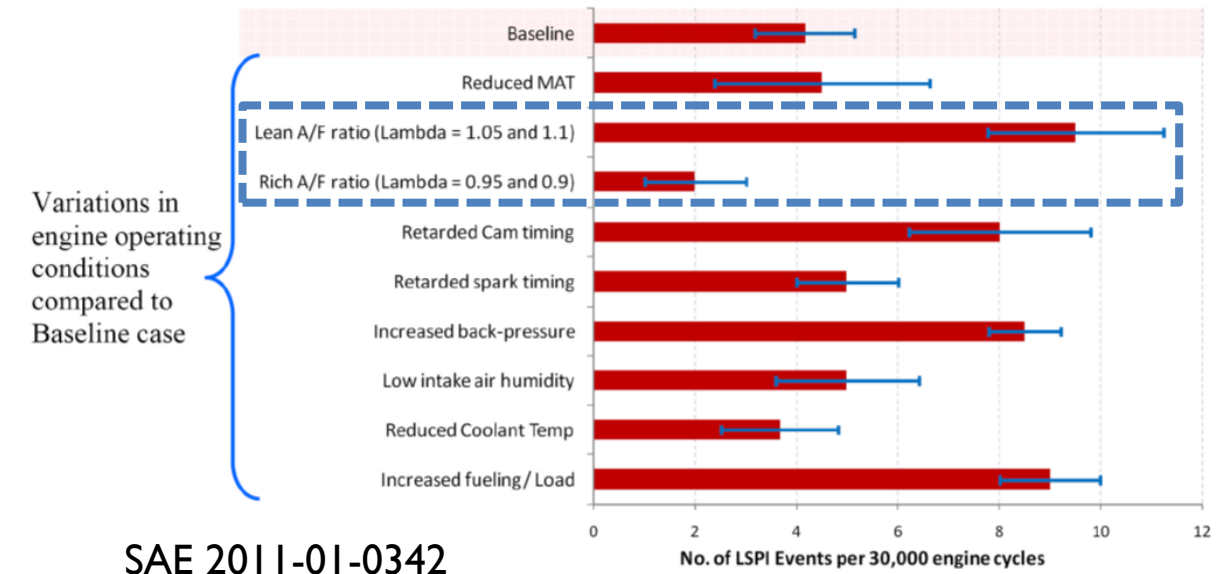
◎: Strong effect
 ○: effect
 △: weak effect
 ×: no effect

SAE 2015-01-0756



Calibration - Air-Fuel Ratio

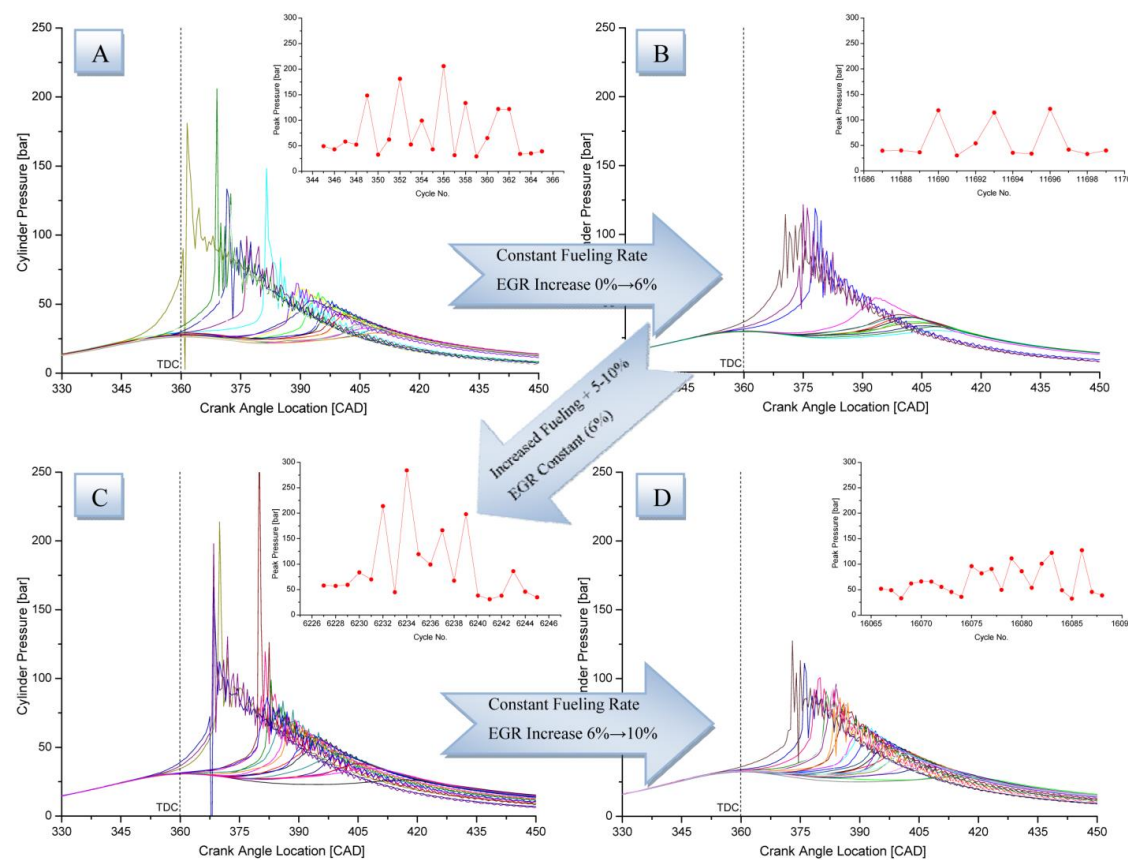
- Lean mixtures generally increase LSPI
 - Either by direct fueling action or indirectly by engine breathing
 - Mechanism is not clear
- This response can be used both to accelerate LSPI during research and testing but also to mitigate in LSPI in real-life calibration



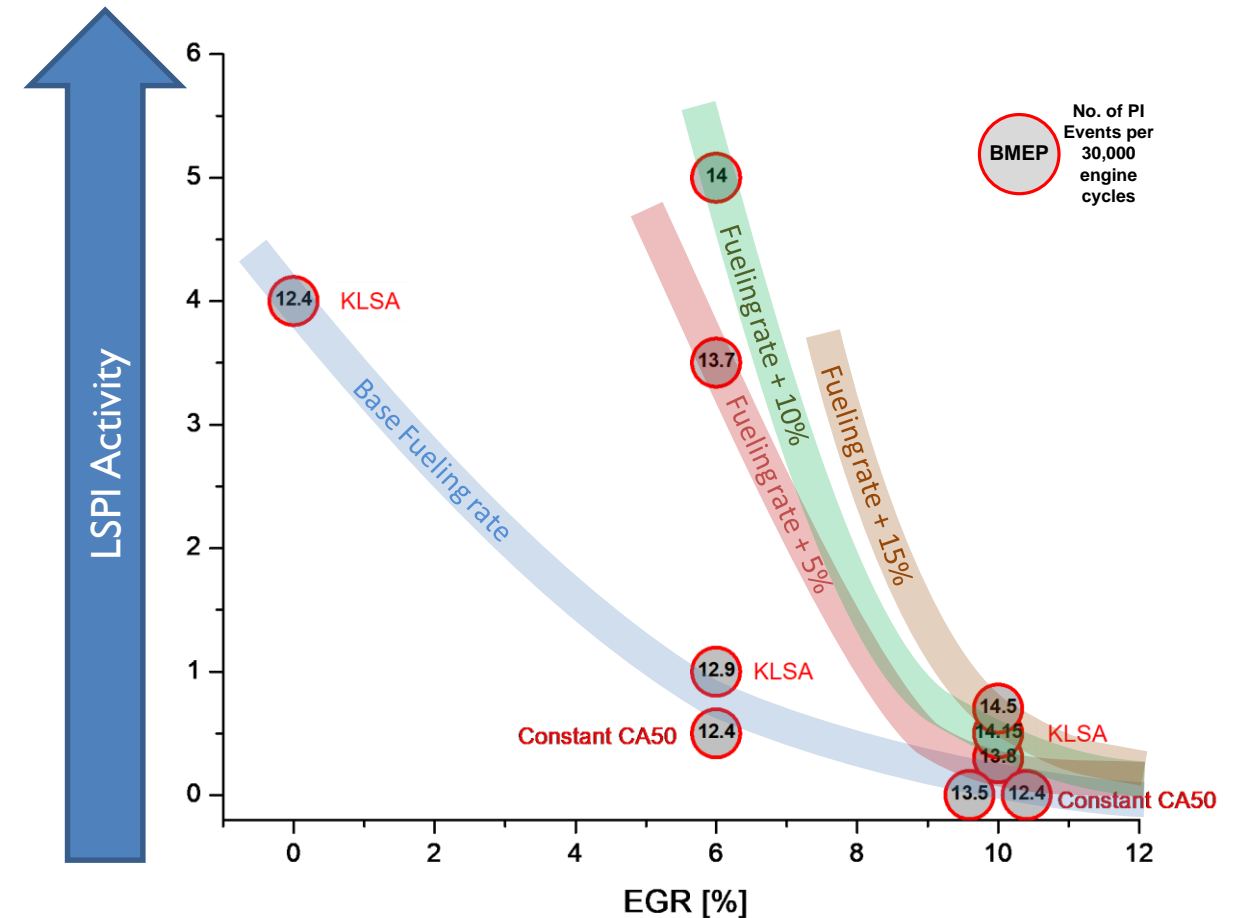
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Blow-by Oil	Little	□ □ □ →	Much

Calibration - EGR

- LSPI frequency is reduced with increasing levels of EGR
 - EGR levels may not be production feasible



SAE 2011-01-0339



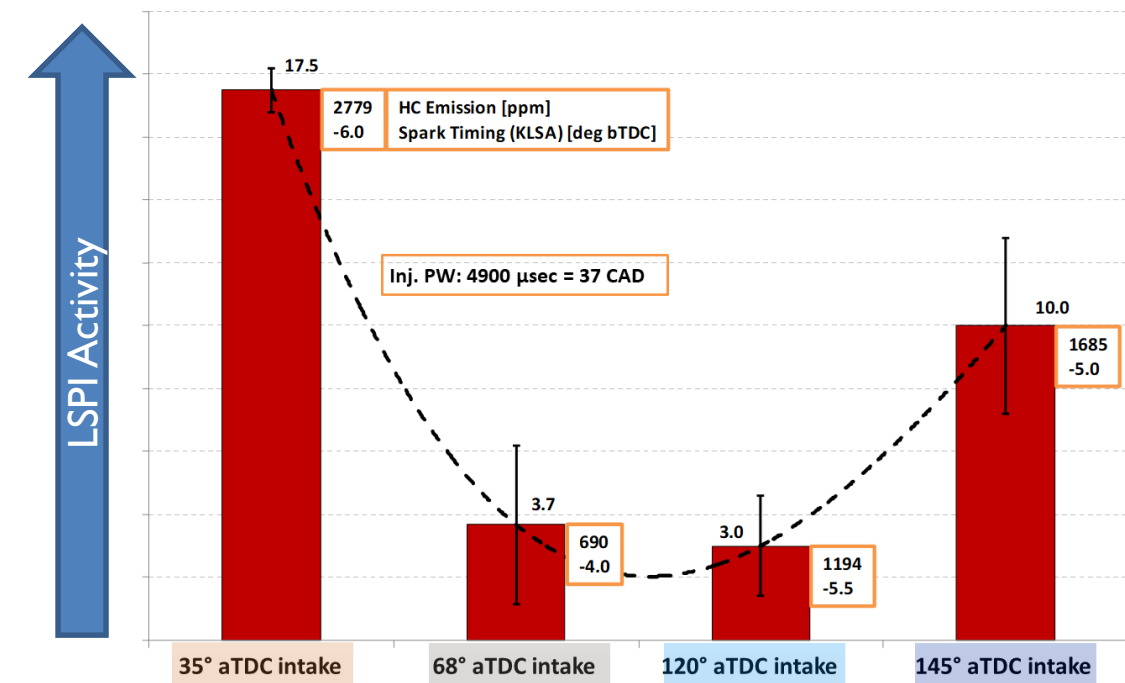
Calibration - Injection Timing and Pressure

- LSPI is affected by fuel injection timing due to wall impingement and mixing
 - Production calibration also needs to consider durability, emissions, NVH and performance
- Similar impact of injection pressure
 - Trade-off between atomization and penetration depth

Coolant temp.	◎
Inj. start timing	◎
Fuel pressure	○
Ig. timing	×
A/F (Exhaust)	×
Blow-by gas	△
Deposit	○
Top ring gap location	◎
Low oil cetane number (and w/o Ca)	◎
Oil w/ & w/o Ca	◎

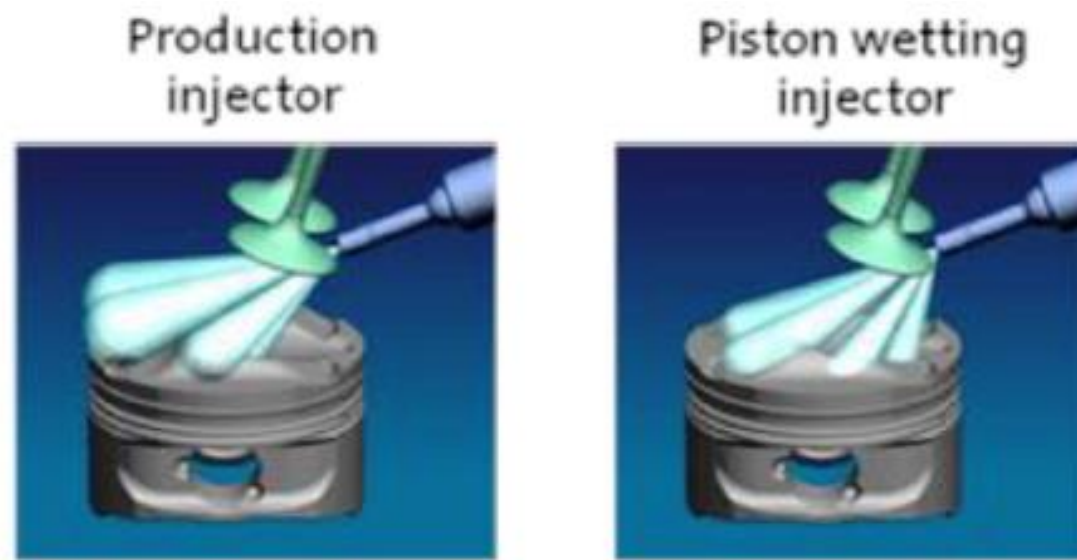
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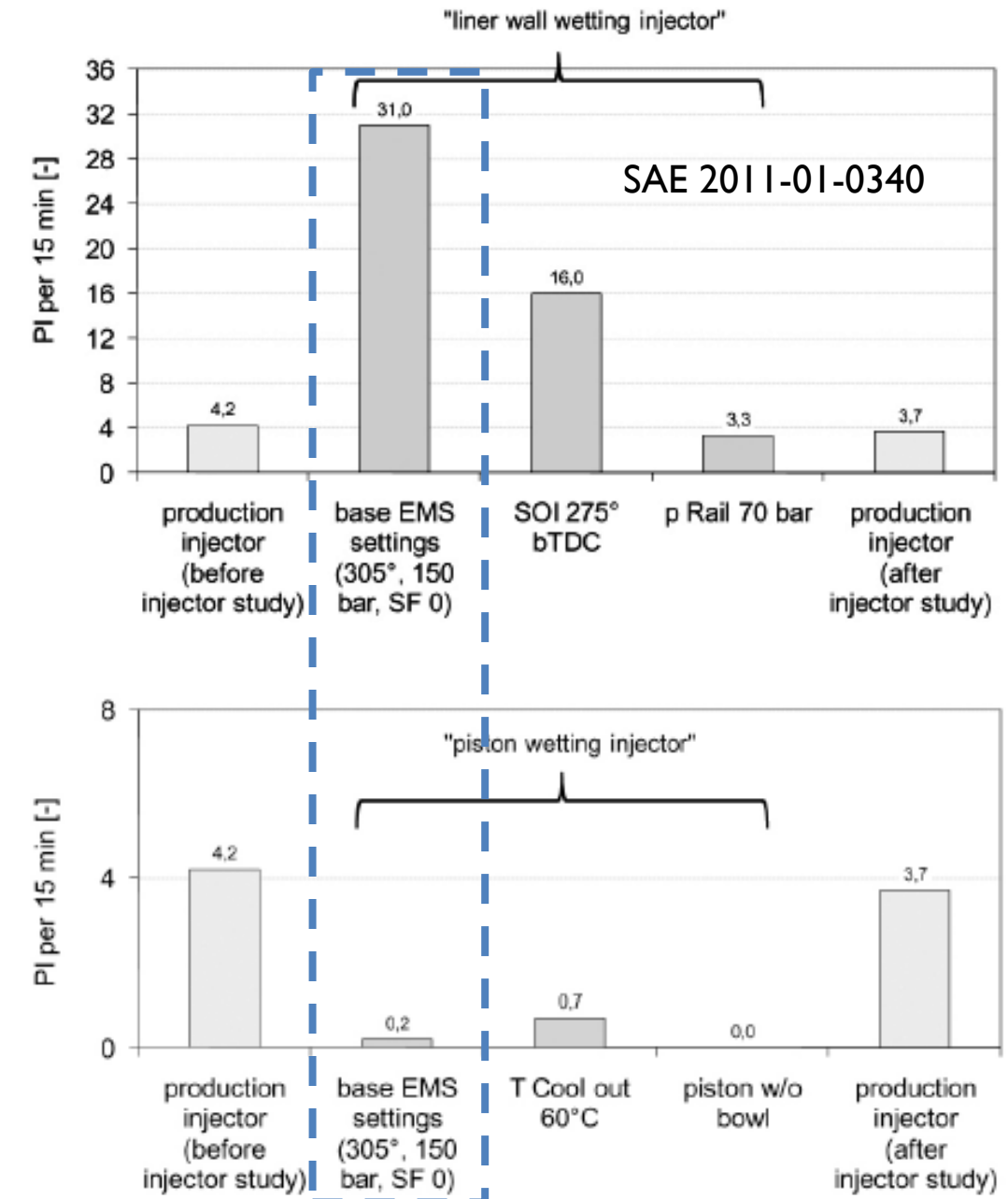


Design - Injection Targeting

- Changing injector targeting to place liquid fuel on piston not liner decreased LSPI
 - Consistent with lowest hydrocarbon emissions at minimum LSPI

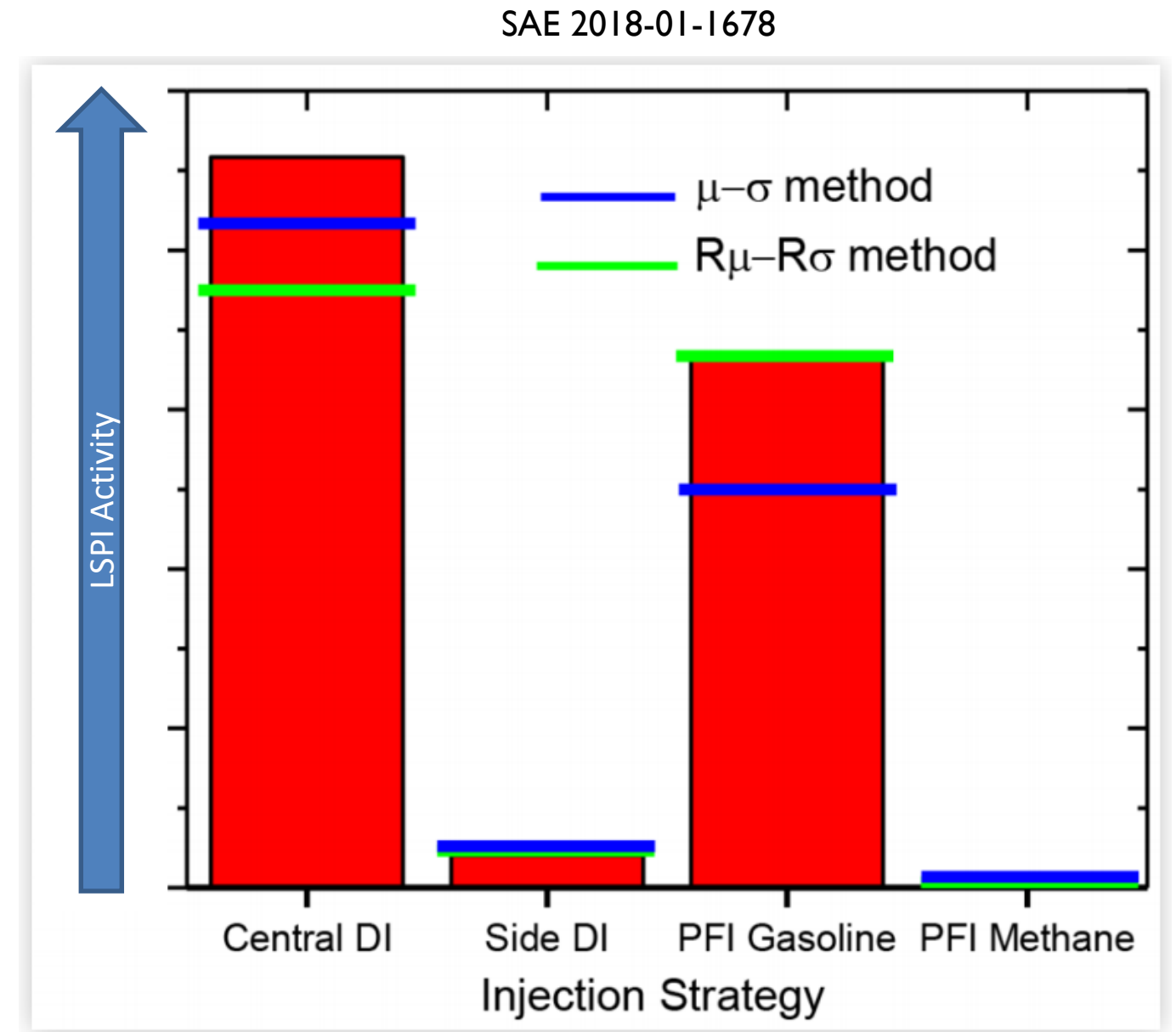


Piston Pos. 30mm below TDC



Design – Injector Location

- Central DI and PFI generally worsens LSPI compared to side DI
 - Attributed to increased wall wetting
- Results are confounded by piston design and injection pressure that are matched to injector type and location



Design - Piston Chamfer

- Chamfered piston crown decreases LSPI frequency
 - Likely leads to reduced crevice fluid accumulation and impacts composition
- Design may not be production appropriate due to emissions, costs or robustness

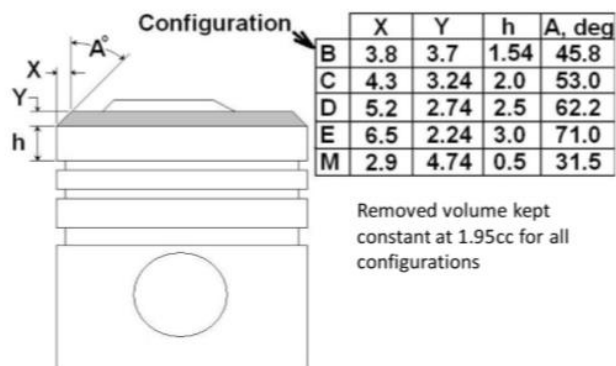
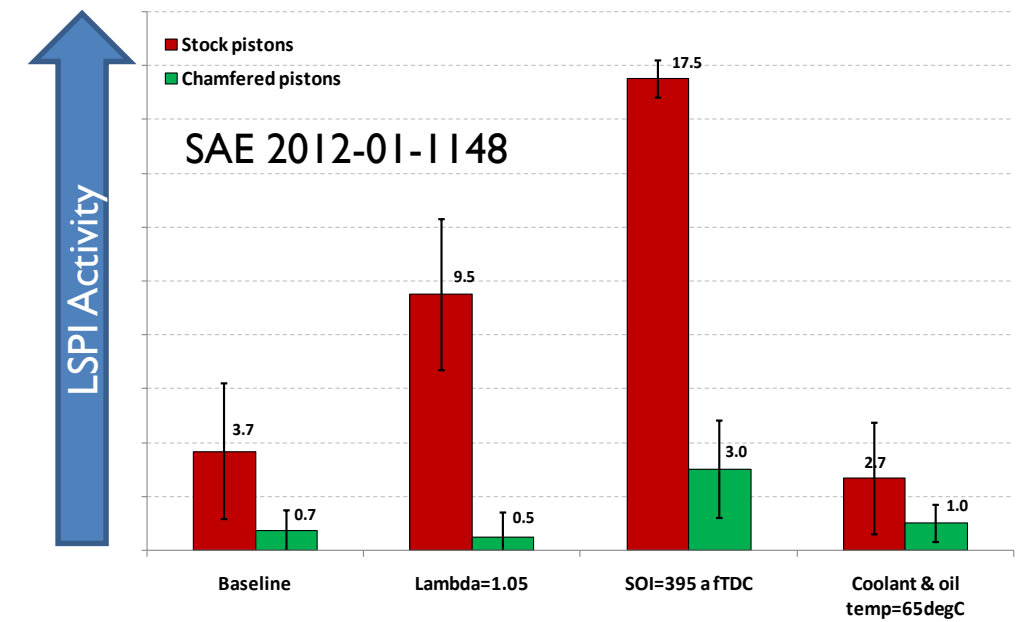


Figure 14. Chamfered Piston Crown - Second Iteration



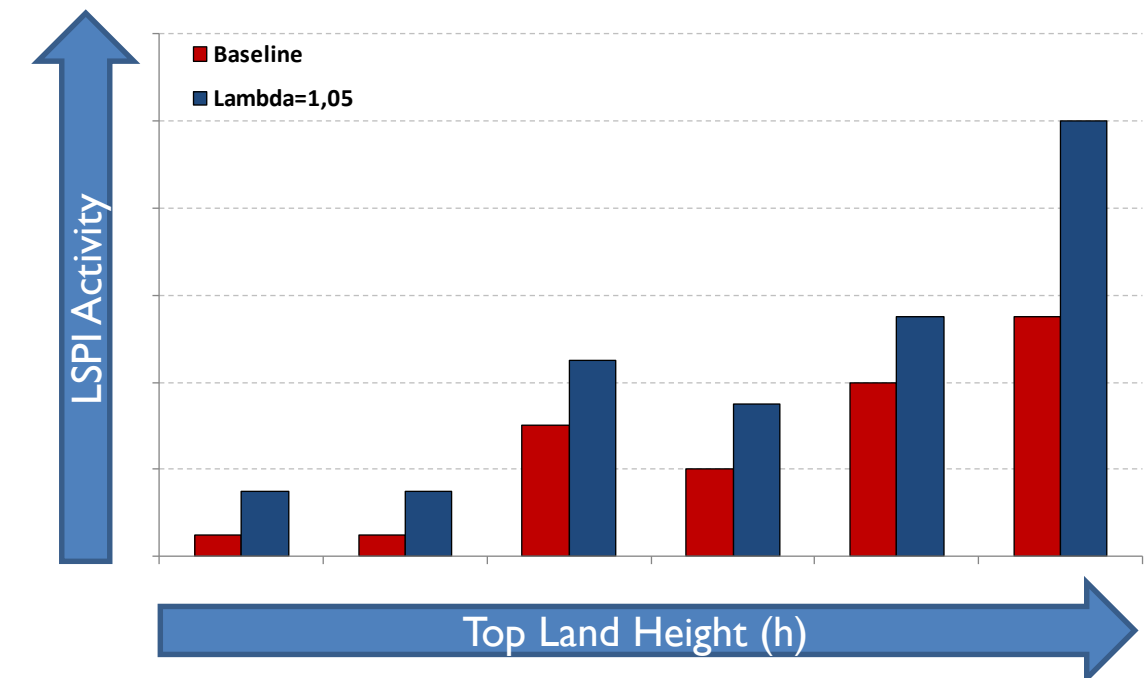
Design – Top Land Height

- Strong correlation between piston top land height and LSPI frequency
 - Reduces crevice volume
- May not be production feasible due to strength and robustness considerations

Coolant temp.	◎
Inj. start timing	◎
Fuel pressure	○
Ig. timing	×
A/F (Exhaust)	×
Blow-by gas	△
Deposit	○
Top ring gap location	◎
Low oil cetane number (and w/o Ca)	◎
Oil w/ & w/o Ca	◎

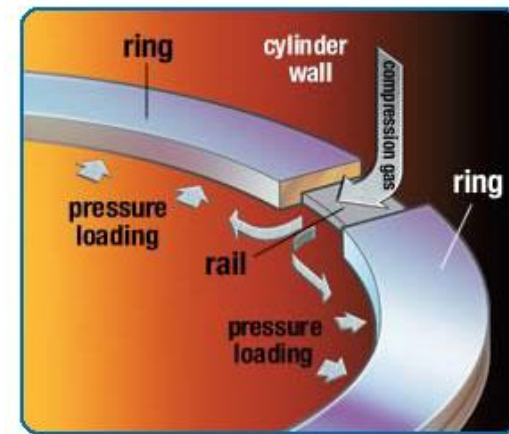
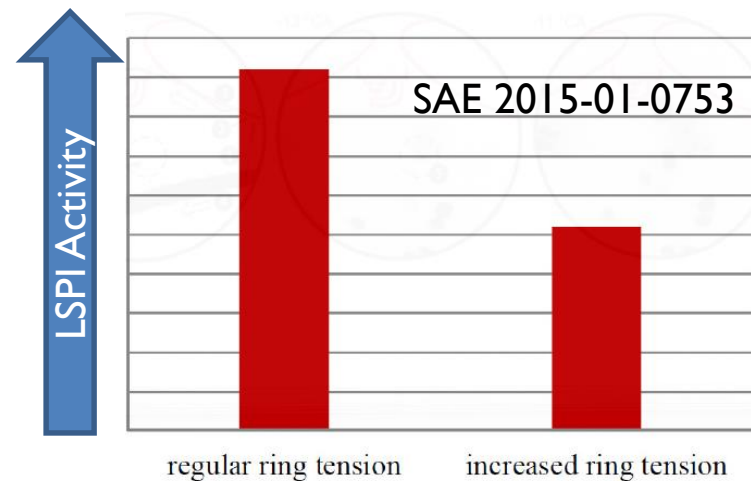
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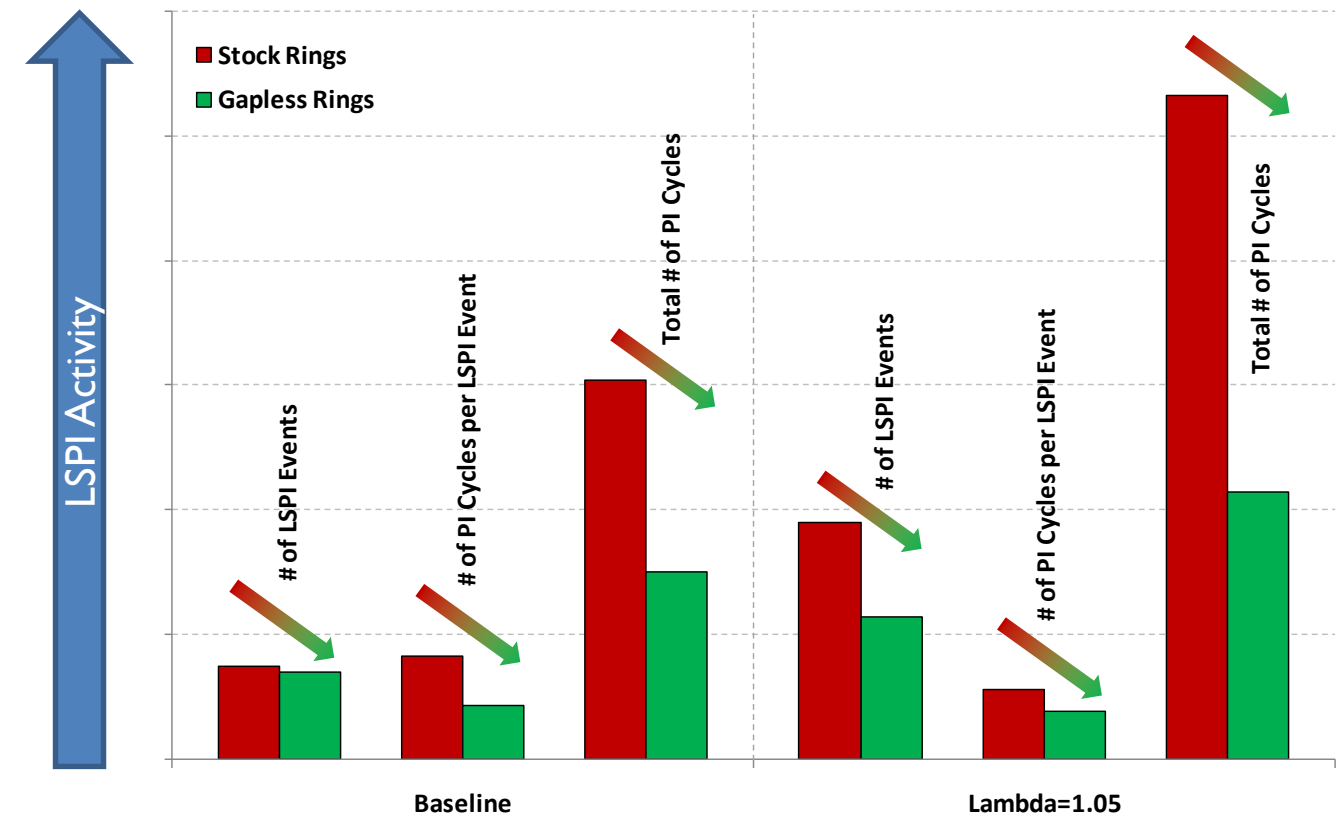


Design - Ring Tension and Gaps

- Higher ring tension and gapless rings reduce LSPI tendency
- Both impact the oil transfer to the crevice region
- Need to balance LSPI benefits with friction and durability



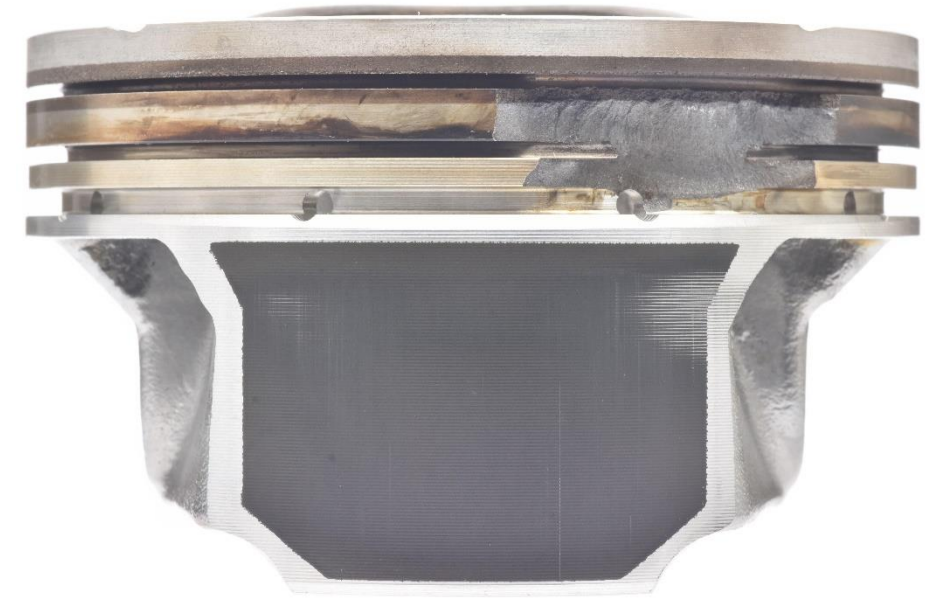
www.totalseal.com



Design – Piston Strength

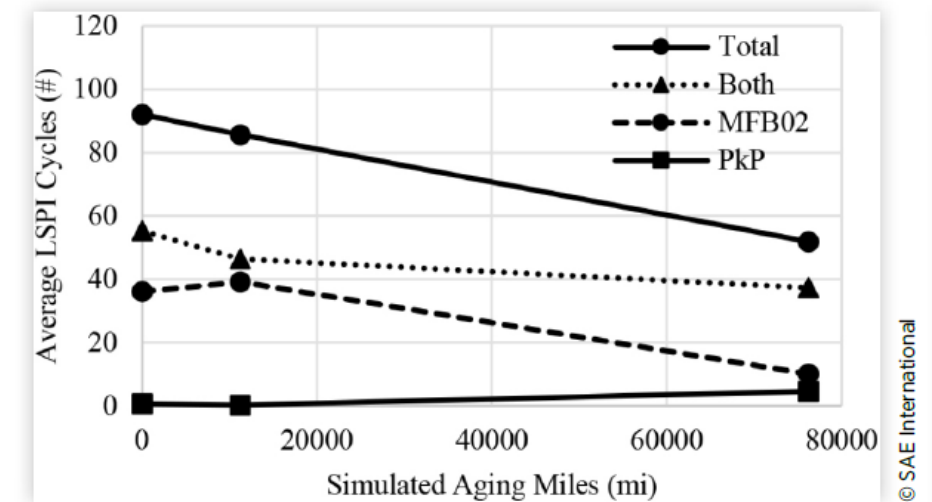
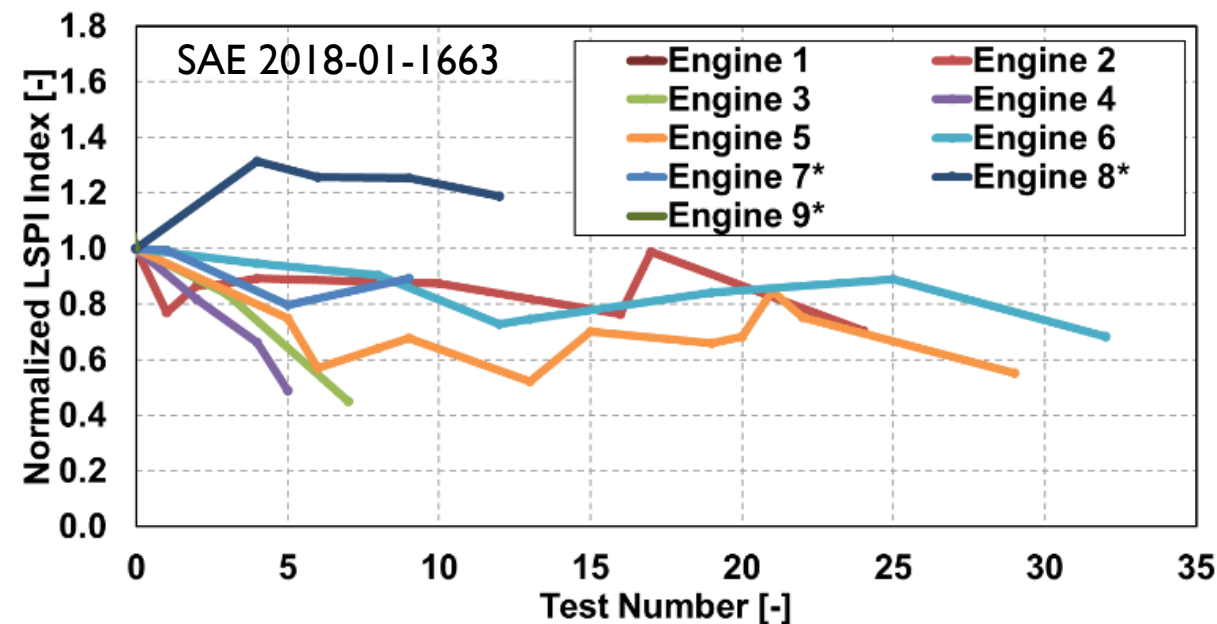
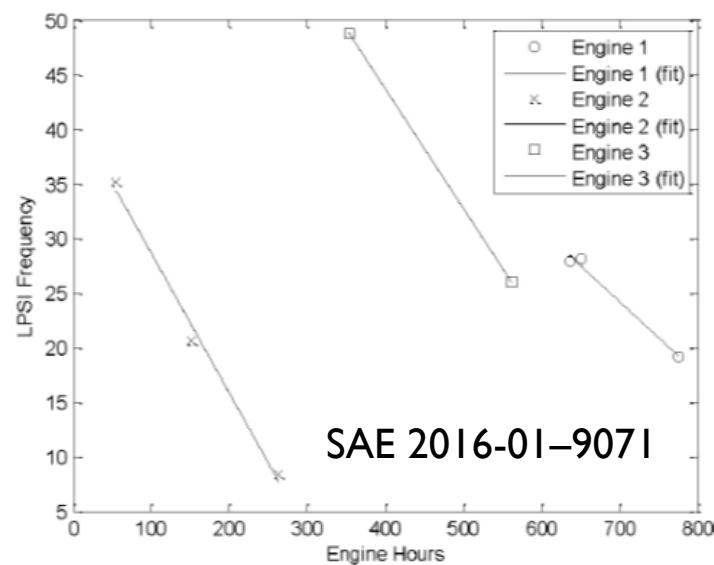
- LSPI typically manifests in piston ring land and skirt damage
 - Less commonly spark plug, valves or conrod damage
- Improved piston design and material choices can enhance strength and improve durability
 - LSPI damage is unlike that caused by spark-knock and may require different solutions
- Ultimately a cost-benefit trade-off

<https://www.sae.org/news/2017/06/mahle-tests-for-mega-knock-in-downsized-boosted-engines>



Engine Condition - Age

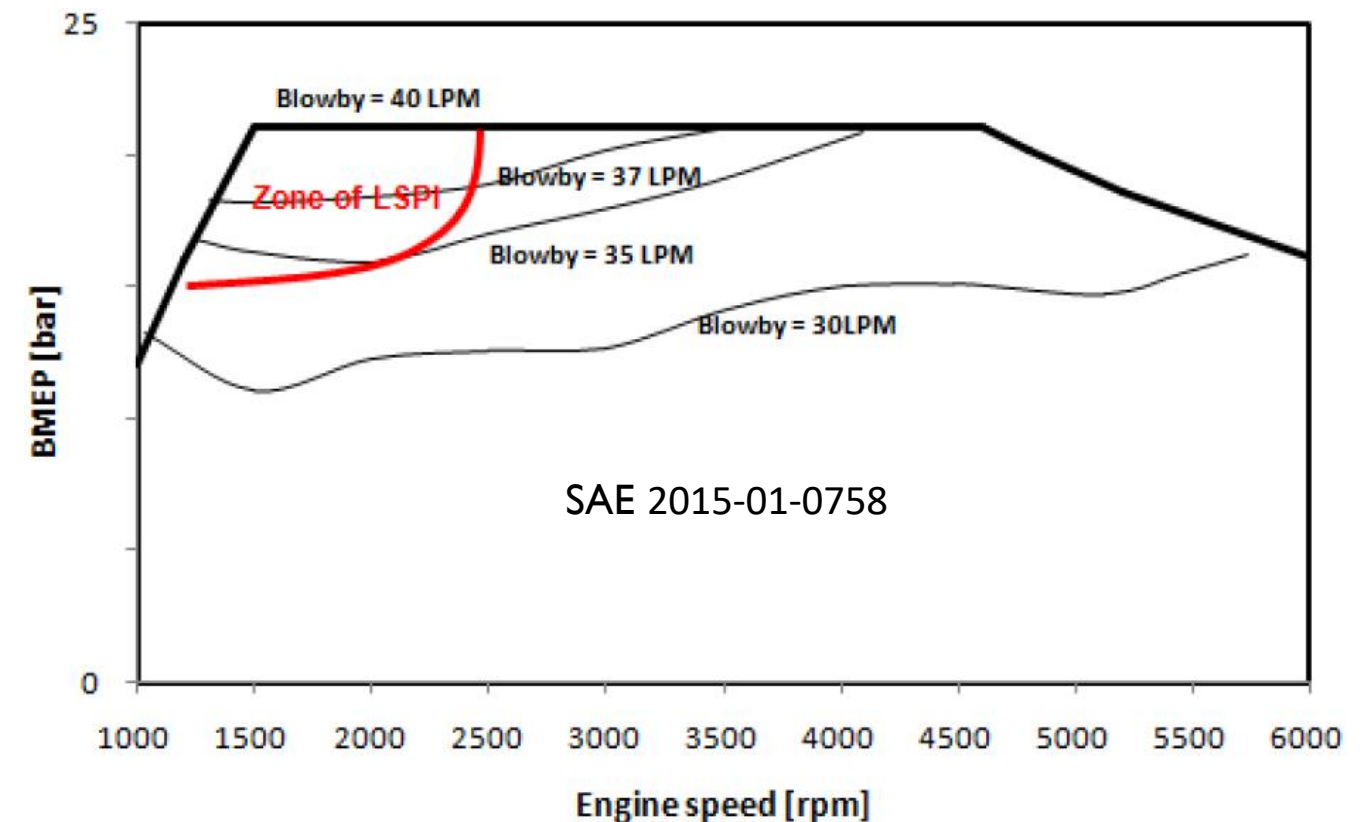
- New oil LSPI activity generally reduces with engine age
 - Test bed (left and middle) and on-road (right) aged engine LSPI activity
- Attributed to engine wear and changes in flow past ring pack and into crevice
 - Countered by re-honing and bore damage (*not shown*)



<https://doi.org/10.4271/03-11-01-0002>

Engine Condition – Fugitive Oil

- Increased LSPI due to increased blow-by either due to design, maintenance or engine wear
- Similar observations with PCV and turbo-seal leakage
- Goldilocks response
 - A small increase increases LSPI
 - A large increase decreases LSPI



Engine Condition - Deposits

- Deposits liberated during first LSPI cycle of a multi-cycle event
 - May not heat up sufficiently within a single engine cycle to cause preignition (*top*)
 - Volatile components incorporated into deposits required for ignition
- Dynamics of real-life deposits nearly impossible to measure / replicate repeatably in an engine
 - “Dirty-up” pre-conditioning in some LSPI bench tests aimed at consistency
- Rebuilding and cleaning of engine does not affect LSPI activity (*bottom*)

SAE 2014-01-1218

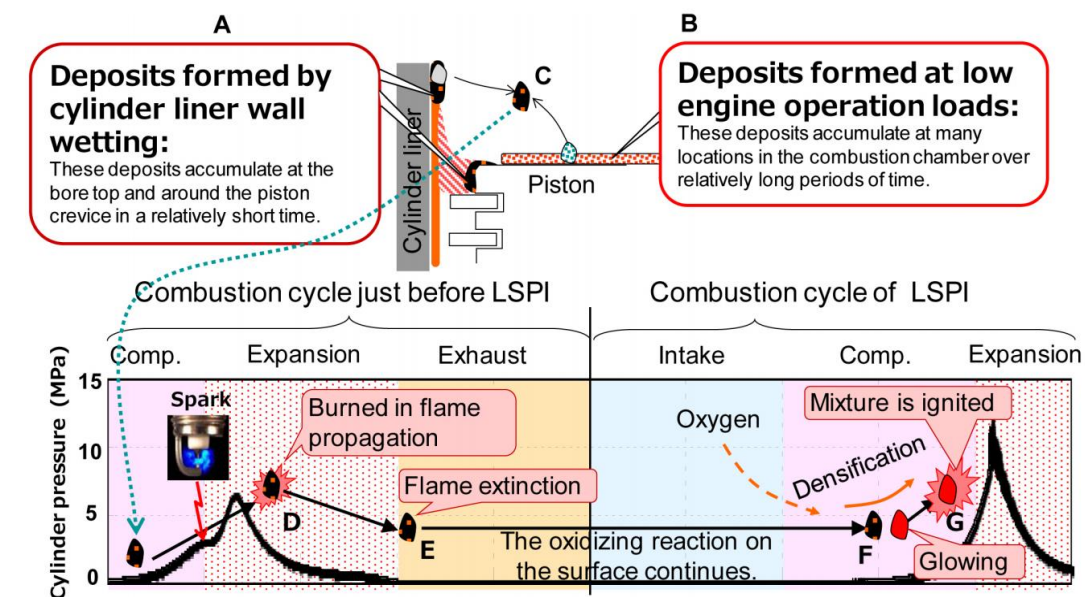
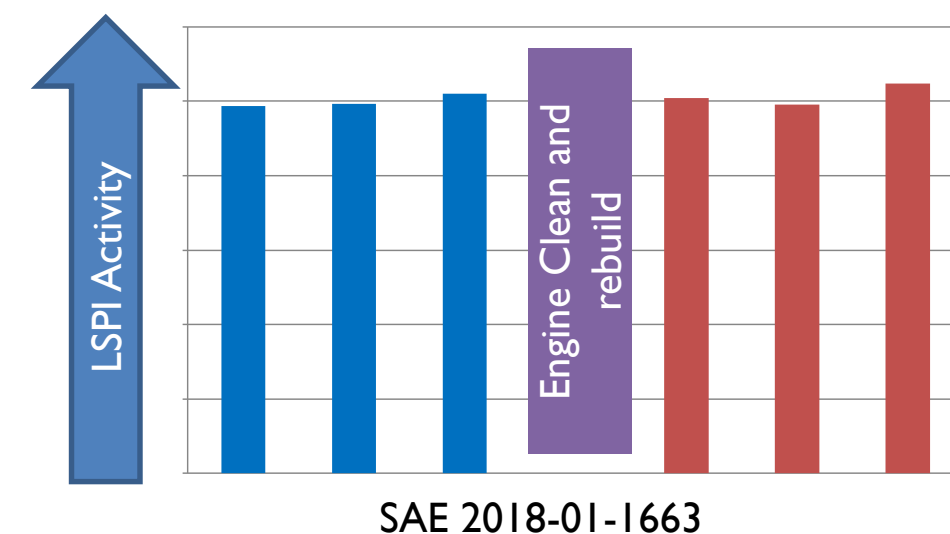
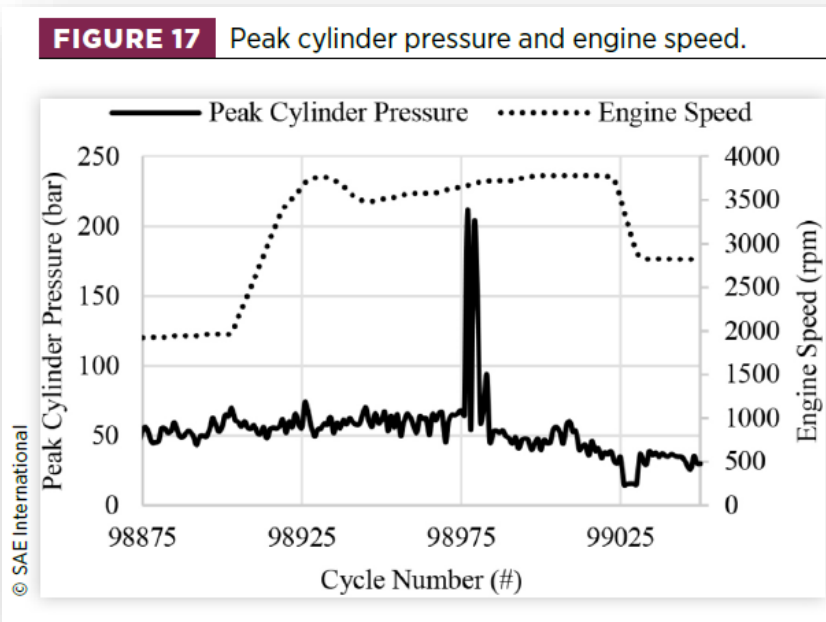


Figure 15. Schematic of new LSPI mechanism.

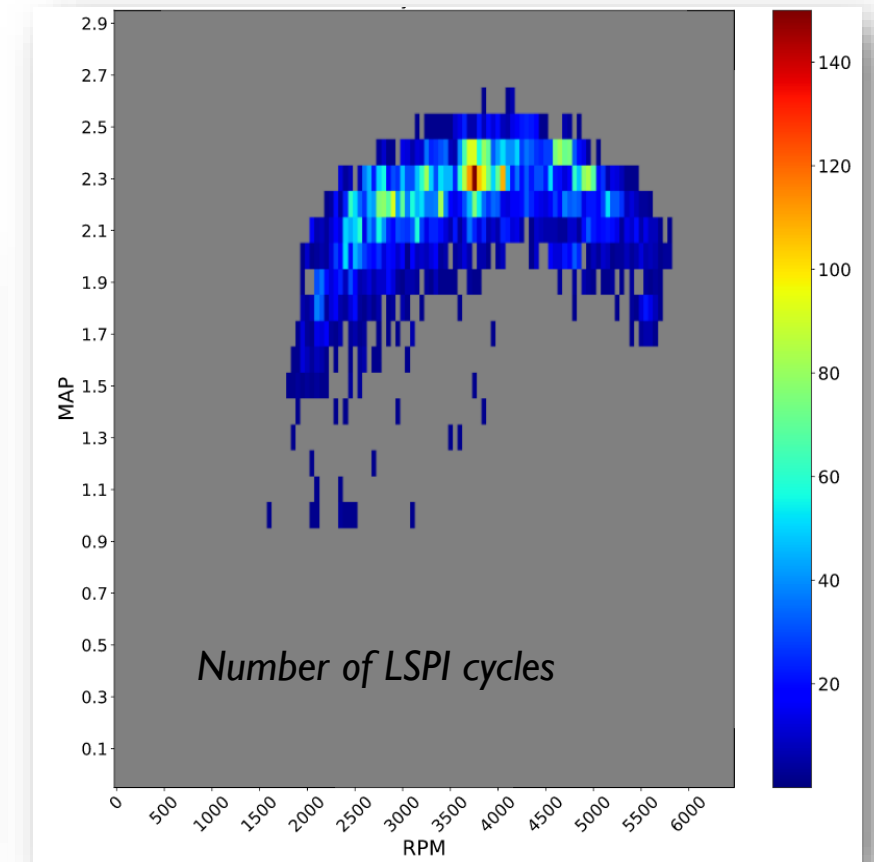


Transient LSPI

- Real-life LSPI is truly a transient phenomenon during which the factors above may reinforce or detract from each other due to dynamics
 - No known systematic study
- On-road LSPI encountered at higher engine speeds ($>3,000$ rpm) and with “real” deposits
 - Rare event ($\sim 5,000/200$ million cycles)



<https://doi.org/10.4271/103-11-01-0002>



Conclusions

- Factors that impact the amount or composition of the crevice fluid appears to impact LSPI
 - Not all design, operation or calibration adjustments are attainable due to emissions / performance / durability / cost considerations
- Operational and hardware factors are agnostic to fluid changes
- Little evidence of the impact of engine deposits, although it is thought to be complementary
- Quantification of transient or real-life LSPI response still open
 - OEM proprietary flagging and mitigation are already in use

Recommendations

- LSPI observed during steady-state testing transients may be mined for additional insight
- Determine how “steady state factors” may manifest during transient testing
 - Acceleration /deceleration
 - Tip-in / tip-out
 - Warm-up / cool down
- Determine the impact on LSPI severity, not only frequency
- Understanding the impact of “real” deposits
- Cost-benefit analyses of design and calibration mitigation versus fluid solutions
 - Likely not in the research realm

Thank You

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