2015 CRC VEHICLE EMISSIONS PROGRAM

on

Effects of 85 and 87 Anti-knock Index (AKI) Gasoline Ethanol Blends on U.S. Light-Duty Vehicle Emissions, Fuel Economy, and Performance at Two Elevations (1,000 ft. and 5,000 ft.)

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(CRC Project No. E-108)

Prepared by the

CRC Emissions Committee

of the

Coordinating Research Council

March 2015

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I. Executive Summary

a. Program Summary

This Program investigated the effects of gasoline anti-knock index (AKI¹) on vehicle fuel economy, tailpipe emissions and engine and exhaust performance parameters for a fleet of nine model year 2008 – 2013 passenger cars and light duty trucks. Three different vehicle chassis dynamometer laboratories, each possessing variable altitude, temperature, and humidity controls, performed a total of 305 vehicle tests over the course of nine months. Two test fuels, closely matched in composition and energy content, however differing in their AKI value (87 and 85 AKI) were tested. The vehicles were tested under two simulated elevations: 1,000 ft. and 5,000 ft., (305 and 1,524 m). Each fuel, vehicle, and elevation combination was tested a minimum of two times using three standard US and California vehicle tailpipe emissions test cycles: US FTP-75, LA92 Unified, and US06. The test cycles were chosen to investigate the effects of a range of driving styles and severities on vehicle octane requirement. The test cycles are described in detail in Appendix E. Statistical analyses of the nine-vehicle-fleet means, individual-vehicle means, and correlation to vehicle attributes were conducted. A Data Capture Team was responsible for the vehicle tests, while a Data Analysis Panel performed the appropriate analyses of the acquired data.

b. Quality of Data Summary – Analysis of Variation, Outliers, and Vehicle Response Drift Rigorous quality assurance and control procedures were employed by the Data Capture Team to minimize the inherent variability introduced by testing that spanned several months and included three separate chassis dynamometer labs. Quality assurance included standardized test procedures (see Appendix B) and application of engineering judgment to flag when additional testing was needed. No data were removed without a documented engineering reason such as an emissions analyzer error or dynamometer malfunction.

The Data Analysis Panel developed statistical models and conducted outlier analyses to indicate when results from combinations of factors did not fit the generated models. Of the 259 core emissions tests collected using the 85 and 87 AKI fuels, 13 data points or 5% of the total were flagged as potential outliers outside the six sigma bounds for Studentized residuals for any of the primary measurements (NMHC, CO, CO_2 , NO_x) and calculation of fuel economy. In general, the quality of data and test precision were considered to be good for a vehicle emissions program of this size.

c. Conclusions

 The test program methodology of using standardized emissions test cycles to evaluate fuel octane number effects on vehicle response was a good approach to gain understanding. The use of a range of emissions test cycles enabled the evaluation of trends in vehicle response and showed driving style is important with respect to the impacts of fuel octane number.

2. Mean FE, CO₂, CO Results for the Combined Nine Vehicle Fleet - Octane for Combined Elevations

The analysis of variance (ANOVA) and linear statistical models used initially to evaluate fleet average FE, CO₂, and CO aggregated the data across the nine vehicles and two elevations but kept test cycle (US FTP-75, LA92 and US06) separate in order to understand the effects of octane number. The fleet average Fuel Economy (FE) results are shown below. The comparison intervals shown in the figure allow assessments of the statistical significance of differences in mean responses to fuel AKI at an Alpha (p-value) of 0.05. Comparison

¹ AKI is defined as the average of the Research Octane Number and Motor Octane Number ratings determined by ASTM International's test methods D2699 and D2700, respectively and calculated as AKI = (RON+MON)/2.

intervals that overlap (e.g., those for 85 AKI and 87 AKI on the US FTP-75 cycle) indicate that the differences in means are not statistically significant while those that don't overlap (e.g., those for 85 AKI and 87 AKI on the US06 cycle) indicate significantly different means.

The mean fuel economy response to fuel AKI is statistically significant when evaluated on the LA92 and US06 test cycles but not the US FTP-75.

The graph below includes the two test fuel names listed as 85 E10 and 87 E10. The two test fuels nominally contained 10% ethanol by volume (E10) and are detailed in Table 4 of the main body of this report. Some figures later in the report show the two test fuel names as simply 85 and 87 AKI, which are the same two test fuels but using a shortened naming convention.



Fleet Averaged Fuel Economy (mpg) Octane Number Effects for Combined Elevations

The three ANOVA models (for US FTP-75, LA92 and US06) yield the following conclusions:

- a. The goodness-of-fit statistics (R-squared terms) for the three test cycle models are very high, i.e. greater than 0.99. Thus, the models fit the data very well.
- b. Vehicle-to-vehicle variability provides the largest influence on mean fuel consumption response to fuel AKI (by two orders of magnitude as measured by the ANOVA model F-ratio statistic) for each of the three emissions driving cycles evaluated.
- c. Variation in altitude (1000 ft. vs 5000 ft.) has a statistically significant effect for the US FTP-75 and LA92 models and is marginally significant (p-value between 0.05 and 0.10) for the US06.
- d. The effect of variation in fuel AKI is marginally significant for the US FTP-75 model and significant for the LA92 and US06 models. Variability in fuel AKI explains a greater proportion of the total variability in measured fuel consumption as the test cycle severity increases.

e. Interaction between altitude and fuel AKI does not provide a statistically significant contribution to the total observed variance in the data for any of the three ANOVA models.

3. Mean FE, CO₂, CO Results for the Combined Nine Vehicle Fleet - Octane Effects within an Elevation

The mean FE, CO₂, and CO₂ data from the combined nine vehicle fleet are shown in the tables below along with the p-values obtained from statistical analysis.

- a. P-values less than 0.05 indicate when the means are significantly different between the two fuels tested and are shaded yellow. The light gray shaded data show the p-values between 0.05 and 0.10 and are considered marginally significantly different.
- b. At 5,000 ft., the US06 FE p-value is 0.11, and just outside the definition of a marginally significant effect at the 90% confidence level.
- c. The nine vehicle fleet FE decreased by about 0.4% while operating on the 85 AKI fuel during the US FTP-75 tests and decreased between 1.6% and 2.4% for the US06 tests, depending on elevation.
- d. Consistent with the loss of FE, the fleet CO₂ results correspondingly increased for the 85 AKI test fuel.
- e. The fleet CO results showed mixed effects during the US FTP-75, with 5,000 ft. showing improvement when using 87 AKI, and CO increased by 24% to 52% for the US06 tests, regardless of elevation while operating on the 85 AKI fuel.
- f. And lastly, it's noted that for a given AKI level, FE at 5,000 ft. elevation is always greater than at 1,000 ft. as a result of reduced parasitic pumping losses within the vehicle's engine due to the lower atmospheric pressure.

| FE (mpg) | | | | | | | | | | |
|-------------------------|---------|---------|---------|---------|----------|---------|---------|---------|---------|----------|
| Outliers Removed | 5000 | 5000 | p-value | Delta | % Change | 1000 | 1000 | p-value | Delta | % Change |
| | 85 AKI | 87 AKI | | 85 - 87 | 87> 85 | 85 AKI | 87 AKI | | 85 - 87 | 87> 85 |
| FTP-75 | 23.8775 | 23.9691 | 0.7353 | -0.0916 | -0.4% | 23.1667 | 23.2834 | 0.5507 | -0.1167 | -0.5% |
| LA92 | 23.3837 | 23.5172 | 0.3083 | -0.1335 | -0.6% | 22.8694 | 23.0942 | 0.0306 | -0.2248 | -1.0% |
| US06 | 22.5226 | 22.9002 | 0.1144 | -0.3776 | -1.6% | 22.2344 | 22.7917 | 0.0122 | -0.5573 | -2.4% |

| CO2 (gpm) | | | | | | | | | | |
|-------------------------|----------|----------|---------|---------|----------|----------|----------|---------|---------|----------|
| Outliers Removed | 5000 | 5000 | p-value | Delta | % Change | 1000 | 1000 | p-value | Delta | % Change |
| | 85 AKI | 87 AKI | | 85 - 87 | 87> 85 | 85 AKI | 87 AKI | | 85 - 87 | 87> 85 |
| FTP-75 | 336.3948 | 335.1829 | 0.6225 | 1.2119 | 0.4% | 346.8585 | 345.5458 | 0.6155 | 1.3127 | 0.4% |
| LA92 | 344.5251 | 343.3285 | 0.7290 | 1.1966 | 0.3% | 352.8187 | 350.2167 | 0.1758 | 2.6020 | 0.7% |
| US06 | 353.3398 | 348.2110 | 0.0965 | 5.1288 | 1.5% | 357.8025 | 351.5022 | 0.0415 | 6.3003 | 1.8% |

| CO (gpm) | | | | | | | | | | |
|------------------|--------|--------|---------|---------|----------|--------|--------|---------|---------|----------|
| Outliers Removed | 5000 | 5000 | p-value | Delta | % Change | 1000 | 1000 | p-value | Delta | % Change |
| | 85 AKI | 87 AKI | | 85 - 87 | 87> 85 | 85 AKI | 87 AKI | | 85 - 87 | 87> 85 |
| FTP-75 | 0.2802 | 0.2708 | 0.9348 | 0.0094 | 3.5% | 0.2626 | 0.2772 | 0.7918 | -0.0146 | -5.3% |
| LA92 | 0.2314 | 0.2249 | 0.9905 | 0.0065 | 2.9% | 0.2073 | 0.1796 | 0.4888 | 0.0277 | 15.4% |
| US06 | 1.8881 | 1.5199 | 0.3359 | 0.3682 | 24.2% | 1.7008 | 1.1183 | 0.0124 | 0.5825 | 52.1% |

4. The Use of Trend Analyses versus Confidence Tests

If the vehicle fleet FE averages were truly equivalent, then one would expect fifty percent of the averages for one octane test fuel to fall below the second octane test fuel fleet averages and fifty percent above. This relatively consistent pattern of worse vehicle performance (evaluated on a fleet average basis) with the use of 85 AKI test fuel versus 87 AKI fuel led the Data Analysis Panel to conduct several binomial probability trend analyses. The statistical trend analyses indicate the probability that all six emissions cycle and altitude combinations of FE or CO_2 would show poorer performance for the 85 AKI case solely by random chance is very small. The statistical probability that all six FE averages would be in the same direction is 1.6%. (Calculation: $0.5^6 = 1/64 = 0.015625$, which is significant [p ≤ 0.05].) While binominal trend analyses may be useful in identifying directional trends, they do not take into account the magnitude or statistical significance of the measured differences.

The figure below shows that for a given elevation, the impact of operating the test fleet on 85 AKI fuel relative to 87 AKI fuel for FE becomes more significant (smaller p-value) as the driving cycle becomes more demanding, starting with the milder US FTP-75-type driving and up to the more aggressive US06. The p-value for the US06 case at 5,000 ft. is 0.11. A statistical analysis was conducted to determine how many test vehicles would have been required for the octane number FE effect to be significant for the US06 5,000 ft. case at a p-value of 0.05. The analysis concluded that a test fleet of twelve vehicles instead of nine would have been needed, assuming that the additional vehicles showed the same behavior as those already tested.

The fleet average FE difference between 5,000 ft. and 1,000 ft. is significant with a p-value of 0.047 but this is due to the combined effects of lower atmospheric pressure and octane number on vehicle FE. At 5,000 ft. the lower air density requires the closed loop air-to-fuel ratio feedback control of the engine control module to open the throttle wider compared to that with more dense air at 1,000 ft., which in turn, reduces parasitic losses from engine pumping. These combined effects are discussed further below.



The chart below shows the percent change in fleet average FE with respect to test cycle average vehicle speed while operating on the 85 AKI fuel relative to the 87 AKI fuel. The test cycle average speeds are as follows: US FTP-75 (21.2 mph), LA92 (24.6 mph), and US06 (48.4 mph).



5. Mean FE, CO₂, CO Results for the Combined Nine Vehicle Fleet - Octane Effects Across Elevations

The tables below show the FE, CO₂, and CO average fleet results when operating the vehicles on 85 AKI fuel at 5,000 ft. and 87 AKI fuel at 1,000 ft. as is commonly done in today's U.S. market. Because of the lower atmospheric pressure at 5,000 ft. and the engines' response to it, the interpretation of results becomes more convoluted. When the vehicles are less knock limited as during the US FTP-75 and LA92 emissions cycle tests, the fleet average fuel economies at 85 AKI/5,000 ft. case are higher than at 87 AKI/ 1,000 ft. and the differences are statistically significant. However, when the vehicles become knock limited during the US06 cycle, the fleet average fuel economy at 85 AKI/5,000 ft. is lower than at 87 AKI/1000 ft. but the difference is not statistically significant. CO₂ in general behaves inversely to FE. Fleet average CO is higher at 85 AKI / 5,000 ft. than at 87 AKI/1000 ft. for all three emissions test cycles evaluated and is significantly higher during the more knock limited US06 test cycle.

| FE (mpg) | | | | | |
|-------------------------|----------|----------|---------|-------------------------------|--------------|
| Outliers Removed | 5000 | 1000 | p-value | Combined Effects Delta | % Change |
| | 85 AKI | 87 AKI | | (85 - 87) | Delta / (87) |
| FTP-75 | 23.8775 | 23.2834 | <0.0001 | 0.5941 | 2.6% |
| LA92 | 23.3837 | 23.0942 | <0.0001 | 0.2895 | 1.3% |
| US06 | 22.5226 | 22.7917 | 0.3869 | -0.2691 | -1.2% |
| | | | | | |
| CO2 (gpm) | | | | | |
| Outliers Removed | 5000 | 1000 | p-value | Combined Effects Delta | % Change |
| | 85 AKI | 87 AKI | | (85 - 87) | Delta / (87) |
| FTP-75 | 336.3948 | 345.5458 | <0.0001 | -9.1510 | -2.6% |
| LA92 | 344.5251 | 350.2167 | <0.0005 | -5.6916 | -1.6% |
| US06 | 353.3398 | 351.5022 | 0.8360 | 1.8376 | 0.5% |
| | | | | | |
| CO (gpm) | | | | | |
| Outliers Removed | 5000 | 1000 | p-value | Combined Effects Delta | % Change |
| | 85 AKI | 87 AKI | | (85 - 87) | Delta / (87) |
| FTP-75 | 0.2802 | 0.2772 | 0.9976 | 0.0030 | 1.1% |
| LA92 | 0.2314 | 0.1796 | 0.0642 | 0.0518 | 28.8% |
| US06 | 1.8881 | 1.1183 | 0.0025 | 0.7698 | 68.8% |

The fuel consumption figure below shows that during the non- or lightly knocking US FTP-75 and LA92 cycles, the effect of lower atmospheric pressure on lower fuel consumption at 5,000 ft. relative to 1,000 ft. is apparent. However, during the more knock limited US06 cycle, seven of the vehicle mean changes in fuel consumption trend above zero. The confidence intervals shown indicate many of the differences are not statistically significant.



Individual Vehicle Fuel Consumption Deltas (85 AKI@5000' gallons - 87 AKI@1000' gallons / 100 miles)

6. Mean Vehicle Fleet Performance Parameter Results for the Combined Vehicle Fleet - Comparisons within an Elevation: Engine speed, Percent Engine Load, Ignition Timing, pre-Catalyst Exhaust Temperature, and mid-Catalyst Exhaust Temperature

Only eight of the nine test vehicles were instrumented with data loggers to record ECM parameters. The combined eight vehicle fleet means and percent changes for engine speed, percent load, and mid-catalyst temperatures shown in the body of the report show no statistically significant differences between operating on the 85 and 87 AKI test fuels. Spark retard (moving ignition timing closer to top dead center of piston travel) and pre-catalyst exhaust temperatures are significantly different between the two test fuels while operating on the US06 cycle at 5,000 ft. The resultant rejected in-cylinder heat from delayed combustion during the more knock-limited US06 cycle leads to increased pre-catalyst temperature differences. Summary tables focused on Ignition timing and pre-catalyst temperatures, respectively, are shown below.

| Ignition Timing (° BI | TDC) | | | | | | | | | |
|-----------------------|--------|--------|---------|---------|----------|--------|--------|---------|---------|----------|
| Outliers Removed 5000 | | 5000 | p-value | Delta | % Change | 1000 | 1000 | p-value | Delta | % Change |
| | 85 AKI | 87 AKI | | 85 - 87 | 87> 85 | 85 AKI | 87 AKI | | 85 - 87 | 87> 85 |
| FTP-75 Bags 1&2 | 23.30 | 23.18 | 0.9344 | 0.13 | 0.5% | 23.39 | 23.27 | 0.9444 | 0.12 | 0.5% |
| FTP-75 Bag 3 | 23.03 | 23.45 | 0.2459 | -0.42 | -1.8% | 23.11 | 23.56 | 0.9606 | -0.45 | -1.9% |
| LA92 | 21.23 | 21.43 | 0.9182 | -0.20 | -0.9% | 21.31 | 21.58 | 0.8085 | -0.27 | -1.2% |
| US06 | 21.71 | 22.62 | 0.0193 | -0.92 | -4.1% | 21.47 | 22.19 | 0.0638 | -0.72 | -3.3% |

| Pre-Cat Temp. (°C) | | | | | | | | | | |
|--------------------|--------|--------|---------|---------|----------|--------|--------|---------|---------|----------|
| Outliers Removed | 5000 | 5000 | p-value | Delta | % Change | 1000 | 1000 | p-value | Delta | % Change |
| | 85 AKI | 87 AKI | | 85 - 87 | 87> 85 | 85 AKI | 87 AKI | | 85 - 87 | 87> 85 |
| FTP-75 Bags 1&2 | 451.88 | 450.88 | 0.7868 | 1.00 | 0.2% | 457.47 | 457.36 | 0.9996 | 0.11 | 0.0% |
| FTP-75 Bag 3 | 463.01 | 461.97 | 0.9409 | 1.04 | 0.2% | 467.02 | 464.31 | 0.4751 | 2.71 | 0.6% |
| LA92 | 512.64 | 510.26 | 0.6397 | 2.38 | 0.5% | 514.38 | 510.75 | 0.2589 | 3.63 | 0.7% |
| US06 | 637.49 | 629.52 | 0.0124 | 7.97 | 1.3% | 640.84 | 635.08 | 0.3228 | 5.76 | 0.9% |

7. Mean FE, CO₂, CO Results for Individual Vehicles

The change in fuel consumption and fuel economy for each vehicle when operating on 85 compared 87 AKI gasoline within a given elevation are shown in the figure and table below, respectively for the three test cycles. For the majority of vehicles, fuel consumption averages are higher while operating on 85 AKI gasoline compared to 87 AKI fuel and the level of fuel consumption increases with test cycle severity. The confidence intervals shown indicate many of the differences are not statistically significant.



Individual Vehicle Fuel Consumption Deltas (85 AKI - 87 AKI gallons / 100 miles)

| | | Fuel Economy Change (%) | | | | | | |
|---------|----------|-------------------------|-------------|-------|--|--|--|--|
| | Altitude | | 87 to 85 AK | [] | | | | |
| VNumber | (ft.) | US FTP | LA92 | US06 | | | | |
| 1 | 5000 | -1.06 | -0.92 | -0.67 | | | | |
| 2 | 5000 | -0.07 | -0.24 | -2.03 | | | | |
| 3 | 5000 | -0.55 | 0.02 | -0.11 | | | | |
| 4 | 5000 | -1.51 | -0.40 | -0.40 | | | | |
| 5 | 5000 | 0.41 | -1.49 | -3.48 | | | | |
| 6 | 5000 | -1.73 | -0.43 | -2.44 | | | | |
| 7 | 5000 | 0.26 | -0.85 | -0.70 | | | | |
| 8 | 5000 | -0.75 | 0.37 | -2.38 | | | | |
| 9 | 5000 | 0.39 | -0.75 | -1.70 | | | | |
| 1 | 1000 | -0.15 | -1.40 | -3.32 | | | | |
| 2 | 1000 | -0.62 | -0.47 | -1.55 | | | | |
| 3 | 1000 | 0.14 | -1.22 | 6.75 | | | | |
| 4 | 1000 | 2.40 | -0.06 | -0.14 | | | | |
| 5 | 1000 | 0.74 | -4.26 | -2.60 | | | | |
| 6 | 1000 | -0.88 | -0.89 | -2.72 | | | | |
| 7 | 1000 | -1.45 | -1.56 | -1.96 | | | | |
| 8 | 1000 | 0.01 | -0.04 | -2.62 | | | | |
| 9 | 1000 | -0.83 | -2.34 | -4.60 | | | | |

Individual Vehicle Fuel Economy Percent Change when moving from 87 to 85 AKI Fuel

If AKI had no consistent effect on fuel economy (FE), each of the individual vehicle percent change deltas would have a 50% chance of being positive and a 50% chance of being negative. For a given elevation, of the 27 percent change deltas (nine vehicles with three test cycles each) at each altitude, 22 FE deltas were negative with the 85 AKI fuel. The chance of flipping a fair coin 27 times and getting 22 or more tails is 0.0008, which is a significant p-value (p < 0.05) for the one-sided test and considers individual vehicle response. Similar binomial statistical analyses were conducted for CO_2 and CO emissions and are summarized below. While binominal trend analyses may be useful in identifying directional trends, they do not take into account the magnitude or statistical significance of the measured differences.

| One-sided p-value for x out of 27 deltas (9 vehicles x 3 test cycles) | | | | | | | | |
|---|----------|----|---------|--|--|--|--|--|
| with worse performance for 85 AKI (positive for emissions, | | | | | | | | |
| negative for fuel economy) | | | | | | | | |
| Measure | Altitude | х | p-value | | | | | |
| СО | 1000 | 17 | 0.12 | | | | | |
| CO ₂ | 1000 | 19 | 0.03 | | | | | |
| Fuel Economy | 1000 | 22 | 0.00 | | | | | |
| СО | 5000 | 18 | 0.06 | | | | | |
| CO ₂ 5000 20 0.02 | | | | | | | | |
| Fuel Economy | 5000 | 22 | 0.00 | | | | | |

The test program included nine test vehicles with a range of attributes; production Model Years 2008 – 2013, four passenger cars and five light duty trucks, engine displacements from 1.4 – 5.4L, two direct and seven port fuel injected, and two turbocharged and seven naturally aspirated engines.

Evaluating the effects of 85 and 87 AKI fuels on the primary emissions metric CO₂, the data showed:

- Cars vs Trucks Trucks had statistically significant higher absolute levels of CO₂ compared to the passenger cars. However, the incremental effects of 85 and 87 AKI for these two vehicle types was not significant.
- DI vs PFI The fuel injection type was not statistically significant for absolute CO₂ emissions levels. However, the incremental effect of 85 and 87 AKI for these two injection types was, in some cases, statistically significant.
- c. Naturally Aspirated vs Turbo-charged The intake air aspiration type was not found to be statistically significant for absolute, nor incremental CO₂ levels.
- d. Test fleet Hardware Attributes Balance Having a better balanced vehicle fleet for fuel injection and induction air aspiration types in future programs will help the statistical analysis of data.
- e. Correlation with Vehicle Load Factor Vehicle load factor is defined as vehicle mass per unit engine displacement. The exhaust CO₂ to vehicle load factor correlation R² values for the lighter loaded US FTP-75 and LA92 test cycles are low and both about 0.5. The US06 CO₂ to vehicle load factor R² decreases to 0.4 as this test cycle is more knock limited and the influence of increased CO confounds the CO₂ response. Response to 85 AKI octane is very vehicle specific and not well correlated to its load factor.
- For the primary vehicle emissions and performance metrics of this program, a series of figures was
 prepared (Figures 41 48) to help the reader visualize the convoluted influences of fuel AKI octane
 number, elevation, and test cycle severity on individual vehicle response.
- 10. And lastly, the Appendix includes additional test program details, data analyses, and pertinent supplemental information, including the full set of Emissions and Vehicle Performance results.

II. Abstract

The Coordinating Research Council, Inc.'s (CRC) Emissions and Performance Committees jointly conducted a vehicle chassis dynamometer test program on a fleet of modern light duty motor vehicles in response to a request from ASTM International's Sub-committee D02.A to determine the effects of 85 and 87 AKI (anti-knock index) rated fuels on tailpipe emissions and general vehicle performance. The octane number effects were evaluated at two elevations, 1,000 and 5,000 ft. (305 and 1,524 m) above sea level, and used test fuels with closely matched fuel compositions, except differing in their AKI octane ratings. Nine modern light duty cars and trucks were chosen for the vehicle test fleet in order to cover a range of vehicle attributes in today's U.S. car fleet; production model years 2008 – 2013, naturally aspirated vs. turbo-charged air induction systems, port-fuel injected vs. direct injected fuel injection systems, a range of Federal Tier 2 emissions certifications, and a range of vehicle load factors (vehicle mass to engine displacement size ratios). Vehicle testing was conducted at three different automotive manufacturer's test sites using variable altitude emissions chassis dynamometers with conditioned environment capability (temperature, humidity, and pressure.) Each vehicle, fuel, and altitude combination was tested using three standard vehicle emissions certification driving cycles in order to evaluate a range of driver behaviors.

III. Introduction

CRC Project E-108 was designed to generate vehicle performance, fuel economy, and emissions data to help update the general understanding of octane and altitude effects on modern vehicle performance. The specifications for gasoline used in spark-ignition automobile engines in the United States are detailed in ASTM International's, "Standard Specification for Automotive Spark-Ignition Engine Fuel", commonly referred to as ASTM D4814. Although ASTM D4814 does not explicitly list mandatory minimum specifications for antiknock/octane number ratings, it does provide non-mandatory information in its Appendix describing the effects of altitude on vehicle antiknock requirements for pre-1984 vehicles. These older vehicles lack sophisticated closed-loop computerized engine control module controls and are predominantly large cylinder bored, carbureted, naturally aspirated designs having emissions certifications much less stringent than today's vehicles. Additionally, the D4814 Appendix shows areas in the western United States where reduced antiknock requirements for pre-1984 vehicles are applicable based on the altitude of the area. Therefore, ASTM D02, Sub-committee A is seeking to update D4814 based on controlled vehicle performance studies and data.

The importance of fuel antiknock quality is highlighted by its impact on vehicle design and performance. Modern day automobile engines are calibrated for maximum fuel economy and performance, while minimizing emissions using the octane grade of gasoline that the manufacturer recommends or requires for use in the vehicle's owner's manual. However, in order to avoid engine failure or permanent damage in case a lower fuel octane than that specified in the owner's manual is used, the engine has to be "protected" for the minimum octane fuel available in the market of sale. Consequently, the engine design and calibration is constrained by the lowest antiknock index fuel commercially available.

The CRC Emissions and Performance Committees collaboratively designed a vehicle chassis dynamometer octane performance test program, as described in the Methodology Section of this report, to help better understand the impact of gasoline octane number ratings on vehicle performance and more specifically, to quantify the change in vehicle performance when operating on 85 and 87 AKI fuels.

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VI. Acronyms and Abbreviations

| AKI | Anti-knock Index | FE | Fuel Economy |
|------|-------------------------------|-------|---------------------------------|
| BTDC | Before Top Dead Center | MON | Motor Octane Number |
| CO | Carbon Monoxide | MPH | Miles per Hour |
| CO2 | Carbon Dioxide | NMOG | Non-methane Organic Gases |
| COV | Coefficient of Variation | OBD | On-Board Diagnostics |
| DVPE | Dry Vapor Pressure Equivalent | OEM | Original Equipment Manufacturer |
| ECM | Engine Control Module | RMSSE | Root Mean Squared Speed Error |
| EOT | End of Testing | RON | Research Octane Number |
| GPM | Gallons per Mile | SOT | Start of Testing |

VII. Program Teams

a. Vehicle Data Capture Team

| Blash, Eric | Fiat Chrysler Automobiles |
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iat Chrysler Automobiles ord Motor Co. Shell Global Solutions Exxon Mobil Petroleum ΒP ord Motor Co. Chevron U.S.A iat Chrysler Automobiles American Petroleum Institute Phillips 66 Co. iat Chrysler Automobiles Chevron Oronite Volkswagen of America ΒP Chevron Oronite - Statistics Intern General Motors Co. Foyota Technical Center General Motors Co.

VIII. Methodology

a. General Description

One objective of the program was to evaluate fuel octane effects on vehicle performance at 5,000 ft. versus 1,000 ft. elevations. Variable pressure vehicle chassis dynamometer emissions test cells were, therefore, required in order to prevent the need for individual vehicles to be tested at two separate chassis dynamometer labs for each elevation. Moving the vehicles to a second lab for 5,000 ft. tests would introduce lab-to-lab variation on the same vehicles into the results. To avoid this additional source of variation, the emissions testing of the nine vehicles was divided up among three automotive OEM test labs, with each vehicle remaining at a single lab. The vehicles were tested over a period nine months at Fiat Chrysler, Ford, and General Motors, as emissions test cells became available.

b. Test Vehicle Matrix – Summary

A summary of the nine test vehicles is found in Table 1 and a more complete list of vehicle characteristics is found in Appendix C. The owner's manuals for each of these vehicles require the use of minimum 87 AKI gasoline for satisfactory performance. The vehicles have been randomly assigned number codes throughout the remainder of the report which do not coincide with the order presented in Table 1.

| <u>Vehicle</u> | Model Year | <u>Odometer</u> | Fuel System | Induction System | Eng. Disp. (L) |
|-----------------------|------------|-----------------|-------------|------------------|----------------|
| <u>Toyota Corolla</u> | 2008 | 13,248 | PFI | Nat. Asp. | 1.8 |
| <u>Honda Odyssey</u> | 2008 | 13,248 | PFI | Nat. Asp. | 3.5 |
| <u>Honda Fit</u> | 2012 | 19,378 | PFI | Nat. Asp. | 1.5 |
| Ford Transit Connect | 2010 | 11,860 | PFI | Nat. Asp. | 2.0 |
| Ford Focus | 2008 | 12,563 | PFI | Nat. Asp. | 2.0 |
| Ford F-150 Ecoboost | 2011 | 5,200 | DI | Turbo | 3.5 |
| Ford F-150 | 2008 | 15,487 | PFI | Nat. Asp. | 5.4 |
| Dodge Dart | 2013 | 14,403 | PFI | Turbo | 1.4 |
| Chevy Equinox | 2010 | 37,396 | DI | Nat. Asp. | 3.0 |

| Table 1 | Test | Vehicle | Summary |
|---------|------|---------|---------|
|---------|------|---------|---------|

c. Standardized Vehicle Emissions Drive Cycles - General

In order to evaluate the effect of octane rating on vehicle performance over a range of consumer driving styles, three standardized emissions tests cycles were utilized to test each vehicle, fuel, and elevation combination.

There are several benefits of using emissions test cycles in evaluating fuel octane rating effects and / or vehicle octane response effects:

- 1) The OEM chassis dynamometer test labs are very familiar with running these cycles, helping to minimize test-to-test and lab-to-lab data variation.
- 2) For a given test cycle, the vehicles are all driven over an equivalent vehicle speed trace, which holds their demanded work output requirement constant, enabling vehicle and fuel effects comparisons.
- 3) Each test cycle contains multiple acceleration events (modes) with varying severities, which changes the vehicle octane requirement during each mode. Because the cycle modes will not change from test to test and vehicle to vehicle, fuel effects on vehicle performance comparisons can be made over a range of driver behaviors.

The three standardized emissions test cycles used for this study are found in Table 2.

Table 2 Standardized Vehicle Emissions Test Cycle Attributes

| Test Cycle | Average Vehicle Speed (mph) | Maximum Vehicle Speed (mph) | Test Cycle Distance (miles) |
|------------|--------------------------------|--------------------------------|--------------------------------|
| US FTP-75 | 21.2 | 56.7 | 11.04 |
| LA92 | 24.6 | 67.2 | 9.80 |
| US06 | 48.4 | 80.0 | 8.01 |

Another benefit of using well defined, well controlled, standardized emissions test cycles is the inclusion of Drive Quality Metrics defined in the SAE International J2951 Recommended Practice for Drive Quality evaluation. The following "Rationale, Foreword, and Scope" are quoted directly out of this Practice.

RATIONALE

To provide standardized metrics for evaluating drive quality on emissions and fuel economy tests. This document has been revised to include a new drive rating metric and typical driver capability ranges.

FOREWORD

It is generally recognized that the manner in which a vehicle is driven during a chassis dynamometer test can impact emissions and fuel economy results. The speed vs. time tolerances used to validate a test do limit this impact, but even within these constraints drive-related effects can be significant contributors to test variability. This document provides drive quality metrics intended to enable improved monitoring and characterization of driver-related variability.

SCOPE

This SAE Recommended Practice establishes uniform procedures for evaluating conformity between the actual and target drive speeds for chassis dynamometer testing utilizing standard fuel economy and emissions drive schedules.

The SAE J2951 RMSSE metric provides the driver's performance in meeting the schedule speed trace throughout the test cycle in terms of the Root Mean Squared (RMS) Speed Error. The value is always a positive number with lower values (closer to zero) indicating better performance. RMSSE has units of miles per hour (mph). Based on discussions with Emissions Lab personnel, it is typical for RMSSE to increase with driving cycle severity but should be kept below 1.0 for all vehicle emissions tests. Values greater than 1.0 indicate drivers having difficulty keeping up with the vehicle speed trace. Drivers "falling behind" the vehicle speed trace would need to increase throttle, which may momentarily impact in-cylinder air-to-fuel ratios and resultant emissions. The drive quality metrics for 2 of the 3 chassis dynamometer laboratories are summarized in Table 3 below.

| Average Root Mean Squared Speed Error (RMSSE) for Two of the Three Chassis Dyno Labs* | | | | | | |
|---|--|-------------|------|------|--|--|
| | ("N" (number of tests per average) is 14 or 15.) | | | | | |
| 85 AKI / 1000 ft. 85 AKI / 5,000 ft. 87 AKI / 1000 ft. 87 AKI / 5,00 | | | | | | |
| US FTP-75 | 0.44 | 0.47 | 0.45 | 0.43 | | |
| LA92 | 0.51 | 0.57 | 0.53 | 0.53 | | |
| US06 | 0.61 | 0.67 | 0.62 | 0.62 | | |
| (*) One lab wa | s upable to report their PN | ASSE values | | | | |

Table 3 SAE J2951 Drive Quality Metrics

*) One lab was unable to report their RMSSE values.

d. Data Capture Procedure – Description and Flow Chart

The core of the test program design plan consisted of 9 vehicles x 2 fuels x 2 elevations x 3 driving cycles x 2 repeats, which equates to 216 tests, minimally. Dynamometer cell temperatures were set to nominally 75°F

and relative humidity between 35 - 40%. Five of the vehicles began testing on the 87 AKI fuel and switched to the 85 AKI fuel and four vehicles began on the 85 AKI fuel and switched to 87 AKI. Figure 1 shows a flowchart of the test procedures for the core emissions program, which aided in keeping procedures the same between the three test laboratories. Frequent review of the emissions and performance test data occurred. Additional test repeats were conducted if the vehicle emission results were not precise and did not meet the following emissions test precision "rules of thumb": CO < 20% COV, CO2 < 1% COV, FE < + / - 0.3 mpg, where COV is the Coefficient of Variation and is defined as

$$COV = \frac{1\sigma}{\bar{x}} \times 100$$

where 1σ equals one standard deviation and \bar{x} is the average of individual observations for a given vehicle, octane, and altitude combination. Also, before the data capture team approved the data from each emissions cycle, each vehicle emissions data file was reviewed to verify the data was valid and that no test equipment or analyzer calibration errors occurred. In addition to the core emissions tests, bracket US FTP-75 duplicate emissions tests were conducted prior to the start of testing (SOT) and then again at the end of testing (EOT) with Tier 2 Federal emissions certification fuel. This was done to ensure that the vehicles showed no illuminated on-board diagnostic (OBD) malfunction lights and also to be able to compare the baseline tailpipe emissions of each vehicle to those of the reported federal emissions certification vehicles. No anomalies were found and the vehicles emissions data taken at the EOT then allowed an analysis of the vehicle emissions system response drift over the months of testing, and this is detailed later in the report. In total at the beginning of the program, 252 emissions tests were estimated to be needed and in the end 305 tests were conducted.



Figure 1 Vehicle Emissions Test Procedure Flow Chart-Core Program (85 and 87 AKI Tests)

e. Octane Test Fuels - Summary

Four independent fuel quality labs analyzed the two test fuels. The results are summarized below in Table 4. The full set of results for all labs is found in Appendix D. Care was given to meet the targeted respective 85 and 87 AKI octane ratings of the two fuels while minimizing differences in density, volatility, energy content and any other properties that may influence the combustion process and result in changes to engine efficiency and emissions. The two test fuels differ only in that a slight amount of zero octane rating n-heptane was added to the 87 AKI E10 blend. The unwashed gum values of fuels are indicative of the presence of detergents and do not impact the octane number effects.

| Test | Units | 85 AKI E10 | | | 87 AKI E10 | | |
|---------------------|--------------|-------------|-------------|-------------|---------------|-----------|--------|
| | | Average | Std | % CoV | Average | Std | % CoV |
| RON | | 87.9 | 0.4 | 0.5% | 90.7 | 0.3 | 0.4% |
| MON | | 82.0 | 0.3 | 0.4% | 83.9 | 0.6 | 0.7% |
| AKI | | 84.9 | 0.2 | 0.2% | 87.3 | 0.3 | 0.4% |
| Sensitivity | | 5.8 | 0.7 | 11.6% | 6.8 | 0.6 | 9.4% |
| | | | | | | | |
| Relative Density | S.G. 60/60F | 0.7360 | 0.0 | 0.1% | 0.7366 | 0.0 | 0.0% |
| | | | | | | | |
| DVPE | psi @ 100F | 8.39 | 0.2 | 2.1% | 8.71 | 0.1 | 1.7% |
| | | | | | | | |
| Distillation | deg. F | | | | | | |
| IBP | | 100.8 | 2.6 | 2.6% | 100.3 | 4.8 | 4.8% |
| T5 | | 126.8 | 1.4 | 1.1% | 124.3 | 1.7 | 1.3% |
| T10 | | 133.8 | 0.8 | 0.6% | 131.3 | 1.1 | 0.8% |
| T20 | | 143.0 | 0.7 | 0.5% | 141.0 | 0.4 | 0.3% |
| T30 | | 149.7 | 1.0 | 0.7% | 147.8 | 0.4 | 0.3% |
| T40 | | 162.4 | 2.7 | 1.6% | 154.3 | 0.9 | 0.6% |
| T50 | | 216.1 | 2.7 | 1.2% | 211.4 | 1.9 | 0.9% |
| T60 | | 240.4 | 0.9 | 0.4% | 242.6 | 1.4 | 0.6% |
| 170 | | 261.7 | 1.9 | 0.7% | 265.1 | 0.5 | 0.2% |
| T80 | | 286.1 | 1.8 | 0.6% | 286.7 | 1.0 | 0.4% |
| T90 | | 313.7 | 0.9 | 0.3% | 313.6 | 1.1 | 0.4% |
| T95 | | 336.5 | 4.6 | 1.4% | 337.0 | 4.2 | 1.3% |
| FBP | | 359.9 | 1.2 | 0.3% | 361.0 | 1.7 | 0.5% |
| Residue | | 1.0 | 0.0 | 0.0% | 1.1 | 0.1 | 9.5% |
| DI | | 1186.1 | 11.1 | 0.9% | 1168.5 | 6.0 | 0.5% |
| | 24 | | | 17 60/ | | | 44.00(|
| Aromatics | V% | 11.6 | 2.1 | 17.6% | 11.6 | 1.4 | 11.8% |
| Diefins | | 8.2 | 1.5 | 17.8% | 8.7 | 1.7 | 19.0% |
| Fthanol | | 70.3 | 3.9 | 5.0% | 69.7 10.1 | 3.5 | 5.0% |
| Ethanoi | | 9.9 | 0.6 | 0.3% | 10.1 | 0.7 | 0.9% |
| Sum | | | | | | | |
| Sulfur | nnm | 03 | | | 0.2 | | |
| Sultu | ppm | 0.3 | | | 0.2 | | |
| Carbon | wt% | 81.6 | 0.1 | 0.1% | 81.8 | 0.2 | 0.2% |
| Hydrogen | wt% | 14.5 | 0.1 | 0.3% | 14.4 | 0.2 | 1 1% |
| H/C Ratio | | 2.1 | 0.0 | 0.0% | 2.1 | 0.0 | 1.8% |
| , с нано | | | 0.0 | 0.070 | | 0.0 | 1.070 |
| NHV* | btu/lb | 18746.7 | 799.5 | 4.3% | 18730.4 | 849.4 | 4.5% |
| | | | | | | 2.3.1 | |
| Existent Gum | mg/100ml | | | | | | |
| - Unwashed | | 11.5 | 5.2 | 45.1% | 10.4 | 5.7 | 55.0% |
| - Washed | | 0.1 | 0.2 | 173.2% | 0.1 | 0.2 | 173.2% |
| | | - | - | | - | - | |
| (*) Note: | | | | | | | |
| Wide variation in N | IHV from two | labs. Chrys | sler re-ana | lyzed the 8 | 7 AKI test fu | el. NHV = | 41.52 |

| Table 4 Test Fuel Co | mposition and | Property Summary |
|----------------------|---------------|------------------|
|----------------------|---------------|------------------|

Wide variation in NHV from two labs. Chrysler re-analyzed the 87 AKI test fuel. NHV = 41.52 MJ/kg (17,894 BTU/lb). Used D240 test method. Lab 3 appears to have reported HHV, not NHV. Confirmed that each of the 3 OEM Emissions Sites used the Average NHV from this spreadsheet. FE numbers should not be compared to those reported to EPA (plus these are not Tier 2 Cert Fuels.)

IX. Data Summaries

a. Statistical Analysis Methodology

As previously mentioned, the core of the test program design plan consisted of 9 vehicles x 2 fuels x 2 elevations x 3 driving cycles x 2 repeats, which equates to 216 tests. Including additional repeats, 265 core emissions tests were conducted. US FTP-75 Tier 2 emissions tests were conducted before and after core testing for each vehicle to monitor vehicle response drift, Nominally, this would have included 9 vehicles x 2 times (before and after) x 2 repeats or 36 tests. As some vehicles had more than two repeat measurements and one vehicle had no post Tier 2 tests, the total number of US FTP-75 Tier 2 emissions tests was 40.

| Fuel | Altitude (ft.) | Test Cycle | Planned Tests |
|------------------|----------------|---------------|---------------|
| | | US FTP-75 | 2 |
| | 1000 | LA92 | 2 |
| | | US06 | 2 |
| 85 ANI | | US FTP-75 | 2 |
| | 5000 | LA92 | 2 |
| | | US06 | 2 |
| | | US FTP-75 | 2 |
| | 1000 | LA92 | 2 |
| | | US06 | 2 |
| 07 ANI | | US FTP-75 | 2 |
| | 5000 | LA92 | 2 |
| | | US06 | 2 |
| | | SOT US FTP-75 | 2 |
| Tier 2 Cert Fuel | Site Elevation | EOT US FTP-75 | 2 |

Table 5 Minimum Test Plan for each Vehicle

For the emissions data, the "usual" transformations were used as a first step in analyses. Emissions in grams per mile theoretically do not go below zero, have increased variability with increased grams per mile, and tend to be impacted multiplicatively rather than additively by both controlled and random factors. For this reason, CRC traditionally has found natural logarithmic transformation (transformed emission = natural logarithm of emission) to yield datasets that more closely satisfy assumptions involved in statistical analyses. Fuel economy in miles per gallon as measured in equal distance emissions tests are also traditionally inverted to gallons per mile for better analysis. This transformation generally yields datasets that more closely satisfy assumptions involved in statistical analyses and also puts the variable being estimated (fuel used) in the numerator rather than the fixed value (miles) which creates more reliable analyses.

For core emissions testing, repeat measurements for each of the 36 combinations of vehicle, fuel, and elevation were averaged after transformation.

The data analysis in this study uses linear models as implemented in SAS[®]. For example, for the core emissions analyses, model fits for the form transformed emissions = f(vehicle, altitude, fuel) + e where 'f' is linear function of the design factors and 'e' are residuals with the assumptions $\sum e_i = 0$, and $e \sim iid N(0, \sigma^2)$, that is the errors are distributed identically and independently as Normal or Gaussian random variables with mean

zero and variance, σ^2 . Significance tests are reported based on these linear models with α =0.05 unless otherwise stated.

Residuals were examined from each of the models to assess whether assumptions on the analyses were based upon could be assumed to be valid. Potential outliers were identified based on externally Studentized residuals. An externally Studentized residual is the difference between actual result and the value predicted by the fitted model divided by an estimate of standard deviation in the residuals from the model fitted without that result. As a rule of thumb, an observation was flagged as a potential outlier when the externally Studentized residual was greater than 3 or less than -3. This should occur purely by chance less than three times in a thousand. Note that flagging as a potential outlier is not proof the observation should be omitted from analyses, but only evidence the observation might have arisen from a process different from the rest of the data. Eliminating potential outliers is an engineering judgment. For the core program data analyses in this report, potential outliers were removed. Outlier analysis was not conducted on data from the Tier 2 bracket fuels for the analysis of drift. In most cases, data were analyzed with and without potential outliers to ensure that their removal did not lead to different conclusions.

b. Data Outlier Analysis

The flagged outlier rate among repeat measurements was considered to be a partial indication of data quality. The outlier flags indicate when results from combinations of factors did not fit the model as well as other combinations.

Of the 259 core <u>emissions</u> tests, 13 (or 5%) were flagged as potential repeatability outliers. The Data Analysis Panel removed these 13 tests before averaging within the 36 (9 vehicles x 2 fuels x 2 altitudes) combinations for each of the 3 test cycles. Of the 36 core emissions tests means only one potential outlier was flagged.

Of the 128 core <u>performance</u> tests, (8 vehicles x 2 fuels x 2 altitudes x 4 test cycles) 125 combinations had analyzable averages. Of these, five means (or 4%) were flagged as potential outliers and were excluded from the final presented analyses.

An example of the low FE vehicle drift response is shown in Figure 2 with additional figures and tables summarizing the drift response located in Appendix G. The vehicle response drift over the course of the program did not change the conclusions of the data.



Figure 2 Vehicle Fuel Economy Drift from SOT to EOT [US FTP-75 FE with Tier 2 Certification Fuel]

c. Description of General Statistical Analysis Approach

The individual test fleet vehicles differ in their engine hardware, emissions certification requirements, and ECM calibration anti-knock mitigation strategies resulting in a wide variation of vehicle performance as a result of octane number and elevation. To better understand how vehicle characteristic variation contributes to the precision of the findings, several statistical confidence analyses and trend analyses are presented for both the fleet averaged and individual vehicle results. Likewise, when interpreting the fuel, elevation, and driver style effects on vehicle performance, comparisons of test fleet averaged results versus individual vehicle results are shown to offer good contrast in understanding their magnitude and statistical significance.

d. Vehicle Emissions and Performance_Data

i. Initial Vehicle Fleet Fuel Economy / Fuel Consumption Linear Models and ANOVAs

For the reasons described in the Statistical Analysis Methodolgy section above the linear models were created using fuel consumption data (gal/mile), however througout the paper, the figures are then converted to Fuel Economy (gpm). (See Figure 3 and Table 6 below.)

For the report figures that include "whiskers", these confidence intervals indicate the comparison bars for 95% confidence level statistics. While comparing any of the means to another within a figure, overlapping bars indicate the differences in means are not statistically significant at an Alpha (p-value) of 0.05. Whiskers that don't overlap for any of the fleet means indicate significantly different means.

Figure 3 shows the fuel economy results from the fuel consumption linear models when the vehicle and elevation data are grouped together but when the three test cycles are kept separate to understand the

effects of octane number. The effects of the fuels are significantly different from each other for the LA92 and US06 test cycles and not the US FTP-75.



Figure 3 Fleet Averaged Fuel Economy (mpg)

Table 6 shows the ANOVAs generated for the three Fuel Consumption models (US FTP-75, LA92 and US06). The following observations may be drawn from the table:

- a. The R-squared terms for all three models are very high, i.e. greater than 0.99, and indicate a very good data fit and that the models can be used with confidence
- b. CRC Emissions programs use p-values magnitudes less than 0.05 to determine if two populations are significantly different at 95% confidence. P-values less than 0.05 are highlighted in yellow indicating a rejection of the null hypothesis. And, p-values between 0.05 and 0.10 are considered marginally significant differences at 90% confidence
- c. For each of the three models, the vehicle variable (VNumber) in the ANOVA shows the highest F-ratios indicating that the vehicle variation is the largest influence on the model by two orders of magnitude.
- d. The Altitude variable is significant for the US FTP-75 and LA92 models and marginally significant for the US06.
- e. The Fuel variable is marginally significant for the US FTP-75 model and significant for the LA92 and US06 models. The Fuel f-ratios show increasing contribution to the model as the test cycle severity increases.
- f. The interactive model term "Altitude*Fuel" is not significant for any of the three models.

| | Fuel Co | Fuel Consumption (gal / mile) | | | | |
|------------------|-----------|-------------------------------|--------------------------|---------------|-----------------|--|
| TestCycle=US FTP | | | | | | |
| | | | | | | |
| Source | DF | Sum of Squares | Mean Square | F Value | Pr > F | |
| Model | 11 | 0.00503781 | 0.00045798 | 4201.93 | <.0001 | |
| Error | 23 | 0.00000251 | 0.0000011 | | | |
| Corrected Total | 34 | 0.00504032 | | | | |
| | | | | | | |
| R-Square | Coeff Var | Root MSE | FC_Mean Mean | | | |
| 0.999503 | 0.779085 | 0.00033 | 0.042376 | | | |
| | | | | | | |
| Source | DF | Type III SS | Mean Square | F Value | Pr > F | |
| VNumber | 8 | 0.00502541 | 0.00062818 | 5763.44 | <.0001 | |
| Altitude | 1 | 0.00001365 | 0.00001365 | 125.21 | <.0001 | |
| Fuel | 1 | 0.0000031 | 0.0000031 | 2.81 | 0.1075 | |
| Altitude*Fuel | 1 | 0.0000001 | 0.0000001 | 0.06 | 0.804 | |
| | | | | | | |
| TestCycle=LA92 | | | | | | |
| Source | DF | Sum of Squares | Mean Square | F Value | Pr > F | |
| Model | 11 | 0.00483024 | 0.00043911 | 5236.61 | <.0001 | |
| Error | 23 | 0.00000193 | 0.0000008 | | | |
| Corrected Total | 34 | 0.00483217 | | | | |
| | | | | | | |
| R-Square | Coeff Var | Root MSE | FC_Mean Mean | | | |
| 0.999601 | 0.679044 | 0.00029 | 0.042645 | | | |
| | | | | | | |
| Source | DF | Type III SS | Mean Square | F Value | Pr > F | |
| VNumber | 8 | 0.00480765 | 0.00060096 | 7166.66 | <.0001 | |
| Altitude | 1 | 0.00000654 | 0.00000654 | 78.04 | <.0001 | |
| Fuel | 1 | 0.0000097 | 0.0000097 | 11.51 | 0.0025 | |
| Altitude*Fuel | 1 | 0.0000007 | 0.0000007 | 0.86 | 0.3635 | |
| TestCusie=USOC | | | | | | |
| resicycle=0506 | | | | | | |
| Source | DF | Sum of Squares | Mean Square | F Value | Pr > F | |
| Model | 11 | 0.0052596 | 0.00047815 | 1101.27 | <.0001 | |
| Error | 23 | 0.0000999 | 0.0000043 | | | |
| Corrected Total | 34 | 0.00526959 | | | | |
| | | | | | | |
| R-Square | Coeff Var | Root MSE | FC_Mean Mean | | | |
| 0.998105 | 1.476268 | 0.000659 | 0.044634 | | | |
| | | | | | | |
| Source | DF | Type III SS | Mean Square | F Value | Pr > F | |
| VNumber | 8 | 0.00524218 | 0.00065527 | 1509.23 | <.0001 | |
| | | | | | | |
| Altitude | 1 | 0.00000133 | 0.00000133 | 3.05 | 0.094 | |
| Altitude Fuel | 1 | 0.00000133 0.00000725 | 0.00000133 0.00000725 | 3.05 16.69 | 0.094 0.0005 | |

ii. Vehicle Fleet Fuel Economy and Emissions Means (Comparisons within an Elevation)

1. Fuel Economy (FE)

Figure 4 shows the fuel economy results for the same fuel consumption ANOVA found in Table 6 but this time the two elevations are separated out, which reduces the number of data points making up each average by half. The figure shows that for a given octane number, FE is always greater at 5,000 ft. than 1,000 ft. This is due to the atmospheric effects of operating a vehicle at the different elevations. The lower air density requires the engine control module's closed loop air-to-fuel ratio control to open the throttle wider than with more dense air, which in turn, reduces parasitic losses from engine pumping. In the field, a second reason for improved fuel economy at higher elevation is from a lower drag coefficient on a vehicle at higher elevation. This effect, however, was not taken into account during laboratory chassis dynamometer tests, and therefore, does not apply for this data set.

Figure 4 also starts to show the consistent pattern of higher fleet average FE for the 87 AKI relative to the 85 AKI fuel. When evaluated over the US FTP-75 cycle (the data points shown in blue in Figure 4), the confidence intervals around the mean 85 AKI and 87 AKI values overlap for both the 5,000 ft. and 1,000 ft. cases. The overlapping confidence intervals lead one to conclude that the population averages are not significantly different. If the population averages were truly equal however, then given enough measurements with the same variation half of the 85 AKI averages would be less than the 87 AKI ones, which is not the case. These persistent trends are analyzed further in the report sections below.



Figure 4 Nine Vehicle FE (mpg) Means with Confidence Intervals

2. Carbon Dioxide (CO₂)

Figure 5, shown below, describes information similar to that presented in the previous Fuel Economy section. This similarity is expected because CO_2 is the main component in calculating the FE of a vehicle. The difference, however, is the data trends in an opposite direction to FE. This is also expected because as a vehicle emits less CO_2 , the fuel economy improves.



Figure 5 Nine Vehicle CO2 (gpm) Mean with Confidence Intervals

| | | In CO2 (gpm) | | | |
|-----------------|-----------|---------------------------|-------------------|---------|--------|
| TestCycle=US FT | P | | | | |
| | | | | | |
| Source | DF | um of Squares Mean Square | | F Value | Pr > F |
| Model | 11 | 2.7807231 | 0.25279301 | 6390.72 | <.0001 |
| Error | 23 | 0.00090979 | 090979 0.00003956 | | |
| Corrected Total | 34 | 2.7816329 | | | |
| D.Causana | CooffMan | | la CO2 Maran M | | |
| K-Square | Coeff var | ROOLIVISE | ean | | |
| 0.999673 | 0.107889 | 0.006289 | 5.829492 | | |
| | | | | | |
| Source | DF | Type III SS | Mean Square | F Value | Pr > F |
| VNumber | 8 | 2.77432467 | 0.34679058 | 8767.02 | <.0001 |
| Altitude | 1 | 0.00805853 | 0.00805853 | 203.72 | <.0001 |
| Fuel | 1 | 0.00011831 | 0.00011831 | 2.99 | 0.0971 |
| Altitude*Fuel | 1 | 0.0000007 | 0.0000007 | 0 | 0.9663 |
| | | | | | |
| TestCycle=LA92 | | | | | |
| Source | DE | Sum of Saucres | Moon Sauara | E Value | Dr \ F |
| Source | UF 44 | 2 E2046244 | | | ri 2 F |
| Ividei | 11 | 2.53846311 | 0.23076937 | 4568.29 | <.0001 |
| Error | 23 | 0.00116186 | 0.00005052 | | |
| Corrected Total | 34 | 2.53962497 | | | |
| R-Square | Coeff Var | Root MSE | InCO2_Mean M | | |
| - | | | ean | | |
| 0.999543 | 0.121674 | 0.007107 | 5.841382 | | |
| | | | | | |
| Source | DF | Type III SS | Mean Square | F Value | Pr > F |
| VNumber | 8 | 2.52775791 | 0.31596974 | 6254.9 | <.0001 |
| Altitude | 1 | 0.00411583 | 0.00411583 | 81.48 | <.0001 |
| Fuel | 1 | 0.00025577 | 0.00025577 | 5.06 | 0.0343 |
| Altitude*Fuel | 1 | 0.00003324 | 0.00003324 | 0.66 | 0.4256 |
| | | | | | |
| lestCycle=US06 | | | | | |
| Source | DF | Sum of Squares | Mean Square | F Value | Pr > F |
| Model | 11 | 2.60301219 | 0.23663747 | 1470.29 | <.0001 |
| Error | 23 | 0.00370176 | 0.00016095 | | |
| Corrected Total | 34 | 2.60671395 | | | |
| | | | | | |
| R-Square | Coeff Var | Root MSE | InCO2_Mean M | | |
| | | | ean | | |
| 0.99858 | 0.215937 | 0.012686 | 5.875079 | | |
| | | | | | |
| Source | DF | Type III SS | Mean Square | F Value | Pr > F |
| VNumber | 8 | 2.59146987 | 0.32393373 | 2012.68 | <.0001 |
| Altitude | 1 | 0.00104176 | 0.00104176 | 6.47 | 0.0181 |
| Fuel | 1 | 0.00226597 | 0.00226597 | 14.08 | 0.001 |
| Altitude*Fuel | 1 | 0.00002139 | 0.00002139 | 0.13 | 0.7188 |

Table 7 CO₂ (gpm) Linear Models within an Elevation

3. Carbon Monoxide (CO)

Figure 6 shows the nine vehicle fleet averages for CO emissions. Similar to the Figures 4 and 5, Figure 6 shows a confidence interval plot for each test cycle, categorized by fuel octane rating and simulated test elevation. The amount of CO emitted increases as cycle severity also increases. At the most severe test cycle, US06, the fleet average emissions from operation on 85 AKI fuel are greater than those from the 87 AKI fuel, but the difference is only statistically significant for the 1,000 ft. elevation case.

Carbon monoxide emissions, however, are indicative of factors in addition to the fuel and elevation tested. These factors include OEM combustion strategy and driver behavior. The latter was mitigated as much as possible by limiting the number of different drivers who tested the vehicles, to a reasonable degree. The former should be a limited contributor to the overall fleet average because the vehicles originated from a bevy of manufacturers.



Figure 6 Nine Vehicle CO (gpm) Mean with Confidence Intervals

Table 8 CO (gpm) Linear Models within an Elevation

| | | In CO (gpm) | | | |
|--|---|---|--|---|--|
| TestCycle=US FT | Р | | | | |
| | | | | | |
| Source | DF | Sum of Squares | Mean Square | F Value | Pr > F |
| Model | 11 | 20.43993696 | 1.85817609 | 121.38 | <.0001 |
| Error | 24 | 0.36741644 | 0.01530902 | | |
| Corrected Total | 35 | 20.80735341 | | | |
| | | | | | |
| P Squaro | | | | | |
| N-Square | Coeff Var | Root MSE | nCO_Mean Mear | 1 | |
| 0.982342 | -9.5195 | 0.12373 | -1.29975 | | |
| | | | | | |
| Source | DF | Type III SS | Mean Square | F Value | Pr > F |
| VNumber | 8 | 20.41767317 | 2.55220915 | 166.71 | <.0001 |
| Altitude | 1 | 0.00387475 | 0.00387475 | 0.25 | 0.6195 |
| Fuel | 1 | 0.00087077 | 0.00087077 | 0.06 | 0.8135 |
| Altitude*Fuel | 1 | 0.01751828 | 0.01751828 | 1.14 | 0.2954 |
| | | | | | |
| TestCycle=LA92 | | | | | |
| | | | | | |
| Source | DF | Sum of Squares | Mean Square | F Value | Pr > F |
| Model | 11 | 41.61994505 | 3.78363137 | 91.58 | <.0001 |
| Error | 23 | 0.9501983 | 0.04131297 | | |
| Corrected Total | 34 | 42.57014335 | | | |
| | | | | | |
| | | | | | |
| P. Couloro | | | | | |
| R-Square | Coeff Var | Root MSE | nCO_Mean Mear | ı | |
| R-Square 0.977679 | Coeff Var -12.9257 | Root MSE 0.203256 | n CO_Mean Mea r -1.572496 | 1 | |
| R-Square 0.977679 | Coeff Var -12.9257 | Root MSE 0.203256 | nCO_Mean Mear -1.572496 |) | |
| R-Square 0.977679 Source | Coeff Var -12.9257 DF | Root MSE 0.203256 Type III SS | nCO_Mean Mear -1.572496 Mean Square | r Value | Pr > F |
| R-Square 0.977679 Source VNumber | Coeff Var -12.9257 DF 8 | Root MSE 0.203256 Type III SS 41.24618049 | nCO_Mean Mear -1.572496 Mean Square 5.15577256 | F Value 124.8 | Pr > F <.0001 |
| R-Square 0.977679 Source VNumber Altitude | Coeff Var -12.9257 DF 8 1 | Root MSE 0.203256 Type III SS 41.24618049 0.24275267 | nCO_Mean Mear -1.572496 Mean Square 5.15577256 0.24275267 | F Value 124.8 5.88 | Pr > F <.0001 0.0236 |
| R-Square 0.977679 Source VNumber Altitude Fuel | Coeff Var -12.9257 DF 8 1 1 | Root MSE 0.203256 Type III SS 41.24618049 0.24275267 0.06399254 | nCO_Mean Mear -1.572496 Mean Square 5.15577256 0.24275267 0.06399254 | F Value 124.8 5.88 1.55 | Pr > F <.0001 0.0236 0.2258 |
| R-Square 0.977679 Source VNumber Altitude Fuel Altitude*Fuel | Coeff Var -12.9257 DF 8 1 1 1 | Root MSE 0.203256 Type III SS 41.24618049 0.24275267 0.06399254 0.02854297 | nCO_Mean Mear -1.572496 Mean Square 5.15577256 0.24275267 0.06399254 0.02854297 | F Value 124.8 5.88 1.55 0.69 | Pr > F <.0001 0.0236 0.2258 0.4144 |
| R-Square 0.977679 Source VNumber Altitude Fuel Altitude*Fuel | Coeff Var -12.9257 DF 8 1 1 1 1 | Root MSE 0.203256 Type III SS 41.24618049 0.24275267 0.06399254 0.02854297 | nCO_Mean Mear -1.572496 Mean Square 5.15577256 0.24275267 0.06399254 0.02854297 | F Value 124.8 5.88 1.55 0.69 | Pr > F <.0001 0.0236 0.2258 0.4144 |
| R-Square 0.977679 Source VNumber Altitude Fuel Altitude*Fuel TestCycle=US06 | Coeff Var -12.9257 DF 8 1 1 1 1 | Root MSE 0.203256 Type III SS 41.24618049 0.24275267 0.06399254 0.02854297 | nCO_Mean Mear -1.572496 Mean Square 5.15577256 0.24275267 0.06399254 0.02854297 | F Value 124.8 5.88 1.55 0.69 | Pr > F <.00010.02360.22580.4144 |
| R-Square 0.977679 Source VNumber Altitude Fuel Altitude*Fuel TestCycle=US06 | Coeff Var -12.9257 DF 8 1 1 1 1 | Root MSE 0.203256 Type III SS 41.24618049 0.24275267 0.06399254 0.02854297 | nCO_Mean Mear -1.572496 Mean Square 5.15577256 0.24275267 0.06399254 0.02854297 | F Value 124.8 5.88 1.55 0.69 | Pr > F <.00010.02360.22580.4144 |
| R-Square 0.977679 Source VNumber Altitude Fuel Altitude*Fuel TestCycle=US06 Source | Coeff Var -12.9257 DF 8 1 1 1 1 1 0 1 0 F | Root MSE 0.203256 Type III SS 41.24618049 0.24275267 0.06399254 0.02854297 | nCO_Mean Mear -1.572496 Mean Square 5.15577256 0.24275267 0.06399254 0.02854297 Mean Square | F Value 124.8 5.88 1.55 0.69 F Value | Pr > F <.0001 0.0236 0.2258 0.4144 Pr > F |
| R-Square 0.977679 Source VNumber Altitude Fuel Altitude*Fuel TestCycle=US06 Source Model | Coeff Var -12.9257 DF 8 1 1 1 1 1 2 0 F 11 | Root MSE 0.203256 Type III SS 41.24618049 0.24275267 0.06399254 0.02854297 Sum of Squares 35.59741153 | nCO_Mean Mear -1.572496 Mean Square 5.15577256 0.24275267 0.06399254 0.02854297 Mean Square 3.23612832 | F Value 124.8 5.88 1.55 0.69 F Value 47.14 | Pr > F <.0001 0.0236 0.2258 0.4144 Pr > F <.0001 |
| R-Square 0.977679 Source VNumber Altitude Fuel Altitude*Fuel TestCycle=US06 Source Model Error | Coeff Var -12.9257 DF 8 1 1 1 1 0 DF 11 23 | Root MSE 0.203256 Type III SS 41.24618049 0.24275267 0.06399254 0.02854297 0.02854297 Sum of Squares 35.59741153 1.57882969 | nCO_Mean Mear -1.572496 Mean Square 5.15577256 0.24275267 0.06399254 0.02854297 Mean Square 3.23612832 0.06864477 | F Value 124.8 5.88 1.55 0.69 F Value 47.14 | Pr > F <.0001 0.0236 0.2258 0.4144 Pr > F <.0001 |
| R-Square 0.977679 Source VNumber Altitude Fuel Altitude*Fuel TestCycle=US06 Source Model Error Corrected Total | Coeff Var -12.9257 DF 8 1 1 1 0 DF 11 23 34 | Root MSE 0.203256 Type III SS 41.24618049 0.24275267 0.06399254 0.02854297 0.02854297 Sum of Squares 35.59741153 1.57882969 37.17624123 | nCO_Mean Mear -1.572496 Mean Square 5.15577256 0.24275267 0.06399254 0.02854297 Mean Square 3.23612832 0.06864477 | F Value 124.8 5.88 1.55 0.69 F Value 47.14 | Pr > F <.0001 0.0236 0.2258 0.4144 Pr > F <.0001 |
| R-Square 0.977679 Source VNumber Altitude Fuel Altitude*Fuel TestCycle=US06 Source Model Error Corrected Total | Coeff Var -12.9257 DF 8 1 1 1 0 DF 11 23 34 | Root MSE 0.203256 Type III SS 41.24618049 0.24275267 0.06399254 0.02854297 Sum of Squares 35.59741153 1.57882969 37.17624123 | nCO_Mean Mear -1.572496 Mean Square 5.15577256 0.24275267 0.06399254 0.02854297 Mean Square 3.23612832 0.06864477 | F Value 124.8 5.88 1.55 0.69 F Value 47.14 | Pr > F <.0001 0.0236 0.2258 0.4144 Pr > F <.0001 |
| R-Square 0.977679 Source VNumber Altitude Fuel Altitude*Fuel TestCycle=US06 Source Model Error Corrected Total R-Square | Coeff Var -12.9257 DF 8 1 1 1 0 DF 11 23 34 | Root MSE 0.203256 Type III SS 41.24618049 0.24275267 0.06399254 0.02854297 | nCO_Mean Mear -1.572496 Mean Square 5.15577256 0.24275267 0.06399254 0.02854297 Mean Square 3.23612832 0.06864477 | F Value 124.8 5.88 1.55 0.69 F Value 47.14 | Pr > F <.0001 0.0236 0.2258 0.4144 Pr > F <.0001 |
| R-Square 0.977679 Source VNumber Altitude Fuel Altitude*Fuel TestCycle=US06 Source Model Error Corrected Total R-Square | Coeff Var -12.9257 DF 8 1 1 1 0 DF 11 23 34 Coeff Var | Root MSE 0.203256 Type III SS 41.24618049 0.24275267 0.06399254 0.02854297 0.02854297 Sum of Squares 35.59741153 1.57882969 37.17624123 | nCO_Mean Mear -1.572496 Mean Square 5.15577256 0.24275267 0.06399254 0.02854297 Mean Square 3.23612832 0.06864477 nCO_Mean Mear | F Value 124.8 5.88 1.55 0.69 F Value 47.14 | Pr > F <.0001 0.0236 0.2258 0.4144 Pr > F <.0001 |
| R-Square 0.977679 Source VNumber Altitude Fuel Altitude*Fuel TestCycle=US06 Source Model Error Corrected Total R-Square 0.957531 | Coeff Var -12.9257 DF 8 1 1 1 1 0 DF 11 23 34 Coeff Var 56.44325 | Root MSE 0.203256 Type III SS 41.24618049 0.24275267 0.06399254 0.02854297 Sum of Squares 35.59741153 1.57882969 37.17624123 Root MSE 0.262001 | nCO_Mean Mear -1.572496 Mean Square 5.15577256 0.24275267 0.06399254 0.02854297 Mean Square 3.23612832 0.06864477 nCO_Mean Mear 0.464186 | F Value 124.8 5.88 1.55 0.69 F Value 47.14 | Pr > F <.0001 0.0236 0.2258 0.4144 Pr > F <.0001 |
| R-Square 0.977679 Source VNumber Altitude Fuel Altitude*Fuel TestCycle=US06 Source Model Error Corrected Total R-Square 0.957531 | Coeff Var -12.9257 DF 8 1 1 1 1 0 DF 11 23 34 Coeff Var 56.44325 | Root MSE 0.203256 Type III SS 41.24618049 0.24275267 0.06399254 0.02854297 Sum of Squares 35.59741153 1.57882969 37.17624123 Root MSE 0.262001 | nCO_Mean Mear -1.572496 Mean Square 5.15577256 0.24275267 0.06399254 0.02854297 Mean Square 3.23612832 0.06864477 nCO_Mean Mear 0.464186 | F Value 124.8 5.88 1.55 0.69 F Value 47.14 | Pr > F <.0001 0.0236 0.2258 0.4144 Pr > F <.0001 |
| R-Square 0.977679 Source VNumber Altitude Fuel Altitude*Fuel TestCycle=US06 Source Model Error Corrected Total R-Square 0.957531 | Coeff Var -12.9257 DF 8 1 1 1 1 0 DF 11 23 34 Coeff Var 56.44325 DF | Root MSE 0.203256 Type III SS 41.24618049 0.24275267 0.06399254 0.02854297 Sum of Squares 35.59741153 1.57882969 37.17624123 Root MSE 0.262001 | nCO_Mean Mear -1.572496 Mean Square 5.15577256 0.24275267 0.06399254 0.02854297 Mean Square 3.23612832 0.06864477 nCO_Mean Mear 0.464186 Mean Square | F Value 124.8 5.88 1.55 0.69 F Value 47.14 | Pr > F <.0001 0.0236 0.2258 0.4144 Pr > F <.0001 |
| R-Square 0.977679 Source VNumber Altitude Fuel Altitude*Fuel TestCycle=US06 Source Model Error Corrected Total R-Square 0.957531 | Coeff Var -12.9257 DF 8 1 1 1 0 DF 11 23 34 Coeff Var 56.44325 DF 8 | Root MSE 0.203256 41.24618049 0.24275267 0.06399254 0.02854297 3.002854297 3.1.57882969 3.7.17624123 Root MSE 0.262001 Type III SS 3.3.31124261 | nCO_Mean Mear -1.572496 Mean Square 5.15577256 0.24275267 0.06399254 0.02854297 Mean Square 3.23612832 0.06864477 nCO_Mean Mear 0.464186 Mean Square 4.16390533 | F Value 124.8 5.88 1.55 0.69 F Value 47.14 | Pr > F <.0001 0.0236 0.4144 Pr > F <.0001 |
| R-Square 0.977679 Source VNumber Altitude Fuel Altitude*Fuel TestCycle=US06 Source Model Error Corrected Total R-Square 0.957531 Source VNumber Altitude | Coeff Var -12.9257 DF 8 1 1 1 1 0 DF 11 23 34 Coeff Var 56.44325 DF 8 1 0 F 8 1 | Root MSE 0.203256 7ype III SS 41.24618049 0.24275267 0.06399254 0.02854297 30.02854297 Sum of Squares 35.59741153 1.57882969 37.17624123 Root MSE 0.262001 Type III SS 33.31124261 0.36545529 | nCO_Mean Mear -1.572496 Mean Square 5.15577256 0.24275267 0.06399254 0.02854297 Mean Square 3.23612832 0.06864477 nCO_Mean Mear 0.464186 Mean Square 4.16390533 0.36545529 | F Value 124.8 5.88 1.55 0.69 F Value 47.14 | Pr > F <.0001 0.0236 0.2258 0.4144 Pr > F <.0001 Pr > F <.0001 0.0304 |
| R-Square 0.977679 Source VNumber Altitude Fuel Altitude*Fuel TestCycle=US06 Source Model Error Corrected Total R-Square 0.957531 Source VNumber Altitude Fuel | Coeff Var -12.9257 DF 8 1 1 1 1 2 0 DF 11 23 34 Coeff Var 56.44325 DF 8 1 1 1 1 1 1 1 1 1 1 1 1 1 | Root MSE 0.203256 7ype III SS 41.24618049 0.24275267 0.06399254 0.02854297 30.02854297 Sum of Squares 35.59741153 1.57882969 37.17624123 Root MSE 0.262001 Type III SS 33.31124261 0.36545529 0.87429692 | nCO_Mean Mear -1.572496 Mean Square 5.15577256 0.24275267 0.06399254 0.02854297 Mean Square 3.23612832 0.06864477 nCO_Mean Mear 0.464186 Mean Square 4.16390533 0.36545529 0.87429692 | F Value 124.8 5.88 1.55 0.69 F Value 47.14 47.14 | Pr > F <.0001 0.0236 0.2258 0.4144 Pr > F <.0001 Pr > F <.0001 0.0304 0.0016 |

iii. Percent Change in Nine Vehicle Fleet Means for FE and Emissions

1. Fuel Economy

The nine vehicle fuel economy means for each of the three test cycles at each elevation are shown in Table 9 along with the deltas between the two means. Table 9 also shows the p-value showing whether the two means are significantly different and the percent change in moving from 87 to 85 AKI test fuels. P-values less than 0.05 are highlighted in yellow.

Table 9 shows that the FE fleet means for the 85 AKI gasoline are all trending lower than the 87 AKI fuel within an elevation comparison, however the p-values are greater than 0.05 except for the LA92 and US06 test cycles for the 1,000 ft. case.

| FE (mpg) | | | | | | | | | | |
|------------------|---------|---------|---------|---------|----------|---------|---------|---------|---------|----------|
| Outliers Removed | 5000 | 5000 | p-value | Delta | % Change | 1000 | 1000 | p-value | Delta | % Change |
| | 85 AKI | 87 AKI | | 85 - 87 | 87> 85 | 85 AKI | 87 AKI | | 85 - 87 | 87> 85 |
| FTP-75 | 23.8775 | 23.9691 | 0.7353 | -0.0916 | -0.4% | 23.1667 | 23.2834 | 0.5507 | -0.1167 | -0.5% |
| LA92 | 23.3837 | 23.5172 | 0.3083 | -0.1335 | -0.6% | 22.8694 | 23.0942 | 0.0306 | -0.2248 | -1.0% |
| US06 | 22.5226 | 22.9002 | 0.1144 | -0.3776 | -1.6% | 22.2344 | 22.7917 | 0.0122 | -0.5573 | -2.4% |

Table 9 Fuel Economy – Nine Vehicle Fleet Means, Deltas, Percent Change, and p-values

Figure 8 shows that the impact of operating the test fleet on 85 AKI fuel relative to 87 AKI fuel for FE becomes more significant (smaller p-value) as the driving cycle becomes more demanding from the US FTP-75-type driving and through to the more aggressive US06.



Figure 7 Fuel Economy p-Values with Respect to Emissions Test Cycle

Figure 9 shows the fleet average percent change in fuel economy moving from 87 to 85 AKI fuel with respect to the average vehicle speed for the emissions cycles tested.


Figure 8 Average Percent Change in FE with Respect to Emissions Test Cycle Average Speed

2. Carbon Dioxide

For the remaining tailpipe emissions and performance parameter summary tables that follow, an additional light gray shading is used to show p-values between 0.05 and 0.10, while yellow continues to show p < 0.05 effects.

| CO2 (gpm) | | | | | | | | | | |
|------------------|----------|----------|---------|---------|----------|----------|----------|---------|---------|----------|
| Outliers Removed | 5000 | 5000 | p-value | Delta | % Change | 1000 | 1000 | p-value | Delta | % Change |
| | 85 AKI | 87 AKI | | 85 - 87 | 87> 85 | 85 AKI | 87 AKI | | 85 - 87 | 87> 85 |
| FTP-75 | 336.3948 | 335.1829 | 0.6225 | 1.2119 | 0.4% | 346.8585 | 345.5458 | 0.6155 | 1.3127 | 0.4% |
| LA92 | 344.5251 | 343.3285 | 0.7290 | 1.1966 | 0.3% | 352.8187 | 350.2167 | 0.1758 | 2.6020 | 0.7% |
| US06 | 353.3398 | 348.2110 | 0.0965 | 5.1288 | 1.5% | 357.8025 | 351.5022 | 0.0415 | 6.3003 | 1.8% |

Table 10 Carbon Dioxide – Nine Vehicle Fleet Means, Deltas, Percent Change, and p-values



Figure 9 Average Percent Change in CO₂ with Respect to Emissions Test Cycle Average Speed

3. Carbon Monoxide

The nine vehicle carbon monoxide (CO) means for each of the three test cycles at each elevation are shown in Table 11 along with the deltas between the two means and p-values. CO is an internal combustion engine partial oxidation species resulting from incomplete combustion. Combustion auto-ignition (knock) is a potentially engine damaging phenomena that is often managed by in-cylinder fuel enrichment, which leads to increased CO emissions and lower FE. Table 11 shows large percent changes in CO for the average fleet when operating on 85 versus 87 AKI test fuels as the test cycles become more knock limited.

| CO (gpm) | | | | | | | | | | |
|------------------|--------|--------|---------|---------|----------|--------|--------|---------|---------|----------|
| Outliers Removed | 5000 | 5000 | p-value | Delta | % Change | 1000 | 1000 | p-value | Delta | % Change |
| | 85 AKI | 87 AKI | | 85 - 87 | 87> 85 | 85 AKI | 87 AKI | | 85 - 87 | 87> 85 |
| FTP-75 | 0.2802 | 0.2708 | 0.9348 | 0.0094 | 3.5% | 0.2626 | 0.2772 | 0.7918 | -0.0146 | -5.3% |
| LA92 | 0.2314 | 0.2249 | 0.9905 | 0.0065 | 2.9% | 0.2073 | 0.1796 | 0.4888 | 0.0277 | 15.4% |
| US06 | 1.8881 | 1.5199 | 0.3359 | 0.3682 | 24.2% | 1.7008 | 1.1183 | 0.0124 | 0.5825 | 52.1% |

Table 11 Carbon Monoxide – Nine Vehicle Fleet Means, Deltas, Percent Change, and p-values



Figure 10 Average Percent Change in CO with Respect to Emissions Test Cycle Average Speed

iv. Fuel Economy and Emissions Averages for Individual Vehicles

Individual vehicle averages for FE, CO2, and CO are shown in this section and are the average of at least two and often three tests.

1. Fuel Economy

Figure 12 shows the average fuel economy (FE) results for each of the nine vehicles for the two test fuels, two elevations, and three emissions test cycles. In absolute numbers, the vehicle test fleet FE covered a large range from approximately 16 to 38 mpg depending on type of vehicle, test conditions and fuel octane level. The FE of the US06 results is generally lower than the US FTP-75 and LA92 primarily as a result of higher vehicle loading as well as being a more knock limited test cycle where fuel enrichment is used to mitigate knock.



Figure 11 Individual Vehicle Average Fuel Economy

2. Fuel Consumption – Vehicle Fuel Consumption Changes for 85 and 87 AKI Fuels The Engine Control Module (ECM) calibration strategies used by vehicle manufacturers vary greatly with respect to managing the effects of autoignition and protecting engine hardware. Consequently, the effect of using 85 AKI gasoline in a vehicle calibrated for 87 AKI is likely to differ across different vehicle makes and models. In order to understand the statistical significance of the individual vehicle FE differences measured in this test program, a heuristic significance test for each vehicle was developed using an estimate of repeatability.

Figures 13, 15, and 17 include intervals showing a heuristic indication of whether the change from 87 to 85 AKI gasoline was significant for each vehicle. Throughout the test program, the test vehicles were first fueled, conditioned, and tested with the specified octane test fuel at the appropriate simulated altitude. Then two or more back-to-back sets of tests were run on the vehicle before changing fuel and repeating the vehicle conditioning. (See Figure 1.) While this "back-to-back" test repeat sequence was needed to conduct the large number of tests in a reasonable amount of time and volume of test fuel available, the test repeats did not truly alternate between 85 and 87 AKI for the individual test observations. Due to the lack of true replication in this study, a rigorous test of individual vehicle response to the fuel AKI difference could not be performed. However for the purpose of this heuristic exercise, analyses were conducted as if the back-to-back tests were replicates and recognize that resultant estimate of residual error for comparisons is biased low due to correlation among back-to-back tests. A simple repeatability type comparison was used for each vehicle without accounting for multiple comparisons. The risk of concluding a significant difference if it were truly by chance is actually greater than the nominal 5% for which these intervals were calculated. With all these caveats, the interpretation for Figures 13, 15, and 17 is that when the interval does not cross zero for the deltas or one for the ratios, there is purported significant evidence of a difference for that individual vehicle.

Figure 13 shows the change in fuel consumption per 100 miles for each vehicle when fueled with 85 versus 87 AKI gasoline for the three test cycles at 5,000 and 1,000 ft. simulated altitudes. Most of the vehicle fuel consumption averages were higher with 85 AKI however their heuristic confidence intervals include the zero point indicating no statistical difference from zero. The deltas between 85 and 87 AKI increase as the test cycle becomes more demanding.



Figure 12 Individual Vehicle Fuel Consumption Deltas (85 AKI - 87 AKI gallons / 100 miles)

Investigating the trends of the averages in Figure 13, if AKI had no consistent effect on fuel economy, each of the deltas would have a 50% chance of being positive and a 50% chance of being negative. For a given altitude, of the 27 percent changes (nine vehicles times three test cycles), 22 were negative or had poorer FE on 85 AKI test fuel. The chance of flipping a fair coin 27 times and getting 22 or more tails is 0.0008. This is a p-value for the one-sided test of whether 85 versus 87 AKI gasoline had significantly lower fuel economy across the nine vehicles and three test cycles at either 5000 or 1000 foot simulated altitude. While binominal trend analyses may be useful in identifying directional trends, they do not take into account the magnitude or statistical significance of the measured differences.

Table 12 below summarizes the binomial probabilities for FE, CO, and CO2. The table shows the probability of the majority of percent deltas resulting in poorer CO_2 and CO emissions and FE while operating on 85 AKI gasoline relative to 87 AKI gasoline at both elevations tested and across all three test cycles arising purely by chance is very low.

| | / 3 | | I | | | | | |
|---|---|----|---------|--|--|--|--|--|
| One-sided p-value for x out of 27 deltas (9 vehicles x 3 test cycles) | | | | | | | | |
| with worse performance for | with worse performance for 85 AKI (positive for emissions, negative | | | | | | | |
| for | fuel economy |) | | | | | | |
| Measure | Altitude | х | p-value | | | | | |
| CO | 1000 | 17 | 0.12 | | | | | |
| CO ₂ | 1000 | 19 | 0.03 | | | | | |
| Fuel Economy | 1000 | 22 | 0.00 | | | | | |
| CO | 5000 | 18 | 0.06 | | | | | |
| CO ₂ | 5000 | 20 | 0.02 | | | | | |
| Fuel Economy | 5000 | 22 | 0.00 | | | | | |

Table 12 P-Value Summary for Individual Vehicle Response

Table 13 Average Vehicle Fuel Economy Change when moving from 87 to 85 AKI Fuel

| | | Fuel Economy Change (%) | | | | | | |
|---------|----------|-------------------------|--------------|-------|--|--|--|--|
| | Altitude | | 87 to 85 AKI | | | | | |
| VNumber | (ft.) | US FTP | LA92 | US06 | | | | |
| 1 | 5000 | -1.06 | -0.92 | -0.67 | | | | |
| 2 | 5000 | -0.07 | -0.24 | -2.03 | | | | |
| 3 | 5000 | -0.55 | 0.02 | -0.11 | | | | |
| 4 | 5000 | -1.51 | -0.40 | -0.40 | | | | |
| 5 | 5000 | 0.41 | -1.49 | -3.48 | | | | |
| 6 | 5000 | -1.73 | -0.43 | -2.44 | | | | |
| 7 | 5000 | 0.26 | -0.85 | -0.70 | | | | |
| 8 | 5000 | -0.75 | 0.37 | -2.38 | | | | |
| 9 | 5000 | 0.39 | -0.75 | -1.70 | | | | |
| 1 | 1000 | -0.15 | -1.40 | -3.32 | | | | |
| 2 | 1000 | -0.62 | -0.47 | -1.55 | | | | |
| 3 | 1000 | 0.14 | -1.22 | 6.75 | | | | |
| 4 | 1000 | 2.40 | -0.06 | -0.14 | | | | |
| 5 | 1000 | 0.74 | -4.26 | -2.60 | | | | |
| 6 | 1000 | -0.88 | -0.89 | -2.72 | | | | |
| 7 | 1000 | -1.45 | -1.56 | -1.96 | | | | |
| 8 | 1000 | 0.01 | -0.04 | -2.62 | | | | |
| 9 | 1000 | -0.83 | -2.34 | -4.60 | | | | |

3. Carbon Dioxide – Absolute Values

Carbon dioxide (CO_2) is the primary exhaust constituent impacting the calculation of a vehicle's fuel economy using the carbon balance methodology. Detailed information on the carbon balance procedure for measuring fuel consumption as it relates to the carbon products of a vehicle's exhaust can be found in the Code of Federal Register, 40 CFR Part 600. In practice, because vehicle exhaust CO_2 is generally three orders of magnitude higher in concentration than the other carbon constituents, it is highly inversely proportional to FE. Each vehicle's average CO_2 emission rates are shown in Figure 14 and ranged approximately from 220 to 525 g/mile.



Figure 13 Individual Vehicle Average CO2 Emissions

4. Carbon Dioxide – Change when moving from 87 to 85 AKI

In order to help visualize the effects octane level, test cycle, and elevation on CO_2 , Figure 15 shows the average change in CO_2 for each vehicle when fueled with 85 versus 87 AKI gasoline. Within an elevation, CO_2 was generally higher while operating on 85 AKI test fuel and the difference increased with test cycle severity, i.e. more differences were higher as the test cycle became more demanding or more spark knock limited. See Table 12 above for the probability of this occurring and its statistical significance.



Figure 14 Individual Vehicle CO2 Ratio (85 AKI gpm / 87 AKI gpm)

| r | | | | | | |
|---------|----------|---|-------|-------|--|--|
| | Altitude | CO ₂ Change (%) 87 to 85 AKI | | | | |
| VNumber | (ft.) | US FTP | LA92 | US06 | | |
| 1 | 5000 | 0.98 | 0.89 | 0.41 | | |
| 2 | 5000 | 0.00 | 0.22 | 1.34 | | |
| 3 | 5000 | 0.45 | -0.10 | 2.70 | | |
| 4 | 5000 | 1.18 | 0.02 | -0.06 | | |
| 5 | 5000 | -0.78 | 1.04 | 2.79 | | |
| 6 | 5000 | 1.86 | 0.56 | 1.97 | | |
| 7 | 5000 | -0.32 | 0.65 | 0.61 | | |
| 8 | 5000 | 0.46 | -0.76 | 1.88 | | |
| 9 | 5000 | -0.53 | 0.64 | 1.65 | | |
| 1 | 1000 | 0.03 | 1.22 | 2.62 | | |
| 2 | 1000 | 0.55 | 0.40 | 1.08 | | |
| 3 | 1000 | -0.23 | 1.15 | -6.62 | | |
| 4 | 1000 | -2.71 | -0.33 | -0.27 | | |
| 5 | 1000 | -1.11 | 4.01 | 2.24 | | |
| 6 | 1000 | 1.02 | 0.85 | 1.68 | | |
| 7 | 1000 | 1.40 | 1.42 | 1.79 | | |
| 8 | 1000 | -0.33 | -0.39 | 1.75 | | |
| 9 | 1000 | 0.80 | 2.32 | 4.36 | | |

| Table 14 Average Vehicle | CO2 Percent Change whe | n movina from 87 t | o 85 AKI Fuel |
|--------------------------|---------------------------|--------------------------|----------------|
| TUDIE 14 AVELAGE VEHICIE | : CO2 rencent chunge when | 1 1110villy ji 0111 07 t | 0 05 ANT 1 461 |

5. Carbon Monoxide – Absolute Values

The individual vehicle carbon monoxide (CO) averages for each of the three test cycles and each elevation are shown in Figure 16. CO is an internal combustion engine partial oxidation species resulting from incomplete combustion. For a warmed-up engine and exhaust system CO generally occurs during times of in-cylinder enrichment and for a cold engine CO generally occurs during the initial rich warm-up operation of the engine and prior to catalyst light-off, although more and more vehicles are utilizing stoichiometric starts and fast light off systems. Abnormal combustion auto-ignition (knock) is a potentially engine damaging phenomena occurring in a fully warmed up engine that is often managed by in-cylinder fuel enrichment and leads to increased CO emissions and lower FE. Figure 16 shows one vehicle in the test fleet consistently demonstrated higher tailpipe CO levels than the others and the nine test vehicle CO values ranged from 0.10 to 10 g/mile. CO emissions rates were highest during the US06 knock limited test cycle.



Figure 15 Individual Vehicle Average CO Emissions





Figure 16 Individual Vehicle CO Ratio (85 AKI gpm / 87 AKI gpm)

| | Altitude | CO Change (%) 87 to 85 AKI | | | | |
|---------|----------|----------------------------|--------|-------|--|--|
| VNumber | (ft.) | US FTP | LA92 | US06 | | |
| 1 | 5000 | 11.64 | -30.56 | 64.74 | | |
| 2 | 5000 | -13.71 | -16.59 | 94.27 | | |
| 3 | 5000 | 15.94 | -12.96 | 63.39 | | |
| 4 | 5000 | -8.57 | -5.12 | 14.88 | | |
| 5 | 5000 | 14.18 | 39.26 | 51.14 | | |
| 6 | 5000 | 8.30 | -9.62 | 97.53 | | |
| 7 | 5000 | -1.37 | 42.59 | 18.69 | | |
| 8 | 5000 | -4.46 | 42.06 | 20.08 | | |
| 9 | 5000 | 14.43 | 6.06 | 70.38 | | |
| 1 | 1000 | 18.34 | 139.51 | 64.74 | | |
| 2 | 1000 | -12.08 | -10.18 | 94.27 | | |
| 3 | 1000 | -20.35 | -22.15 | 63.39 | | |
| 4 | 1000 | -6.71 | -2.65 | 14.88 | | |
| 5 | 1000 | 14.90 | 36.24 | 51.14 | | |
| 6 | 1000 | -3.90 | 3.95 | 97.53 | | |
| 7 | 1000 | -5.56 | 30.42 | 18.69 | | |
| 8 | 1000 | -10.86 | 206.38 | 20.08 | | |
| 9 | 1000 | -14.38 | 2.41 | 70.38 | | |

| Table 15 Average Vehicle CO Percent | : Change when | moving from 8 | 87 to 85 AKI Fuel |
|-------------------------------------|---------------|---------------|-------------------|
|-------------------------------------|---------------|---------------|-------------------|

v. Vehicle Performance Data Means for Eight Vehicle Fleet Means

In the Vehicle Performance series of charts, there are four composite mean results for each vehicle performance parameter compared to only three composite means for the tailpipe emissions data. This is due to an artifact of the emissions test cycle details and the data recording devices monitoring the signals coming from the vehicle engine control module (ECM). During the US FTP-75 cycle, the vehicle is turned off between the 2nd and 3rd phases. Upon "key-on" for the 3rd phase, the restart triggers the data acquisition unit to start a new and separate data file. The reader should also note that there are only eight vehicles included in these mean results because one of the test vehicles was not equipped with an ECM data logger. The ninth test vehicle without the data logger did complete the same set of emissions tests as the others, however, no ECM Performance data were captured from it.

1. Engine Speed

For a given emissions cycle, each of the vehicles is being commanded to run a series of maneuvers in exactly the same way and therefore, the composite mean vehicle speed across the entire emissions cycle is equivalent and precise from test to test. The engine speed, however, is a measure of how fast or slow the engine had to operate to drive the commanded vehicle speed trace under a given combination of elevation and fuel octane level. Note that engine speed in rpm is different than vehicle speed in mph or kph.



Figure 17 Eight Vehicle Fleet Engine Speed (rpm) Means with Confidence Intervals





Figure 18 Eight Vehicle Fleet Engine Load (%) Means with Confidence Intervals



3. Ignition Timing

Figure 19 Eight Vehicle Fleet Ignition Timing (°BTDC) Means with Confidence Intervals

4. Pre-Catalyst Temperature

For this octane study, the Pre-Cat temperature is indicative of the effect of octane on engine combustion temperature whereas the Mid-Cat temperature is indicative of impact of octane and the knock control response system on the heat release across the catalyst system (and potentially catalyst durability.) The average eight vehicle test fleet pre- and mid- catalyst temperature changes with octane shown in Figures 21 and 22 are small for the reasons described above regarding the vehicle to vehicle calibration differences in mitigating knock. The fleet average temperatures for 85 AKI test fuel compared to the 87 AKI temperatures on average were higher for the LA92 and US06 test cycles but not significant.



Figure 20 Eight Vehicle Fleet Pre-Catalyst Temperature (°C) Means with Confidence Intervals



5. Mid-catalyst Temperature

Figure 21 Eight Vehicle Fleet Mid-Catalyst Temperature (°C) Means with Confidence Intervals

vi. Percent Change in the Fleet Vehicle Performance Means: Engine speed, Percent Load, Ignition Timing, pre-Catalyst Exhaust Temperature, and mid-Catalyst Exhaust Temperature

The combined eight vehicle fleet means and percent changes for engine speed, percent load, and mid-catalyst temperatures show no significant differences while operating on the 85 and 87 AKI test fuels. Table 16 shows that spark retard (moving ignition timing closer to top dead center of piston travel) is however significantly different between the two test fuels while operating on the US06 cycle at 5,000 ft. and the resultant rejected in-cylinder heat from delayed combustion starts to show up in Table 17 as increased pre-catalyst (engine out) temperature differences.

| Ignition Timing (° B1 | TDC) | | | | | | | | | |
|-----------------------|--------|--------|---------|---------|----------|--------|--------|---------|---------|----------|
| Outliers Removed | 5000 | 5000 | p-value | Delta | % Change | 1000 | 1000 | p-value | Delta | % Change |
| | 85 AKI | 87 AKI | | 85 - 87 | 87> 85 | 85 AKI | 87 AKI | | 85 - 87 | 87> 85 |
| FTP-75 Bags 1&2 | 23.30 | 23.18 | 0.9344 | 0.13 | 0.5% | 23.39 | 23.27 | 0.9444 | 0.12 | 0.5% |
| FTP-75 Bag 3 | 23.03 | 23.45 | 0.2459 | -0.42 | -1.8% | 23.11 | 23.56 | 0.9606 | -0.45 | -1.9% |
| LA92 | 21.23 | 21.43 | 0.9182 | -0.20 | -0.9% | 21.31 | 21.58 | 0.8085 | -0.27 | -1.2% |
| US06 | 21.71 | 22.62 | 0.0193 | -0.92 | -4.1% | 21.47 | 22.19 | 0.0638 | -0.72 | -3.3% |

1. Ignition Timing

| Table 16 Fleet Average | Ignition | Timing |
|------------------------|----------|--------|
|------------------------|----------|--------|



Figure 22 Percent Change in Ignition Timing with Respect to Average Vehicle Speed

| Pre-Cat Temp. (°C) | | | | | | | | | | |
|-------------------------|--------|--------|---------|---------|----------|--------|--------|---------|---------|----------|
| Outliers Removed | 5000 | 5000 | p-value | Delta | % Change | 1000 | 1000 | p-value | Delta | % Change |
| | 85 AKI | 87 AKI | | 85 - 87 | 87> 85 | 85 AKI | 87 AKI | | 85 - 87 | 87> 85 |
| FTP-75 Bags 1&2 | 451.88 | 450.88 | 0.7868 | 1.00 | 0.2% | 457.47 | 457.36 | 0.9996 | 0.11 | 0.0% |
| FTP-75 Bag 3 | 463.01 | 461.97 | 0.9409 | 1.04 | 0.2% | 467.02 | 464.31 | 0.4751 | 2.71 | 0.6% |
| LA92 | 512.64 | 510.26 | 0.6397 | 2.38 | 0.5% | 514.38 | 510.75 | 0.2589 | 3.63 | 0.7% |
| US06 | 637.49 | 629.52 | 0.0124 | 7.97 | 1.3% | 640.84 | 635.08 | 0.3228 | 5.76 | 0.9% |

2. Pre-Catalyst Temperature

| Table 17 I | Fleet Averaae | Pre-Catalvst | Temperature |
|------------|---------------|--------------|-------------|
| | recerniciage | The Calaryst | remperature |

3. Engine Speed

| Table : | 18 | Fleet | Averaae | Enaine | Speed |
|---------|----|-------|---------|--------|-------|
|---------|----|-------|---------|--------|-------|

| Engine Speed (rpm) | | | | | | | | | | |
|-------------------------|---------|---------|---------|---------|----------|---------|---------|---------|---------|----------|
| Outliers Removed | 5000 | 5000 | p-value | Delta | % Change | 1000 | 1000 | p-value | Delta | % Change |
| | 85 AKI | 87 AKI | | 85 - 87 | 87> 85 | 85 AKI | 87 AKI | | 85 - 87 | 87> 85 |
| FTP-75 Bags 1&2 | 1276.09 | 1276.28 | 0.9998 | -0.19 | 0.0% | 1269.58 | 1269.54 | 1.0000 | 0.04 | 0.0% |
| FTP-75 Bag 3 | 1370.89 | 1372.28 | 0.9206 | -1.39 | -0.1% | 1360.87 | 1360.85 | 1.0000 | 0.02 | 0.0% |
| LA92 | 1406.36 | 1405.44 | 0.9952 | 0.92 | 0.1% | 1389.40 | 1390.70 | 0.9850 | -1.30 | -0.1% |
| US06 | 2118.66 | 2113.33 | 0.9623 | 5.33 | 0.3% | 2061.89 | 2055.54 | 0.9306 | 6.35 | 0.3% |

4. Engine Load

| | | | | | | - | | | | |
|-------------------------|--------|--------|---------|---------|----------|--------|--------|---------|---------|----------|
| Engine Load (%) | | | | | | | | | | |
| Outliers Removed | 5000 | 5000 | p-value | Delta | % Change | 1000 | 1000 | p-value | Delta | % Change |
| | 85 AKI | 87 AKI | | 85 - 87 | 87> 85 | 85 AKI | 87 AKI | | 85 - 87 | 87> 85 |
| FTP-75 Bags 1&2 | 27.78 | 27.66 | 0.9238 | 0.12 | 0.4% | 28.75 | 29.08 | 0.3396 | -0.33 | -1.1% |
| FTP-75 Bag 3 | 29.12 | 28.96 | 0.8173 | 0.16 | 0.6% | 30.25 | 30.07 | 0.7730 | 0.18 | 0.6% |
| LA92 | 30.02 | 29.94 | 0.9899 | 0.07 | 0.2% | 31.15 | 31.00 | 0.9164 | 0.15 | 0.5% |
| US06 | 41.43 | 40.93 | 0.6360 | 0.50 | 1.2% | 43.32 | 43.22 | 0.9947 | 0.10 | 0.2% |

Table 19 Fleet Average Engine Load

5. Mid-Catalyst Temperature

Table 20 Fleet Average Mid-Catalyst Temperature

| Mid-Catalyst Temp. | (°C) | | | | | | | | | |
|-------------------------|--------|--------|---------|---------|----------|--------|--------|---------|---------|----------|
| Outliers Removed | 5000 | 5000 | p-value | Delta | % Change | 1000 | 1000 | p-value | Delta | % Change |
| | 85 AKI | 87 AKI | | 85 - 87 | 87> 85 | 85 AKI | 87 AKI | | 85 - 87 | 87> 85 |
| FTP-75 Bags 1&2 | 564.20 | 562.67 | 0.6146 | 1.53 | 0.3% | 566.12 | 565.93 | 0.9986 | 0.20 | 0.0% |
| FTP-75 Bag 3 | 581.67 | 581.73 | 1.0000 | -0.06 | 0.0% | 579.56 | 576.60 | 0.5130 | 2.96 | 0.5% |
| LA92 | 638.79 | 636.25 | 0.4787 | 2.54 | 0.4% | 634.48 | 631.91 | 0.4718 | 2.56 | 0.4% |
| US06 | 766.67 | 759.46 | 0.2350 | 7.20 | 0.9% | 766.92 | 759.55 | 0.1861 | 7.38 | 1.0% |

vii. Individual Vehicle Performance Data Ignition Timing and Pre-Catalyst Exhaust Temperatures

The following series of charts show the percent change and absolute unit change due to the octane number and test cycle severity effects for each vehicle as it was driven over the many acceleration and deceleration modes of the emissions test cycles. In absolute terms, the averaged incremental vehicle ignition timing and exhaust temperature effects appear small relative to the FE and emissions impacts shown previously. Here analysis of modal emissions data, where vehicle acceleration maneuvers are separated from decelerations would help to better understand the true magnitude of octane number effects on spark timing and exhaust temperatures. The magnitude of emissions and FE effects are considered cumulative responses while ECM parameter impacts are essentially instantaneous differences.

1. Ignition Timing - Percentage Change for Individual Vehicles

Figure 24 and Table 21 show the ignition timing percent change while operating on 85 AKI relative to 87 AKI fuel. A negative number indicates "spark retard" as a control strategy of coping with auto-ignition. The amount of spark retard increases with test cycle severity. These percent change deltas do not include confidence intervals. Table 16 indicates that the intervals for the US FTP-75 and LA92 test cycles would cross zero and not be statistically different. The same conclusion can be drawn for the pre-catalyst temperature percent change deltas in Figure 25.



Figure 23 Average Vehicle Ignition Timing Percent Change when moving from 87 to 85 AKI Fuel

| | Altitude | lgniti | on Timing Cha | nge (%) 87 to 8 | 5 AKI |
|---------|----------|---------|---------------|-----------------|-------|
| VNumber | (ft.) | Bags1&2 | Bag3 | LA92 | US06 |
| 1 | 5000 | -1.10 | -5.52 | -4.92 | -5.37 |
| 2 | 5000 | -0.53 | -1.37 | -0.95 | -0.33 |
| 3 | 5000 | -0.15 | na | na | na |
| 4 | 5000 | 0.66 | -1.16 | -1.69 | -1.07 |
| 5 | 5000 | -0.30 | -2.25 | -0.69 | -7.66 |
| 6 | 5000 | 5.88 | na | 4.68 | -8.99 |
| 7 | 5000 | -0.15 | -1.68 | -0.76 | -1.43 |
| 8 | 5000 | 1.33 | -1.38 | -2.71 | -7.86 |
| 1 | 1000 | -0.35 | -6.42 | -3.19 | -6.95 |
| 2 | 1000 | 2.03 | -0.13 | -1.21 | -2.34 |
| 3 | 1000 | -0.23 | -2.60 | -2.32 | 0.54 |
| 4 | 1000 | -0.53 | -1.57 | 0.02 | -3.67 |
| 5 | 1000 | 0.36 | -5.64 | -7.05 | -6.50 |
| 6 | 1000 | 4.02 | 2.73 | 11.50 | 2.14 |
| 7 | 1000 | 0.03 | 0.04 | -2.15 | -1.05 |
| 8 | 1000 | -0.67 | -2.85 | -2.86 | -9.60 |

Table 21 Average Vehicle Ignition Timing Percent Change when moving from 87 to 85 AKI Fuel

| | Altitude | Ignition T | iming Chang | ge (°BTDC) 87 | to 85 AKI |
|---------|----------|------------|-------------|---------------|-----------|
| VNumber | (ft.) | Bags1&2 | Bag3 | LA92 | US06 |
| 1 | 5000 | -0.22 | -1.01 | -0.81 | -1.00 |
| 2 | 5000 | -0.14 | -0.38 | -0.26 | -0.10 |
| 3 | 5000 | -0.03 | na | na | na |
| 4 | 5000 | 0.17 | -0.32 | -0.43 | -0.29 |
| 5 | 5000 | -0.07 | -0.49 | -0.13 | -1.50 |
| 6 | 5000 | 1.03 | na | 0.68 | -1.33 |
| 7 | 5000 | -0.04 | -0.44 | -0.19 | -0.40 |
| 8 | 5000 | 0.32 | -0.32 | -0.57 | -1.48 |
| 1 | 1000 | -0.07 | -1.18 | -0.51 | -1.30 |
| 2 | 1000 | 0.54 | -0.04 | -0.33 | -0.71 |
| 3 | 1000 | -0.05 | -0.62 | -0.54 | 0.13 |
| 4 | 1000 | -0.14 | -0.43 | 0.00 | -0.99 |
| 5 | 1000 | 0.08 | -1.24 | -1.45 | -1.26 |
| 6 | 1000 | 0.73 | 0.57 | 1.80 | 0.31 |
| 7 | 1000 | 0.01 | 0.01 | -0.54 | -0.28 |
| 8 | 1000 | -0.16 | -0.65 | -0.58 | -1.67 |

2. Exhaust Pre-Catalyst Percent Change Deltas for Individual Vehicles



Figure 24 Average Vehicle Exhaust Pre-catalyst Percent Change when moving from 87 to 85 AKI Fuel

| | | Exhaust Precatalyst Temperature Change (%) | | | | | | |
|---------|----------|--|---------|--------|-------|--|--|--|
| | Altitude | | 87 to 3 | 85 AKI | 0 . / | | | |
| VNumber | (ft.) | Bags1&2 | Bag3 | LA92 | US06 | | | |
| 1 | 5000 | 1.42 | 1.52 | 1.83 | 2.23 | | | |
| 2 | 5000 | -0.76 | -0.61 | -0.97 | 0.27 | | | |
| 3 | 5000 | 0.03 | na | na | na | | | |
| 4 | 5000 | 0.58 | 0.54 | 0.96 | -0.23 | | | |
| 5 | 5000 | 1.03 | -0.17 | 1.77 | 3.82 | | | |
| 6 | 5000 | -0.02 | -0.08 | -0.35 | 0.87 | | | |
| 7 | 5000 | -0.38 | 0.41 | 0.10 | -0.30 | | | |
| 8 | 5000 | -0.02 | 0.22 | -0.01 | 1.65 | | | |
| 1 | 1000 | -0.41 | 1.60 | 0.82 | 1.47 | | | |
| 2 | 1000 | 0.36 | 0.27 | 0.70 | 0.75 | | | |
| 3 | 1000 | 0.22 | na | 0.61 | -0.45 | | | |
| 4 | 1000 | 0.24 | 0.86 | 0.74 | 1.10 | | | |
| 5 | 1000 | -0.29 | 2.07 | 3.38 | 2.32 | | | |
| 6 | 1000 | -0.77 | -2.03 | -0.87 | -0.14 | | | |
| 7 | 1000 | 1.14 | 0.56 | 0.71 | 0.87 | | | |
| 8 | 1000 | -0.31 | 0.39 | -0.16 | 1.46 | | | |

Table 24 Average Vehicle Exhaust Pre-Catalyst Temperature Change (°C) when moving from 87 to 85 AKI Fuel

| | Altitude | Exhaust Precatalyst Temperature | | | | | | |
|---------|----------|---------------------------------|------|------|------|--|--|--|
| VNumber | (ft.) | 87 to 85 AKI | | | | | | |
| 1 | | Bags1&2 | Bag3 | LA92 | US06 | | | |
| 1 | 5000 | 6.3 | 7 | 9.1 | 13.2 | | | |
| 2 | 5000 | -3.6 | -2.9 | -5.1 | 1.7 | | | |
| 3 | 5000 | 0.2 | na | na | na | | | |
| 4 | 5000 | 2.8 | 2.8 | 5.4 | -1.6 | | | |
| 5 | 5000 | 4 | -0.6 | 8.1 | 21.8 | | | |
| 6 | 5000 | -0.1 | -0.3 | -1.6 | 5.4 | | | |
| 7 | 5000 | -1.6 | 1.7 | 0.5 | -1.8 | | | |
| 8 | 5000 | -0.1 | 1.1 | -0.1 | 11.2 | | | |
| 1 | 1000 | -1.9 | 7.5 | 4.1 | 8.8 | | | |
| 2 | 1000 | 1.7 | 1.3 | 3.7 | 4.7 | | | |
| 3 | 1000 | 1.1 | na | 3.2 | -2.9 | | | |
| 4 | 1000 | 1.2 | 4.4 | 4.1 | 7.5 | | | |
| 5 | 1000 | -1.2 | 8 | 15.4 | 13.3 | | | |
| 6 | 1000 | -3.2 | -8.3 | -4 | -0.9 | | | |
| 7 | 1000 | 4.8 | 2.4 | 3.4 | 5.3 | | | |
| 8 | 1000 | -1.6 | 2.1 | -0.9 | 10.2 | | | |

e. Mean FE, CO₂, CO Results for the Combined Nine Vehicle Fleet - Octane Effects across Elevations The tables below show the FE, CO₂, and CO average fleet results when operating the vehicles on 85 AKI fuel at 5,000 ft. and 87 AKI fuel at 1,000 ft. as is commonly done in today's U.S. market. Because of the lower atmospheric pressure at 5,000 ft. and the engines' response to it, the interpretation of results becomes more convoluted. During the US FTP-75 and LA92 emissions cycle tests when the vehicles are less knock limited the FEs are statistically significantly higher for the 85 AKI/5,000 ft. case than the 87 AKI/ 1,000 ft. case but when the vehicles become knock limited during the US06 cycle 85 AKI/5,000 ft. the average is lower but not significantly. CO₂ behaves generally inversely to FE. CO shows higher averages in all cases for the 85 AKI / 5,000 ft. combination and is significantly higher value during the more knock limited US06 test cycle.

| FE (mpg) | | | | | |
|-------------------------|----------|----------|---------|-------------------------------|--------------|
| Outliers Removed | 5000 | 1000 | p-value | Combined Effects Delta | % Change |
| | 85 AKI | 87 AKI | | (85 - 87) | Delta / (87) |
| FTP-75 | 23.8775 | 23.2834 | <0.0001 | 0.5941 | 2.6% |
| LA92 | 23.3837 | 23.0942 | <0.0001 | 0.2895 | 1.3% |
| US06 | 22.5226 | 22.7917 | 0.3869 | -0.2691 | -1.2% |
| | | | | | |
| CO2 (gpm) | | | | | |
| Outliers Removed | 5000 | 1000 | p-value | Combined Effects Delta | % Change |
| | 85 AKI | 87 AKI | | (85 - 87) | Delta / (87) |
| FTP-75 | 336.3948 | 345.5458 | <0.0001 | -9.1510 | -2.6% |
| LA92 | 344.5251 | 350.2167 | <0.0005 | -5.6916 | -1.6% |
| US06 | 353.3398 | 351.5022 | 0.8360 | 1.8376 | 0.5% |
| | | | | | |
| CO (gpm) | | | | | |
| Outliers Removed | 5000 | 1000 | p-value | Combined Effects Delta | % Change |
| | | 07 4141 | | (05 07) | Dalta //07) |

| | 85 AKI | 87 AKI | | (85 - 87) | Delta / (87) |
|--------|--------|--------|--------|-----------|--------------|
| FTP-75 | 0.2802 | 0.2772 | 0.9976 | 0.0030 | 1.1% |
| LA92 | 0.2314 | 0.1796 | 0.0642 | 0.0518 | 28.8% |
| US06 | 1.8881 | 1.1183 | 0.0025 | 0.7698 | 68.8% |
| | | | | | |

f. Mean FE, CO₂, CO Results for the Individual Vehicles - Octane Effects across Elevations

Figures 26, 27, and 28 show the individual vehicle responses for Fuel Consumption, CO2, and CO, respectively when evaluating 85 AKI fuel at 5,000 ft. and 87 AKI fuel at 1,000 ft. During the non- or lightly knocking US FTP-75 and LA92 cycles the lower atmospheric pressure impacts on improved FE at 5,000 ft. can be seen relative to 1,000 ft. elevation. When octane is required as is the case during the US06 cycle, the benefits of higher octane show up.



Figure 25 Individual Vehicle Fuel Consumption Deltas (85 AKI@5000' gallons - 87 AKI@1000' gallons / 100 miles)



Figure 26 Individual Vehicle CO2 Ratio (85 AKI@5000' gpm / 87 AKI@1000' gpm)



Figure 27 Individual Vehicle CO Ratio (85 AKI@5000' gpm / 87 AKI@1000' gpm)

g. Vehicle Attribute Analyses

The test program included nine test vehicles with a range of attributes; production Model Years 2008 – 2013, four passenger cars and five light duty trucks, engine displacements from 1.4 - 5.4L, two direct and seven port fuel injected, and two turbocharged and seven naturally aspirated engines.

A series of general box plots were created to visualize how the vehicle attributes, test fuels, and emissions test cycles affected CO_2 tailpipe emissions; Cars vs Trucks, DI vs PFI, and Natural Aspiration vs Turbocharged. A Box Plot describes the range of data, its median, and 25th and 75th percentile data. A general example of the information a Box Plot shows is described in Figure 29.



Figure 28 Box Plot Statistical Representation of Data

i. CO₂ – Trucks versus Cars

Cars and trucks have different regulatory emissions certification levels and vehicle masses so it is not surprising that the four passenger cars and five light duty trucks of this study had significantly different levels of CO_2 (g/mile) from each other. (See Figure 30.) Significance testing showed them to have a p-value of <0.0001 for all emissions cycles and elevations tested. (See Figure 33.) However, looking at the impact of the incremental change (percent delta) in octane number from 85 to 87 AKI, neither of the two group (cars and trucks) mean CO_2 values were found to have a significant effect. (See bottom portion of Figure 33.) In other words, the incremental impacts of 85 and 87 AKI octane are very vehicle specific as described earlier in this report.



Figure 29 CO₂ (g/mile) Car and Truck Test Vehicles

ii. CO₂ – DI versus PFI

 CO_2 levels from the two Direct Injected and seven Port Fuel Injected vehicles were not significantly different. p-values ranged from 0.15 – 0.25.



Figure 30 CO2 (g/mile) Direct Injected and Port Fuel Injected Test Vehicles

iii. CO₂ - Naturally Aspirated versus Turbocharged

 CO_2 levels from the two turbocharged and seven naturally aspirated test vehicles were not significantly different. P-values ranged from 0.68 – 0.94. This may be a result of the fact that of the turbocharged vehicles, half (one) of them was a truck and the other a car. Of the seven naturally aspirated vehicles, three were cars and four were trucks. With an even distribution of cars and trucks within both naturally aspirated and turbocharged vehicles, it is unsurprising the p-values showed little statistical difference between the two attributes.



Figure 31 CO₂ (g/mile) Naturally Aspirated and Turbocharged Test Vehicles

iv. Significance of Vehicle Attributes for Carbon Dioxide Emissions

Statistical analysis of the CO_2 (g/mile) test vehicle means with respect to several vehicle attributes shows Cars to be significantly lower than Trucks. There were insignificant differences for the effects of the Fuels System type (DI vs PFI) and the Aspiration type (Naturally Aspirated vs Turbocharged.) (See top half of Figure 33.)

Statistical analysis of the percent changes in CO₂ within each vehicle using 87 versus 85 AKI fuel within an elevation and across elevations shows the Fuel System type to be significant in some cases. The Aspiration type becomes more significant while the differences between Cars and Trucks becomes less significant. (See bottom half of Figure 33.)

| | | | Car | /Truck | Fue | el System | Aspiration | |
|---------------|------------|------------|------------------|---------|---------------|-----------|-----------------|----------|
| | Altitude | Fuel1 | Car vs. Truck | p-value | DI vs. PFI | p-value | NA vs. Turbo | p-value |
| US FTP | 1,000 | 85 E10 | < | <.0001 | > | 0.15 | v | 0.89 |
| | 1,000 | 87 E10 | < | <.0001 | > | 0.15 | < | 0.89 |
| | 5,000 | 85 E10 | < | <.0001 | > | 0.17 | < | 0.93 |
| | 5,000 | 87 E10 | < | <.0001 | > | 0.15 | < | 0.93 |
| LA92 | 1,000 | 85 E10 | < | <.0001 | > | 0.19 | ~ | 0.89 |
| | 1,000 | 87 E10 | < | <.0001 | > | 0.23 | ~ | 0.94 |
| | 5,000 | 85 E10 | < | <.0001 | > | 0.18 | ~ | 0.88 |
| | 5,000 | 87 E10 | < | <.0001 | > | 0.19 | ~ | 0.90 |
| US06 | 1,000 | 85 E10 | < | <.0001 | > | 0.20 | ~ | 0.72 |
| | 1,000 | 87 E10 | < | <.0001 | > | 0.25 | ~ | 0.75 |
| | 5,000 | 85 E10 | < | <.0001 | > | 0.20 | < | 0.68 |
| | 5,000 | 87 E10 | < | <.0001 | > | 0.21 | < | 0.72 |
| | | | | | | | | |
| | | | Car | /Truck | Fue | el System | Asp | biration |
| | Percent | Change | Car vs. Truck | p-value | DI vs. PFI | p-value | NA vs. Turbo | p-value |
| US FTP | 87 to 85 A | KI @ 5000' | > | 0.17 | < | 0.05 | < | 0.77 |
| | 87 to 85 A | KI @ 1000' | > | 0.42 | < | 0.92 | < | 0.99 |
| | 85@5000 t | o 87@1000 | > | 0.97 | > | 0.02 | < | 0.25 |
| LA92 | 87 to 85 A | KI @ 5000' | > | 0.87 | > | 0.18 | < | 0.23 |
| | 87 to 85 A | KI @ 1000' | < | 0.62 | > | 0.01 | < | 0.15 |
| | 85@5000 t | o 87@1000 | > | 0.15 | < | 0.04 | > | 0.16 |
| US06 | 87 to 85 A | KI @ 5000' | > | 0.76 | > | 0.26 | < | 0.16 |
| | 87 to 85 A | KI @ 1000' | < | 0.33 | > | 0.17 | < | 0.66 |
| | 85@5000 t | o 87@1000 | > | 0.26 | < | 0.20 | > | 0.34 |

Figure 32 Significance of Vehicle Attributes for CO2 Emissions

v. Correlation of CO2 (g/mile) and Vehicle Load Factor (kg/L)

Vehicle load factor, as defined here, is the ratio of vehicle mass (kg) to engine displacement (L). The trend in most global markets is toward higher efficiency vehicles and load factors, with older less efficient vehicles and performance vehicles generally having lower load factors. The load factors represented in this program span from 441 kg/L to 1,032 kg/L and this distribution was chosen to better understand the influence of gasoline octane number on a broad range of U.S. marketplace vehicles. Figure 33 shows the Model Year 2013 U.S. passenger car and light duty truck load factor distribution.



Figure 33 MY 2013 U.S. Passenger Car and Light Duty Truck Load Factor Distributions

Figures 35 through 37 show the general trend of lower load factor vehicles producing more CO_2 emissions (g/mile) than higher load factor vehicles for the three emissions test cycles and nine test vehicles used throughout this program. The statistical R^2 "goodness of fit to the modeled equation" value is low and approximately 0.5 for the US FTP-75 and LA92 test cycles and decreases to approximately 0.4 for the US06 more aggressive drive cycle.



Figure 34 Correlation of Vehicle Load Factor to CO₂ Emissions for US FTP-75 Tests



Figure 35 Correlation of Vehicle Load Factor to CO₂ Emissions for LA92 Tests



Figure 36 Correlation of Vehicle Load Factor to CO₂ Emissions for US06 Tests

Figures 38 through 40 show no correlation between the Percent Delta CO2 emissions when using 85 and 87 AKI test fuels and vehicle load factors except for a mild correlation ($R^2 = 0.68$) for the 87 to 85 AKI case at 5,000 ft.



Figure 37 Correlation of Vehicle Load Factor to CO₂ Percent Deltas for the US FTP-75 Tests



Figure 38 Correlation of Vehicle Load Factor to CO₂ Percent Deltas for the LA92 Tests



Figure 39 Correlation of Vehicle Load Factor to CO₂ Percent Deltas for the US06 Tests

h. Vehicle Attributes Analyses – Individual Vehicle Results

i. Fuel Economy

Figure 41 shows the mean FE for each vehicle with respect to the altitude, and octane number. Each of the three emissions test cycles (driver styles) show a series of data (incremental effects of octane rating) that are either vertical or leaning to the right from bottom to the top indicating a neutral or increasing fuel economy for the 87 AKI test fuel compared to the 85 AKI test fuel.



Figure 40 Vehicle Fuel Economy with Respect to Octane Number and Altitude

ii. Carbon Dioxide

Figure 42 shows the CO₂ trends for each vehicle and are essentially the inverse of FE trends; lower CO2 with 87 AKI relative to 85 AKI fuel.



Figure 41 Vehicle CO₂ (gpm) with Respect to Octane Number and Altitude

iii. Carbon Monoxide

Figure 43 shows the CO emissions clustered tightly together for the USFTP-75 and LA92 cycles and much more varied for the US06 cycle. CO emission levels are usually lower for the 87 AKI fuel in each pair.



Figure 42 Vehicle CO (gpm) with Respect to Octane Number and Altitude



Figure 43 Engine Speed (rpm) with Respect to Octane Number and Altitude



v. Engine Load (Percent)

Figure 44 Engine Load (%) with Respect to Octane Number and Altitude





Figure 45 Engine Ignition Timing (°BTDC) with Respect to Octane Number and Altitude



vii. Pre-Catalyst Temperature

Figure 46 Exhaust Pre-Catalyst Temperature (°C) with Respect to Octane Number and Altitude





Figure 47 Exhaust Mid-Catalyst Temperature (°C) with Respect to Octane Number and Altitude

X. Recommendations

Next tests (future programs) should include both HC only and ethanol gasoline blends to understand the influence of ethanol or future renewable fuels on the magnitude of octane effects. Once the vehicle is designed for an "E10 blend" what are the implications of removing the ethanol for a given octane level?

To look for effects within individual vehicles using paired t-test statistics, the next programs should include multiple vehicles of the same model and replicate tests should be truly randomized in test sequence, i.e. flush and re-conditioning should be included along with each repeat.

More aggressive cycles like US06 only require fewer vehicles, while less aggressive cycles require more test vehicles. Also, consider increasing the number of tests on the less severe cycles while maintaining the number of more aggressive cycle tests.

If the research goal is to understand the impacts of two similar fuel octane number values on a fleet of vehicles then future programs should include additional fuels just outside these ranges, e.g. 83 and 89 AKI to improve the understanding of the two octane numbers of interest. In this study, the octane numbers were relatively close together. Interpolation of results around the octane numbers of interest would have offered better understanding of octane number effects on vehicle performance.

Because calculated fuel economy is a function of vehicle emissions (primarily CO₂) and vehicle emission levels vary considerably based on vehicle type, consider running blocks of vehicles in the same or closely matched

fuel economy ranges to improve the evaluation of the incremental octane effects on a block of more similar vehicles.

XI. Acknowledgments

The program Data Analysis Panel thanks Jim Rutherford (Chevron Oronite Statistician) for his many long hours providing a multitude of data analyses, figures and chart options to help understand the magnitude of fuel octane number effects on vehicle performance, both statistically and visually. His coaching, experience and discussions on the data statistical significance and trend analyses were very much appreciated.

The program Data Capture Team thanks Dave Gian (FEV Inc.) for his technical guidance and insights into developing robust vehicle emissions test methodologies and protocols and Sridhar Koushik (FEV Inc.) for his excellent help in identifying the web-based vehicle data loggers and ensuring their proper function. Dave and Sri were essential in helping the test program get started properly and to collect accurate data.
XII. Appendices

a. SOW

SOW: Sub-Regular Grade Octane Rating (85AKI) Study

Background: The performance of spark-ignition engines is dependent upon the antiknock rating for which the engine was designed. Modern day engines are calibrated for maximum fuel economy and performance while minimizing emissions using the grade of gasoline that the manufacturer requires for use in the vehicle's operating manual. The use of fuel that is below the recommended AKI rating may result in the vehicle or engine being operated outside of conditions for which it was designed and calibrated, creating the possibility for voiding the vehicle's warranty.

The specifications for gasoline used in spark-ignition engines in the United States are found under ASTM D4814. Although the ASTM standard does not explicitly list specifications for antiknock/ octane ratings, it does provide non-mandatory information in its appendix. In the Appendix of ASTM D4814, the effect of altitude on vehicle antiknock requirement is listed for vehicles that are pre-1984 vintage. These vehicles lack the sophisticated control systems found in today's vehicles and may require fuels with different antiknock ratings upon changing altitude. The ASTM standard lists five areas in the western United States where reduced antiknock requirements for pre-1984 vehicles are applicable based on the altitude of the area. However, the ASTM standard also notes that "new vehicles have sensors to measure and engine management computers, which take into account such conditions as air charge temperature and barometric pressure. These vehicles are designed to have the same antiknock requirement at all altitudes."

Based on recent regulatory changes in some western states that allow the use of 85 AKI for newer vehicles, the importance of maintaining AKI levels in market fuels at levels that meet the engine manufacturer's requirements was made clear. As stated above, modern day vehicles do not experience any decreases in octane requirements as altitude increases. Currently, there are no publically available studies that show the degradation of performance and/or increased exhaust emissions due to the use of sub-regular grade 85 AKI fuel. Thus, a study is needed to evaluate the potential for decreased performance or increased emissions when using 85 AKI fuel versus the manufacturer's recommended "regular grade" 87 AKI fuel.

Program Proposal (General): The proposed study may consist of engine dynamometer and/or vehicle tests evaluating the impacts on fuel economy and emissions (criteria pollutants and CO2) when an 85 AKI fuel is used versus 87 AKI fuel. Higher load conditions, such as during towing performance tests or a high load emissions test may be considered. Vehicle selection should include vehicles that are expected to come to the market such as those equipped with engines that are downsized and exhibit a lower ratio of engine displacement size to vehicle weight. Likewise, vehicles that can tow heavy trailers relative to their engine size are also candidates for evaluation and testing. The study should include the use of fuels that are representative of fuels available in the high altitude market place where the 85 AKI and equivalent fuels are found, this would include E10 85 AKI and E10 87 AKI fuels, it is possible that an 85AKI E0 fuel could be included for comparison while the fuel recommended by the manufacturer (87 AKI) would serve as baseline fuel.

Program Proposal (Specific):

The request for CRC Funds is for fuel blending, vehicle transport from SwRI to Michigan, and ECM data acquisition instrumentation in a program structure as outlined below. The vehicles will come from OEM fleets and the current EPAct fleet at SwRI.

- Program Objective
 - Evaluate vehicle performance and emissions effects of 85 AKI gasoline relative to 87 AKI gasoline at two elevations.

Test Locations

- Variable Altitude Chassis Dynamometer Emissions Chambers (GM, Ford, Chrysler)
- Two test elevations: Low = 1,000 ft and High 5,000 ft
- No other contract lab with variable altitude emissions capability located

Metrics for evaluation

- Fuel economy
- Emissions (CO₂, CO, NO_x, THC, NMOG)
- Pre-cat inlet temperature
- Spark Advance
- Stoichiometry

• Vehicle selection criteria

- 9 Test vehicles Purposely varied engine architectures, load factors,
- model years, manufacturers, and passenger cars and trucks.

• Vehicle load factors have been increasing for some time in the US marketplace as a result of a push for higher vehicle FE and lower GHG emissions.

| <u>Vehicle</u> | Model Year | <u>Odometer</u> | Fuel System | Induction System | Eng. Disp. (L) |
|-----------------------|------------|-----------------|-------------|------------------|----------------|
| <u>Toyota Corolla</u> | 2008 | 13,248 | PFI | Nat. Asp. | 1.8 |
| <u>Honda Odyssey</u> | 2008 | 13,248 | PFI | Nat. Asp. | 3.5 |
| <u>Honda Fit</u> | 2012 | 19,378 | PFI | Nat. Asp. | 1.5 |
| Ford Transit Connect | 2010 | 11,860 | PFI | Nat. Asp. | 2.0 |
| Ford Focus | 2008 | 12,563 | PFI | Nat. Asp. | 2.0 |
| Ford F-150 Ecoboost | 2011 | 5,200 | DI | Turbo | 3.5 |
| <u>Ford F-150</u> | 2008 | 15,487 | PFI | Nat. Asp. | 5.4 |
| Dodge Dart | 2013 | 14,403 | PFI | Turbo | 1.4 |
| <u>Chevy Equinox</u> | 2010 | 37,396 | DI | Nat. Asp. | 3.0 |

Test Fuels

- Matched E10 blends of 85 and 87 AKI fuel pair
- Equivalent properties including heating value, composition, (aromatics, olefins and sulfur), RVP, distillation (T50 and T90) and H/C ratio
- Octane tolerance 85.0-85.4 and 87.0-87.4; Sensitivity tolerance 6-8
- Fuel supplier can meet targets except Octane Sensitivity for 85 AKI, currently 4.9
- Lab inspections: 3 or 4 lab validation. BP, Flint Hills, Chevron confirmatory labs
- Fuel Volume: 4 gal flush +12 gal fill. (20 mile conditioning and 2 repeat tests)

Test cycles

- Preliminary: Each vehicle will receive a USFTP-75 on Tier 2 to validate emissions performance
 - Test cycles: 1×USFTP-75 (cold) + 1×LA92 (hot) + 1×US06 (hot)
 - Repeat 2 consecutive days no fuel change between
- Test order:
 - Five cars will start with 87 AKI and switch to 85 AKI (A \rightarrow B)
 - Five cars will start with 85 AKI and switch to 87 AKI ($B \rightarrow A$)
- Number of tests:
 - 9 vehicles x 2 fuels x 2 repeats x 2 altitudes = 72 observations
 - 2 observations / day = 40 work days
 - Additional 20 days for fuel switching, initial data analysis, extra tests





| | | | | | CRC E-108 Program Tes | t Vehicles | | | |
|------------------------------|-------------------|-------------------|-------------------|-------------------|-----------------------|--------------------------|-------------------|-------------------|-------------------|
| Year | 2012 | 2008 | 2008 | 2010 | 2011 | 2013 | 2008 | 2008 | 2010 |
| Make | Honda | Ford | Toyota | Ford | Ford | Dodge | Ford | Honda | Chevrolet |
| Model | Fit | Focus | Corolla CE | Transit Connect | F-150 | Dart SXT | F150 XL 5.4 4x2 | Odyssey LX | Equinox |
| VIN | JHMGE8H3XCC005253 | FAHP32N58W151200 | 1NXBR32E88Z050881 | NMOKS9BN5AT000010 | 1FTFX1ET8BKD00021 | 1C3CDFBH5DD576113 | 1FTPF12V98KB22903 | 5FNRL38288B017848 | 2CNFLDEY0A6200484 |
| Odometer | | 12563 | 13248 | 11860 | 5,200 | 14403 | 15487 | 13248 | 37396 |
| Engine | 1.5L I4 Nat Asp | 2.0L 14 | 1.8L I4 | 2.0L I4 | 3.5L V6 | 1.4L Turbo | 5.4L Nat Asp | 3.5L Nat.Asp | 1706 |
| Displacement | 1.5 | 2.0 | 1.8 | 2.0 | 3.5 | 1.4 | 5.4 | 3.5 | 3.0 |
| Transmission | 5-spd A/T - 6T40 | 4-spd A/T - 4F27E | 5-spd A/T | 4-spd A/T | 6-speed A/T - 6R80 | 6-speed DDCT - C635 | 4-SPD - 4R75E | 5-spd A/T | 6-spd A/T - 6T70 |
| 1st gear | 2.996 | 2.81 | 3.166 | 2.82 | 4.17 : 1 | 4.15 | 2.84 | 2.7 | 4.48 |
| 2nd gear | 1.679 | 1.49 | 1.904 | 1.5 | 2.34 : 1 | 2.26 | 1.95 | 1.61 | 2.87 |
| 3rd gear | 1.067 | 1 | 1.31 | 1 | 1.52 : 1 | 1.44 | 1.00 | 1.07 | 1.84 |
| 4th gear | 0.761 | 0.73 | 0.885 | 0.73 | 1.14 : 1 | 0.97 | 0.70 | 0.77 | 1.41 |
| 5th gear | 0.552 | | 0.725 | | 0.86 : 1 | 0.75 | | 0.58 | 1 |
| 6th gear | - | | | | 0.69 : 1 | 0.62 | | - | 0.74 |
| Reverse | 1.957 | | | 2.65 | 3.40 : 1 | 4 | | 1.89 | 2.88 |
| Final Drive | 4.563 | 3.34 | 2.96 | 4.2 | 3.55 | 4.43 | 3.55 | 4.312 | 2.77 |
| Fuel System | PFI | PFI | PFI | PFI | GDI | PFI | PFI-FFV | PFI | GDI |
| Recommended fuel (R+M)/2 | 87 | 87 | 87 | 87 | 87 | 93 prefered, 87 accepted | 87 | 87 | 87 |
| Aspiration | NA | NA | NA | NA | Turbocharged | Turbocharged | NA | NA | Nat. Asp. |
| Curb Weight (FEV measured) | 2,553 | 2,588 | 2,520 | 3492 | 5,289 | 3,261 | 4,844 | 4,311 | 3900 |
| ETW in lbs | 2,875 | 3,000 | 2,875 | 3750 | 5,500 | 3,500 | 5,250 | 4,750 | 4500 |
| Curb Weight (kg) | 1158 | 1174 | 1143 | 1584 | 2399 | 1479 | 2197 | 1955 | 1769 |
| Load Factor (kg/L) | 772 | 587 | 635 | 792 | 685 | 1057 | 407 | 559 | 590 |
| | | | | | | | | | |
| Emission Control Information | | | | | | | | | |
| U.S.EPA | T2B5 | T2B4 | T2B5 | T2B4 | T2B4 | T2B5 | T2B8 | T2B5 | T2B4 |
| Emission Cert Group | LDV | LDV | LDV | LDT1 | LDT2 | LDV | LDT2 | LDT2 | LDT2 |
| California | Lev II ULEV PC | ULEV II | ULEV II | not certified | | LEV II PC | | ULEV II | ULEV Qual. |
| OBD | CA OBD II | CA II | OBD II | OBD II | OBD II | CA OBD II | FII | CA OBD II | CA OBD II |
| Fuel | Gasoline | Gasoline | Gasoline | Gasoline | Gasoline | Gasoline | Gasoline | Gasoline | Gasoline |
| Test Group | CHNXV01.5HB2 | 8FMXV02.0VD4 | 8TYXV01.8BEA | AFMXT2.01DV | BFMXT03.54EP | DCRXV01.44P1 | 8FMXT05.44HF | 8HNXT03.54KR | AGMXJ03.0157 |
| Evaporative Family | CHNXROO96VEA | 8FMXR0125KAK | 8TYXR0115P12 | AFMXR0125NBB | BFMXR0265NBV | DCRXR0100PKO | 8FMXR0240NBR | 8HNXR0163BBA | AGMXR0138813 |

d. Octane Test Fuels – Detailed

| Name | | | Test Methods | Test Method | Test Method | Test Method | Test | 85 AKI E10 | 85 AKI E10 | 85 AKI E10 | 85 AKI E10 | | | | 87 AKI E10 | 87 AKI E10 | 87 AKI E10 | 87 AKI E10 | 87 AKI E10 | | | |
|------------------|-----------------|-----------|-----------------|----------------|----------------|----------------|------------------|-------------------|--------------------|--------------------|--------------------|---------------|---------------------|--------------|--------------------|--------------------|----------------------|----------------------|-------------------|---------|---------|----------|
| | | Requested | GAGE | Used? | Used? | Used? | | GAGE | lah 2 | lah 3 | Lah 4 | Average | Std | % CoV | GAGE | Lah 2 | Lah 2 | Lah 3 | Lah 4 | Average | Std | % CoV |
| RON | | D2699 | D2699 | D2699 | D2699 | D2699 | RON | 88.0 | 88.4 | 87.4 | 87.6 | 87.9 | 0.4 | 0.5% | 91.0 | 91.0 | 90.8 | 90.5 | 90.2 | 90.7 | 0.3 | 0.4% |
| MON | | D2700 | D2700 | D2700 | D2700 | D2700 | MON | 82.0 | 81.7 | 82.0 | 82.4 | 82.0 | 0.3 | 0.4% | 83.2 | 84.7 | 84.0 | 83.6 | 84.0 | 83.9 | 0.6 | 0.7% |
| AKI | | | (R+M)/2 | (R+M)/2 | (R+M)/2 | (R+M)/2 | AKI | 85.0 | 85.1 | 84.7 | 85.0 | 84.9 | 0.2 | 0.2% | 87.1 | 87.9 | 87.4 | 87.1 | 87.1 | 87.3 | 0.3 | 0.4% |
| Sensitivity | | Calc. | R-M | R-M | R-M | R-M | Sensitivity | 6.0 | 6.7 | 5.4 | 5.2 | 5.8 | 0.7 | 11.6% | 7.8 | 6.3 | 6.8 | 6.9 | 6.2 | 6.8 | 0.6 | 9.4% |
| , | | | | | | | , | | | | | | | | | | | | | | | |
| Relative Density | S.G. 60/60F | D1298 | D4052 | D4052 | D4052 | D4052 | Relative Density | 0.7357 | 0.7359 | 0.7357 | 0.7365 | 0.7360 | 0.0 | 0.1% | 0.7367 | 0.7368 | | 0.7365 | 0.7364 | 0.7366 | 0.0 | 0.0% |
| DVPE | psi @ 100F | D5191 | D5191 | D5191 | D5191 | D5191 | DVPE | 8.32 | 8.18 | 8.59 | 8.48 | 8.39 | 0.2 | 2.1% | 8.57 | 8.62 | | 8.89 | 8.77 | 8.71 | 0.1 | 1.7% |
| Distillation | deg. F | D86 | D86 | D86 | D86 | D86 | Distillation | | | | | | | | | | | | | 1 | | |
| IBP | uc <u>p</u> . 1 | 500 | 200 | 200 | 200 | 500 | IBP | 100.0 | 100.4 | 98.2 | 104.4 | 100.8 | 2.6 | 2.6% | 105.8 | 96.2 | | 96.3 | 102.9 | 100.3 | 4.8 | 4.8% |
| T5 | | | | | | | T5 | 125.2 | 128.7 | 126.6 | 126.6 | 126.8 | 1.4 | 1.1% | 123.3 | 122.9 | | 126.6 | 124.4 | 124.3 | 1.7 | 1.3% |
| T10 | | | | | | | T10 | 133.0 | 134.9 | 134.0 | 133.5 | 133.8 | 0.8 | 0.6% | 130.6 | 130.3 | | 132.7 | 131.5 | 131.3 | 1.1 | 0.8% |
| T20 | | | | | | | T20 | 142.5 | 144.0 | 142.8 | 142.5 | 143.0 | 0.7 | 0.5% | 140.7 | 140.7 | | 141.3 | 141.4 | 141.0 | 0.4 | 0.3% |
| T30 | | | | | | | T30 | 149.2 | 151.2 | 149.2 | 149.3 | 149.7 | 1.0 | 0.7% | 147.7 | 147.8 | | 147.4 | 148.3 | 147.8 | 0.4 | 0.3% |
| T40 | | | | | | | T40 | 162.0 | 166.1 | 159.7 | 162.0 | 162.4 | 2.7 | 1.6% | 153.1 | 155.3 | | 154.3 | 154.5 | 154.3 | 0.9 | 0.6% |
| T50 | | | | | | | T50 | 214.7 | 220.0 | 214.3 | 215.2 | 216.1 | 2.7 | 1.2% | 213.3 | 212.2 | | 208.8 | 211.3 | 211.4 | 1.9 | 0.9% |
| T60 | | | | | | | T60 | 240.8 | 241.5 | 239.4 | 240.0 | 240.4 | 0.9 | 0.4% | 240.6 | 243.0 | | 242.8 | 243.8 | 242.6 | 1.4 | 0.6% |
| T70 | | | | | | | T70 | 260.1 | 264.4 | 261.2 | 261.2 | 261.7 | 1.9 | 0.7% | 264.4 | 265.1 | | 265.3 | 265.5 | 265.1 | 0.5 | 0.2% |
| T80 | | | | | | | Т80 | 285.3 | 288.7 | 284.9 | 285.5 | 286.1 | 1.8 | 0.6% | 287.1 | 286.5 | | 285.5 | 287.9 | 286.7 | 1.0 | 0.4% |
| Т90 | | | | | | | Т90 | 313.3 | 315.0 | 313.2 | 313.2 | 313.7 | 0.9 | 0.3% | 314.8 | 313.5 | | 312.1 | 314.0 | 313.6 | 1.1 | 0.4% |
| T95 | | | | | | | T95 | 333.7 | 341.8 | 334.1 | | 336.5 | 4.6 | 1.4% | 337.5 | 340.9 | | 332.5 | | 337.0 | 4.2 | 1.3% |
| FBP | | | | | | | FBP | 360.3 | 361.1 | 358.3 | 359.7 | 359.9 | 1.2 | 0.3% | 360.1 | 363.0 | | 359.2 | 361.5 | 361.0 | 1.7 | 0.5% |
| Residue | | | | | | | Residue | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 0.0 | 0.0% | 1.2 | 1.0 | | 1.0 | 1.0 | 1.1 | 0.1 | 9.5% |
| DI | | | | | | | DI | 1180 | 1203 | 1179 | 1182 | 1186.1 | 11.1 | 0.9% | 1174 | 1172 | | 1160 | 1168 | 1168.5 | 6.0 | 0.5% |
| Aromatics | v% | D1319 | D1319 | D1319 | D1319 | | Aromatics | 10.5 | 14.0 | 10.4 | | 11.6 | 2.1 | 17.6% | 11.1 | 13.1 | | 10.5 | | 11.6 | 1.4 | 11.8% |
| Olefins | | | | | D1319 | | Olefins | 6.7 | 9.6 | 8.2 | | 8.2 | 1.5 | 17.8% | 7.0 | 10.3 | | 8.7 | | 8.7 | 1.7 | 19.0% |
| Paraffins | | | | | D1319 | | Paraffins | 73.0 | 65.8 | 72.1 | | 70.3 | 3.9 | 5.6% | 72.0 | 65.7 | | 71.3 | | 69.7 | 3.5 | 5.0% |
| Ethanol | | | | D4815 | D4815 | | Ethanol | 9.80 | 10.6 | 9.3 | 9.4 | 9.9 | 0.6 | 6.3% | 9.86 | 10.9 | | 9.5 | 9.5 | 10.1 | 0.7 | 6.9% |
| Sum | | | | | | | Sum | 100.0 | 100.0 | 100.0 | | - | | | 100.0 | 100.0 | | 100.0 | | - | | |
| | | | | | | | | | | | | - | | | | | | | | 4 | | |
| Sulfur | ppm | D7039 | D5453 | D2622 | D5453 | D5453 | Sulfur | <0.0001 | <5 | <1 | 0.25 | 0.3 | #DIV/0! | #DIV/0! | <0.0001 | <5 | | <1 | 0.22 | 0.2 | #DIV/0! | #DIV/0! |
| Carbon | wt% | D3343 | D5291 | | 5291 | | Carbon | 81.68 | | 81.51 | | 81.6 | 0.1 | 0.1% | 81.90 | | | 81.62 | | 81.8 | 0.2 | 0.2% |
| Hydrogen | wt% | D3343 | D5291 | | 5291 | D3343 | Hydrogen | 14.57 | | 14.50 | 14.56 | 14.5 | 0.0 | 0.3% | 14.22 | | | 14.49 | 14.51 | 14.4 | 0.2 | 1.1% |
| H/C Ratio | | Calc. | Calc. | | | | H/C Ratio | 2.120 | | 2.12 | | 2.1 | 0.0 | 0.0% | 2.068 | | | 2.12 | | 2.1 | 0.0 | 1.8% |
| | | | | | | | | | | | | | | | | | | | | 1 | | |
| NHV* | btu/lb | D240 | D240 | | D4809 | | NHV* | 18,181.3 | | 19,312 | | 18746.7 | 799.5 | 4.3% | 18,129.8 | | | 19,331 | | 18730.4 | 849.4 | 4.5% |
| Existent Gum | mg/100ml | D381 | D381 | D381 | D381 | D381 | Existent Gum | | | | | | | | <0.5 | | | | | 1 | | |
| - Unwashed | 116/ 100111 | 0301 | 200 nnm P | FA Added | 0301 | 0301 | - Unwashed | 14.6 | 5.0 | 9.8 | 16.6 | 11.5 | 52 | 45 1% | 5.8 | 60 | | 11.8 | 17.8 | 10.4 | 57 | 55.0% |
| - Washed | 1 | | 200 pp/111 | | 1 | | - Washed | <0.5 | 0.0 | 0.0 | 0.0 | 01 | 0.2 | 173.2% | 5.0 | 0.0 | | 0.0 | 0.4 | 0.1 | 0.2 | 173.2% |
| washeu | | | | | | I | washeu | -U.J | 0.0 | 0.0 | 0.4 | 0.1 | 0.2 | 1/ J.2/0 | | 0.0 | | 0.0 | 0.4 | 0.1 | 0.2 | 11 J.2/0 |
| | | | | | | | (*) Note: | Wide variation in | NHV from two lab | s Chrysler re-and | lyzed the 97 AVI + | est fuel NH | V = <u>4</u> 1 52 M | MI/kg (17 90 | 94 BTH/Ih) Ikod F |)740 test method I | ah 3 annears to have | e reported HHV inc | nt NHV | | | |
| | | | | | | | () Hote: | Confirmed that e | ach of the 3 OEM E | missions Sites use | d the Average NH | V from this s | preadshee | et. FE numb | pers should not be | compared to those | reported to EPA (p | lus these are not Ti | er 2 Cert Fuels.) | | | |
| - | | | | | | | | | | | ~ | | | | | | | | , | | | |

e. Standardized Vehicle Emissions Drive Cycles - Detailed

Reference: https://www.dieselnet.com/standards/cycles/#us-ld

US-FTP-75

i.

The FTP-75-75 (Federal Test Procedure) has been used for emission certification and fuel economy testing of lightduty vehicles in the United States since 1978. The test is often referred to as simply 'FTP-75' (this should not be confused with the FTP-75 test for heavy-duty engines).

The FTP-75-75 and the FTP-75-72 are two variants of the EPA Urban Dynamometer Driving Schedule (UDDS). The FTP-75-75 cycle is derived from the FTP-75-72 by adding a third phase of 505 s, identical to the first phase of FTP-75-72 but with a hot start. The third phase starts after the engine is stopped for 10 minutes. Thus, the entire FTP-75-75 cycle consists of the following segments:

- 1. Cold start transient phase (ambient temperature 20-30°C), 0-505 s
- 2. Stabilized phase, 506-1372 s
- 3. Hot soak (min 540 s, max 660 s)
- 4. Hot start transient phase, 0-505 s

Emissions from each phase are collected in a separate teflon bag, analyzed and expressed in g/mile (g/km). The weighting factors are 0.43 for the cold start phase, 1.0 for the 'stabilized' phase and 0.57 for the hot start phase.



Figure 48 Vehicle Speed Trace of US FTP-75 Emissions Test Cycle

ii. LA92

The California Unified Cycle (UC), Figure 1, is a dynamometer driving schedule for light-duty vehicles developed by the California Air Resources Board. The test is also referred to as the Unified Cycle Driving Schedule (UCDS). The UC test was referred to in the past as the LA92 test. It was often called the "Unified LA92", to distinguish it from a "short LA92"; test, which included the first 969 seconds of the Unified LA92.

The UC test has a similar three-bag structure to the US FTP-75, but is a more aggressive driving cycle than the federal FTP-75-75; it has higher speed, higher acceleration, fewer stops per mile, and less idle time. The UC test is run in the

following manner: Bags 1 and 2 are run consecutively, followed by a ten minute hot soak, then Bag 3 which is a duplicate of Bag 1. Overall cycle emissions are calculated in the same manner as the weighted, overall FTP-75-75 formula, taking actual mileage from the UC into account.



Figure 49 Vehicle Speed Trace of LA92 Emissions Test Cycle

iii. USO6

The US06 Supplemental Federal Test Procedure (SFTP-75) was developed to address the shortcomings with the FTP-75-75 test cycle in the representation of aggressive, high speed and/or high acceleration driving behavior, rapid speed fluctuations, and driving behavior following startup.

Since model year 2008, the US06 results are also used for the determination of the EPA on-road fuel economy ratings using the EPA 5-cycle method.



Figure 50 Vehicle Speed Trace of US06 Emissions Test Cycle

g. Significance of Vehicle Driver Behavior on Real World Fuel Economy and Results of This Program Reference: U.S. EPA, Final Technical Support Document, "Fuel Economy Labeling of Motor Vehicles: Revisions to Improve Calculation of Fuel Economy Estimates," EPA420-R-06-01, December 2006.

There is a general recognition that the original US FTP-75 emissions test cycle and fuel economy (FE) vehicle label calculations did not adequately represent enough consumer driving habits to ensure consumer real world fuel economy matched their vehicle's FE label estimates. The 2006 U.S. EPA Technical Support Document describes the new 5-cycle calculation of vehicle FE and significance of understanding a range of driver behaviors on this program's measurement of fuel octane rating effects on vehicle performance.

"A fundamental issue with today's fuel economy estimates is that the underlying test procedures do not fully represent real-world driving conditions. Some of the key limitations are that the highway test has a top speed of only 60 miles per hour, both the city and highway tests are run at mild climatic conditions (75°F), both tests have mild acceleration rates, and neither test is run with the use of accessories, such as air conditioning. However, since the time of the last fuel economy labeling revisions in the mid-1980's, EPA has established several additional test procedures, used for emissions compliance purposes, which capture a much broader range of real-world driving conditions. Specifically, these emissions test cycles capture the effects of higher speeds, more aggressive driving (i.e., higher acceleration rates), the use of air conditioning at higher ambient temperatures, and colder temperature operation. Our analysis indicates that these factors can have a significant impact on fuel economy, and that the impacts can vary widely across different vehicles."

EPA's Technical Support document goes on to state, "Our final rule revises the test methods by which the city and highway fuel economy estimates are calculated. We are replacing the current method of adjusting the city (FTP-75) test result downward by 10% and the highway (HFET) test result downward by 22%. Instead, we are finalizing a new approach that incorporates additional test methods that address factors that impact fuel economy, but are missing from today's tests – specifically, higher speeds, more aggressive driving (higher acceleration rates), the use of air conditioning, and the effect of cold temperature. The new test methods will bring into the fuel economy estimates the test results from the five emissions tests in place today: FTP-75, HFET, US06, SC03, and Cold FTP-75.^a

[°] The US06 test is designed to represent high speed highway driving and aggressive (i.e., rapid accelerations and decelerations) urban driving. The SC03 test is designed to represent the impact of air conditioner operation at high temperatures. The Cold FTP-75, which is conducted at 20°F, is designed to reflect the impact of cold temperatures. "

h. Potential Data Outlier Tables

| Cor | e Emission | s Data Rep | eatability |
|-----------|--|--|--|
| | Poten | tial Outliers | 6 |
| | LA92 | US FTP | US06 |
| InCO | 1 (2, 5000, 87 E10) | 1 (3, 1000, 87 E10) | 2 (2, 1000, 87E 10) (2, 1000, 87 E10) |
| InCO2 | 0 | 0 | 1 (3, 1000, 85 E10) |
| FC | 0 | 0 | 2 (3, 1000, 85 E10) (3, 5000, 85 E10) |
| InNMOG | 3 (2, 1000, 85 E10) (2, 5000, 85 E10) (2, 5000, 85 E10) | 3 (2, 1000, 87 E10) (2, 5000, 85 E10) (3, 5000, 85 E10) | 0 |
| (vehicle, | altitude, fuel) | | |

| (| Core Emissi | ions Data M | leans |
|-----------|-------------------|-------------------|-------------------|
| | Poten | tial Outliers | 5 |
| | LA92 | US FTP | US06 |
| | 1 | 0 | 1 |
| InCO | (8, 1000, 85 E10) | | (5, 5000, 85 E10) |
| | 1 | 1 | 1 |
| InCO2 | (5, 1000, 87 E10) | (4, 1000, 85 E10) | (3, 1000, 87 E10) |
| | 1 | 1 | 1 |
| FC | (5, 1000, 87 E10) | (4, 1000, 85 E10) | (3, 1000, 87 E10) |
| | 1 | 1 | 1 |
| InNMOG | (3, 5000, 85 E10) | (2, 1000, 85 E10) | (4, 5000, 85 E10) |
| (vehicle, | altitude, fuel) | | |

| | Performance Data | Potential | Outliers | |
|--------------------|--------------------|-----------|-------------------|------|
| | Bag3 | Bags1&2 | LA92 | US06 |
| | 1 | | | |
| Engine Speed | (6, 1000, 87 E10) | 0 | 0 | 0 |
| | 1 | | | |
| Load | (7, 1000, 85 E10) | 0 | 0 | 0 |
| | 1 | | | |
| Ignition Timing | (6, 5000, 87 E10) | 0 | 0 | 0 |
| | 1 | | | |
| ExPreCatAvg | (3, 1000, 85 E 10) | 0 | 0 | 0 |
| | | | 1 | |
| CatMidAvg | 0 | 0 | (5, 1000, 87 E10) | 0 |
| (vehicle, altitude | e, fuel) | | | |



Figure 51 CO2 Emissions from SOT to EOT Measured on Tier2 Emissions Certification Fuel



Figure 52 CO Drift SOT to EOT

Analysis of Vehicle Response Drift: SOT → EOT Emissions and FE Data US FTP Tests; Tier 2 Emissions Cert Fuel

- Significant (p<0.05) drift for CO₂ and FE for vehicle 1.
- Significant (p < 0.05) drift for CO, CO₂ and FE for vehicle 5.
- Significant drift for CO for vehicle 7.

| | | | | p-val | ues for | drift | | | |
|-----------------|-------|-------|-------|-------|---------|-------|-------|-------|-------|
| Vehicle Number | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| со | 0.164 | 0.749 | 0.419 | 0.252 | 0.004 | 0.522 | 0.045 | 0.324 | 0.722 |
| CO ₂ | 0.000 | 0.826 | 0.754 | 0.073 | 0.001 | 0.944 | 0.906 | 0.127 | 0.521 |
| FE | 0.002 | 0.889 | 0.753 | 0.087 | 0.001 | 0.955 | 0.802 | 0.225 | 0.926 |
| NMOG | 0.706 | 0.540 | 0.385 | 0.173 | 0.955 | 0.870 | 0.167 | 0.220 | 0.211 |

Emissions Data Sheet Inspection

- Vehicle 1: CO2 / FE Data Tight Precision. Small change in magnitude.
- Vehicle 5: Change in response over time.
 - SOT FE Avg. = 17.80 mpg EOT FE Avg. = 18.55 (+4.2% Inc.)
- Vehicle 7: CO Change in Response over time.
 SOT CO Avg. = 1.26 g/mile EOT CO Avg. = 0.95 (-24.6% Dec.)



Figure 53 Analysis of Emissions Drift

Figure 54 Engine Speed Response Drift



Figure 55 Ignition Timing Response Drift

Analysis of Vehicle Response Drift: SOT → EOT Performance Data US FTP Tests; Tier 2 Emissions Cert Fuel

• Significant (p<0.05) drift for each vehicle with testable data for at least one performance result.

| | | | | p-v | alu | es f | or drift | : | | |
|---------|-----------------|-------|-------|-------|-----|------|----------|-------|-------|----|
| | Vehicle Number | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| Bag3 | Vehice Speed | 0.172 | 0.272 | 0.780 | na | na | 0.203 | 0.160 | 0.615 | na |
| Bag3 | Load | 0.015 | 0.509 | 0.690 | na | na | 0.904 | 0.632 | 0.873 | na |
| Bag3 | Ignition Timing | 0.527 | 0.353 | 0.058 | na | na | 0.669 | 0.130 | 0.187 | na |
| Bag3 | ExPreCatAvg | 0.210 | 0.016 | 0.451 | na | na | 0.049 | 0.077 | na | na |
| Bag3 | CatMidCatAvg | 0.815 | 0.021 | 0.071 | na | na | 0.117 | 0.569 | na | na |
| Bags1&2 | Vehice Speed | 0.814 | 0.639 | 0.233 | na | na | 0.731 | 0.018 | 0.012 | na |
| Bags1&2 | Load | 0.207 | 0.238 | 0.508 | na | na | 0.863 | 0.886 | 0.962 | na |
| Bags1&2 | Ignition Timing | 0.279 | 0.675 | 0.913 | na | na | 0.914 | 0.054 | 0.395 | na |
| Bags1&2 | ExPreCatAvg | 0.114 | 0.844 | 0.230 | na | na | 0.071 | 0.014 | na | na |
| Bags1&2 | CatMidCatAvg | 0.432 | 0.963 | 0.035 | na | na | 0.160 | 0.227 | na | na |

Figure 56 Vehicle Performance Testing Analysis of Drift from SOT to EOT



j. Individual Vehicle FE, CO₂, and CO Percent Change Data

Figure 57 Individual Vehicle Fuel Economy Percent Change when moving from 87 to 85 AKI Fuel



Figure 58 Individual Vehicle CO₂ Percent Change when moving from 87 to 85 AKI Fuel



Figure 59 Individual Vehicle CO Percent Change when moving from 87 to 85 AKI Fuel

k. Vehicle Emissions Data – Core Data (85 and 87 AKI)

| VNumber | Altitude | Fuel | TestCycle | TestID | TestDate | THC | CH4 | NonMethane | со | Nox | CO2 | FE | NMOG |
|---------|----------|--------|-----------|-------------|------------|----------|----------|------------|----------|----------|----------|---------|----------|
| | (ft) | | | | | (g/mile) | (g/mile) | (g/mile) | (g/mile) | (g/mile) | (g/mile) | (mpg) | (g/mile) |
| 1 | 5,000 | 87 E10 | US FTP | MS34008535 | 9/11/2013 | 0.0230 | 0.0028 | 0.0204 | 0.1090 | 0.0047 | 219.8340 | 37.7864 | 0.0212 |
| 1 | 5,000 | 87 E10 | LA92 | MS34008536 | 9/11/2013 | 0.0044 | 0.0017 | 0.0028 | 0.4300 | 0.0010 | 235.6490 | 35.1861 | 0.0029 |
| 1 | 5,000 | 87 E10 | US06 | MS34008537 | 9/11/2013 | 0.0199 | 0.0054 | 0.0148 | 3.6782 | 0.0185 | 245.5540 | 33.0789 | 0.0154 |
| 1 | 5,000 | 87 E10 | US FTP | MS34008541 | 9/12/2013 | 0.0260 | 0.0031 | 0.2312 | 0.1552 | 0.0052 | 223.0740 | 37.2246 | 0.0284 |
| 1 | 5,000 | 87 E10 | LA92 | MS34008542 | 9/12/2013 | 0.0039 | 0.0016 | 0.0024 | 0.1797 | 0.0023 | 235.9480 | 35.2005 | 0.0025 |
| 1 | 5,000 | 87 E10 | US06 | MS34008543 | 9/12/2013 | 0.0179 | 0.0047 | 0.0135 | 3.7308 | 0.0180 | 244.0100 | 33.2731 | 0.0141 |
| 1 | 1,000 | 87 E10 | US FTP | MS34008565 | 9/18/2013 | 0.0218 | 0.0031 | 0.0189 | 0.1385 | 0.0051 | 230.1060 | 36.0947 | 0.0197 |
| 1 | 1,000 | 87 E10 | LA92 | MS340008566 | 9/18/2013 | 0.0034 | 0.0015 | 0.0020 | 0.0881 | 0.0015 | 243.6930 | 34.1034 | 0.0021 |
| 1 | 1,000 | 87 E10 | US06 | MS340008567 | 9/18/2013 | 0.0130 | 0.0032 | 0.0100 | 2.0111 | 0.0128 | 250.7260 | 32.7491 | 0.0103 |
| 1 | 1,000 | 87 E10 | US FTP | MS34008574 | 9/19/2013 | 0.0214 | 0.0030 | 0.0186 | 0.1233 | 0.0056 | 229.9390 | 36.1249 | 0.0193 |
| 1 | 1,000 | 87 E10 | LA92 | MS34008575 | 9/19/2013 | 0.0036 | 0.0015 | 0.0022 | 0.1586 | 0.0021 | 243.1560 | 34.1631 | 0.0023 |
| 1 | 1,000 | 87 E10 | US06 | MS34008576 | 9/19/2013 | 0.0118 | 0.0028 | 0.0092 | 1.7285 | 0.0120 | 246.9140 | 33.3079 | 0.0096 |
| 1 | 5,000 | 85 E10 | US FTP | MS34008583 | 9/23/2013 | 0.0240 | 0.0025 | 0.0217 | 0.1386 | 0.0065 | 223.3590 | 37.1511 | 0.0226 |
| 1 | 5,000 | 85 E10 | LA92 | MS34008584 | 9/23/2013 | 0.0035 | 0.0015 | 0.0021 | 0.3704 | 0.0019 | 237.3920 | 34.9131 | 0.0022 |
| 1 | 5,000 | 85 E10 | US06 | MS34008585 | 9/23/2013 | 0.0134 | 0.0042 | 0.0095 | 3.4323 | 0.0078 | 244.5620 | 33.2357 | 0.0099 |
| 1 | 5,000 | 85 E10 | US FTP | MS34008590 | 9/24/2013 | 0.0263 | 0.0034 | 0.0232 | 0.1521 | 0.0056 | 223.8560 | 37.0640 | 0.0241 |
| 1 | 5,000 | 85 E10 | LA92 | MS34008591 | 9/24/2013 | 0.0032 | 0.0012 | 0.0021 | 0.1006 | 0.0005 | 238.3950 | 34.8285 | 0.0022 |
| 1 | 5,000 | 85 E10 | US06 | MS34008592 | 9/24/2013 | 0.0160 | 0.0048 | 0.0116 | 4.5957 | 0.0080 | 247.0240 | 32.6739 | 0.0120 |
| 1 | 1,000 | 85 E10 | US FTP | MS34008653 | 10/1/2013 | 0.0234 | 0.0033 | 0.0203 | 0.1248 | 0.0051 | 228.9860 | 36.2429 | 0.0211 |
| 1 | 1,000 | 85 E10 | LA92 | MS34008654 | 10/1/2013 | 0.0032 | 0.0015 | 0.0019 | 0.3251 | 0.0020 | 244.7850 | 33.8712 | 0.0020 |
| 1 | 1,000 | 85 E10 | US06 | MS34008655 | 10/1/2013 | 0.0127 | 0.0037 | 0.0092 | 3.3260 | 0.0102 | 255.0090 | 31.9233 | 0.0096 |
| 1 | 1,000 | 85 E10 | US FTP | MS34008668 | 10/3/2013 | 0.0340 | 0.0042 | 0.0301 | 0.1915 | 0.0047 | 231.2180 | 35.8723 | 0.0313 |
| 1 | 1,000 | 85 E10 | LA92 | MS34008669 | 10/3/2013 | 0.0161 | 0.0017 | 0.0145 | 0.2466 | 0.0025 | 248.0040 | 33.4439 | 0.0151 |
| 1 | 1,000 | 85 E10 | US06 | MS34008670 | 10/3/2013 | 0.0201 | 0.0034 | 0.0169 | 2.8367 | 0.0081 | 255.6410 | 31.9373 | 0.0176 |
| 2 | 5,000 | 87 E10 | US FTP | MS34008825 | 11/5/2013 | 0.0162 | 0.0029 | 0.0137 | 0.2773 | 0.0035 | 271.5260 | 30.5718 | 0.0142 |
| 2 | 5,000 | 87 E10 | LA92 | MS34008826 | 11/5/2013 | 0.0005 | 0.0006 | 0.0000 | 0.1390 | 0.0003 | 277.2410 | 29.9712 | 0.0000 |
| 2 | 5,000 | 87 E10 | US06 | MS34008827 | 11/5/2013 | 0.0046 | 0.0015 | 0.0033 | 1.3737 | 0.0089 | 276.4490 | 29.8463 | 0.0034 |
| 2 | 5,000 | 87 E10 | US FTP | MS34008839 | 11/7/2013 | 0.0145 | 0.0026 | 0.0126 | 0.2183 | 0.0086 | 266.9410 | 31.1073 | 0.0131 |
| 2 | 5,000 | 87 E10 | LA92 | MS34008840 | 11/7/2013 | 0.0008 | 0.0008 | 0.0001 | 0.4594 | 0.0002 | 276.8800 | 29.9622 | 0.0001 |
| 2 | 5,000 | 87 E10 | US06 | MS34008841 | 11/7/2013 | 0.0045 | 0.0012 | 0.0034 | 0.8442 | 0.0078 | 273.1100 | 30.3000 | 0.0035 |
| 2 | 5,000 | 87 E10 | US FTP | MS34008849 | 11/8/2013 | 0.0129 | 0.0023 | 0.0110 | 0.1932 | 0.0027 | 269.2880 | 30.8416 | 0.0115 |
| 2 | 5,000 | 87 E10 | LA92 | MS34008850 | 11/8/2013 | 0.0005 | 0.0005 | 0.0001 | 0.1424 | 0.0000 | 273.5200 | 30.3780 | 0.0001 |
| 2 | 5,000 | 87 E10 | US06 | MS34008851 | 11/8/2013 | 0.0033 | 0.0010 | 0.0024 | 0.5907 | 0.0061 | 273.9240 | 30.2546 | 0.0025 |
| 2 | 1,000 | 87 E10 | US FTP | MS34008868 | 11/10/2013 | 0.0162 | 0.0033 | 0.0135 | 0.3038 | 0.0013 | 276.0650 | 30.0719 | 0.0148 |
| 2 | 1,000 | 87 E10 | LA92 | MS34008869 | 11/10/2013 | 0.0003 | 0.0003 | 0.0001 | 0.0931 | 0.0012 | 280.0420 | 29.6793 | 0.0001 |
| 2 | 1,000 | 87 E10 | US06 | MS34008870 | 11/10/2013 | 0.0031 | 0.0010 | 0.0022 | 0.6593 | 0.0038 | 275.9040 | 30.0265 | 0.0023 |
| 2 | 1,000 | 87 E10 | LA92 | MS34008878 | 11/12/2013 | 0.0003 | 0.0007 | 0.0000 | 0.1188 | 0.0007 | 281.2040 | 29.5526 | 0.0000 |
| 2 | 1,000 | 87 E10 | US06 | MS34008879 | 11/12/2013 | 0.0033 | 0.0012 | 0.0022 | 0.5813 | 0.0072 | 278.1930 | 29.7934 | 0.0023 |
| 2 | 1,000 | 87 E10 | US FTP | MS34008894 | 11/14/2013 | 0.0334 | 0.0048 | 0.0294 | 0.3670 | 0.0048 | 277.7280 | 29.8695 | 0.0305 |
| 2 | 1,000 | 87 E10 | US FTP | MS34008911 | 11/18/2013 | 0.0152 | 0.0030 | 0.0126 | 0.2498 | 0.0008 | 277.5540 | 29.9139 | 0.0131 |
| 2 | 1,000 | 87 E10 | LA92 | MS34008912 | 11/19/2013 | 0.0003 | 0.0005 | 0.0000 | 0.1005 | 0.0016 | 279.6820 | 29.7163 | 0.0000 |
| 2 | 1,000 | 87 E10 | US06 | MS34008913 | 11/19/2013 | 0.0022 | 0.0008 | 0.0015 | 0.1076 | 0.0118 | 274.5750 | 30.2669 | 0.0015 |
| 2 | 5,000 | 85 E10 | US FTP | MS34008930 | 11/21/2013 | 0.0136 | 0.0027 | 0.0115 | 0.2451 | 0.0037 | 266.6900 | 31.1055 | 0.0119 |
| 2 | 5,000 | 85 E10 | LA92 | MS34008931 | 11/21/2013 | 0.0006 | 0.0004 | 0.0002 | 0.1059 | 0.0028 | 274.3200 | 30.2701 | 0.0002 |
| 2 | 5,000 | 85 E10 | US06 | MS34008932 | 11/21/2013 | 0.0044 | 0.0016 | 0.0029 | 2.4528 | 0.0052 | 273.6760 | 29.9369 | 0.0030 |
| 2 | 5,000 | 85 E10 | US FTP | MS34008941 | 11/22/2013 | 0.0106 | 0.0022 | 0.0085 | 0.1680 | 0.0024 | 267.5020 | 31.0263 | 0.0089 |
| 2 | 5,000 | 85 E10 | LA92 | MS34008942 | 11/22/2013 | 0.0005 | 0.0007 | 0.0000 | 0.1260 | 0.0015 | 276.1220 | 30.0693 | 0.0000 |
| 2 | 5,000 | 85 E10 | US06 | MS34008943 | 11/22/2013 | 0.0051 | 0.0016 | 0.0036 | 2.0738 | 0.0054 | 276.2780 | 29.7218 | 0.0038 |
| 2 | 5,000 | 85 E10 | US FTP | MS35004518 | 11/26/2013 | 0.0249 | 0.0030 | 0.0221 | 0.1824 | 0.0039 | 273.5700 | 30.3317 | 0.0230 |
| 2 | 5,000 | 85 E10 | LA92 | MS35004519 | 11/26/2013 | 0.0119 | 0.0007 | 0.0112 | 0.1211 | 0.0023 | 278.9880 | 29.7578 | 0.0117 |
| 2 | 5,000 | 85 E10 | US06 | MS35004520 | 11/26/2013 | 0.0086 | 0.0016 | 0.0071 | 1.6365 | 0.0084 | 284.6480 | 28.9257 | 0.0074 |
| 2 | 1,000 | 85 E10 | US FTP | MS35004534 | 11/27/2013 | 0.0186 | 0.0033 | 0.0156 | 0.1952 | 0.0014 | 279.0010 | 29.7418 | 0.0162 |
| 2 | 1,000 | 85 E10 | LA92 | MS35004535 | 11/27/2013 | 0.0063 | 0.0008 | 0.0056 | 0.0895 | 0.0005 | 281.1800 | 29.5329 | 0.0058 |
| 2 | 1,000 | 85 E10 | US06 | MS35004536 | 11/27/2013 | 0.0060 | 0.0014 | 0.0047 | 1.2280 | 0.0063 | 283.3950 | 29.1186 | 0.0049 |
| 2 | 1,000 | 85 E10 | US FTP | MS34008988 | 12/5/2013 | 0.0329 | 0.0045 | 0.0288 | 0.3333 | 0.0033 | 278.0580 | 29.8148 | 0.0300 |
| 2 | 1,000 | 85 E10 | LA92 | MS34008989 | 12/5/2013 | 0.0005 | 0.0005 | 0.0002 | 0.0976 | 0.0004 | 280.9870 | 29.5537 | 0.0002 |
| 2 | 1,000 | 85 E10 | US06 | MS34008990 | 12/5/2013 | 0.0030 | 0.0010 | 0.0021 | 0.8033 | 0.0020 | 277.3190 | 29.8244 | 0.0021 |
| 2 | 1,000 | 85 E10 | US FTP | MS34008998 | 12/6/2013 | 0.0229 | 0.0038 | 0.0198 | 0.2908 | 0.0017 | 278.8810 | 29.7372 | 0.0206 |
| 2 | 1,000 | 85 E10 | LA92 | MS34008999 | 12/6/2013 | 0.0004 | 0.0005 | 0.0001 | 0.0923 | 0.0012 | 282.0840 | 29.4398 | 0.0001 |
| 2 | 1,000 | 85 E10 | US06 | MS34009000 | 12/6/2013 | 0.0040 | 0.0017 | 0.0024 | 1.4598 | 0.0082 | 276.9410 | 29.7543 | 0.0025 |

| (ff) reg (g/mile) (g/m | VNumber | Altitude | Fuel | TestCycle | TestID | TestDate | THC | CH4 | NonMethane | со | Nox | CO2 | FE | NMOG |
|--|---------|----------|--------|-----------|--------------|------------|----------|----------|------------|----------|----------|----------|---------|----------|
| S. 5000 8FT0 USTP MS4008822 11/1/2/031 0.0028 0.0014 8FS00 11.116 0.0274 0.0034 164.300 14.429 0.0044 S. 5000 8F101 USIN MS4008823 11/1/2/031 0.0019 1.225 0.0077 20.5700 11.116 0.0218 S. 5000 8F101 USIN MS4008863 11/1/2/031 0.0011 0.0016 0.0012 60.118 0.0012 26.118 1.2321 0.0012 26.118 1.2321 0.0012 26.118 1.2321 0.0013 26.119 1.2321 0.0013 26.119 1.2321 0.0013 26.119 1.2321 0.0013 26.119 1.2321 0.0013 26.119 1.2321 0.0013 26.119 1.2321 0.0013 26.119 1.2321 0.0013 26.119 1.2321 0.0013 26.119 1.2321 0.0013 26.119 1.2321 0.0013 26.119 1.2321 0.0015 27.1791 28.109 1.106 1.0017 1.0003 1.0 | | (ft) | | | | | (g/mile) | (g/mile) | (g/mile) | (g/mile) | (g/mile) | (g/mile) | (mpg) | (g/mile) |
| S | 3 | 5.000 | 85 E10 | US FTP | MS34008822 | 11/5/2013 | 0.0249 | 0.0022 | 0.0228 | 0.1074 | 0.0154 | 266.7820 | 31.1161 | 0.0237 |
| 3 5,000 85:101 5,077 7,072 5,04455 6,0002 3 5,000 85:101 LAP2 M53008837 11///2101 0.0012 0.0005 0.0021 0.0021 0.0021 0.0021 0.0007 26:7003 31:11 0.033 5 35:000 85:101 US6 M53008884 11///2101 0.0014 0.0012 0.0021 0.0012 0.0021 0.0021 0.0021 0.0021 0.0012 0.0021 0.0012 0.0011 0.0019 0.0019 0.0012 0.0011 0.0014 0.0012 0.0011 0.0014 0.0012 0.0011 0.0014 0.0012 0.0011 0.0014 0.0014 0.0012 0.0011 0.0014 0.0014 0.0014 0.0014 | 3 | 5.000 | 85 E10 | LA92 | MS34008823 | 11/5/2013 | 0.0012 | 0.0009 | 0.0004 | 0.0289 | 0.0031 | 264.3100 | 31,4299 | 0.0004 |
| 3 5,000 85101 10/2/10 10/2/10 00135 012/3 00007 265110 13/3 3 5,000 85101 10/5 M53008888 11/2/1011 00037 00066 0.0007 265110 13/371 00071 25110 13/371 00071 25110 13/371 00071 25110 13/371 00071 25110 13/371 00010 00131 25110 13/371 00010 00131 25110 13/371 00001 00131 25110 13/371 00001 00016 0.0002 13/371 0.0001 0.0002 <t< td=""><td>3</td><td>5.000</td><td>85 E10</td><td>US06</td><td>MS34008824</td><td>11/5/2013</td><td>0.0031</td><td>0.0013</td><td>0.0019</td><td>1.2255</td><td>0.0047</td><td>270.9720</td><td>30.4455</td><td>0.0020</td></t<> | 3 | 5.000 | 85 E10 | US06 | MS34008824 | 11/5/2013 | 0.0031 | 0.0013 | 0.0019 | 1.2255 | 0.0047 | 270.9720 | 30.4455 | 0.0020 |
| 3 5:000 85:101 Vis2 Mis2 0:006 0:006 0:007 1:001 25:150 3:34:46 0:000 3 5:000 85:101 US Mis3008882 11/7/2013 0:0041 0:0021 0:011 25:1503 27:224 0:035 3 5:000 85:101 US Mis3008842 11/7/2013 0:007 0:0021 0:024 0:0015 26:13103 3:30:0 0:0015 26:13103 3:30:0 0:0017 3:30:000 0:0016 0:0016 0:0016 0:0016 0:0016 0:0016 0:0016 0:0016 0:0016 0:0007 0:0000 0:0001 0:0001 0:0001 0:0001 0:0001 0:0001 0:0016 0:0007 0:0000 0:0011 0:0012 0:0001 0:0001 0:0011 0:0012 0:0011 0:0012 0:0011 0:0012 0:0011 0:0012 0:0011 0:0012 0:0011 0:0012 0:0011 0:0011 0:0011 0:0011 0:0011 0:0011 0:0011 <td>3</td> <td>5.000</td> <td>85 F10</td> <td>US FTP</td> <td>MS34008836</td> <td>11/6/2013</td> <td>0.0337</td> <td>0.0026</td> <td>0.0315</td> <td>0.1243</td> <td>0.0130</td> <td>266.7700</td> <td>31,1113</td> <td>0.0328</td> | 3 | 5.000 | 85 F10 | US FTP | MS34008836 | 11/6/2013 | 0.0337 | 0.0026 | 0.0315 | 0.1243 | 0.0130 | 266.7700 | 31,1113 | 0.0328 |
| 3 5:000 85:101 US6 NS34008882 11/7/2013 0.0073 0.0074 0.0024 1.2231 0.0013 254.1800 3.1.207 0.0013 3 5:000 85:101 US6 MS34008842 11/7/2013 0.0031 0.0012 0.0028 0.0013 254.1800 31.007 0.0003 20.012 0.0028 0.0013 254.1803 31.020 0.0013 25.101 S1.77 0.0013 31.000 85:101 US6 MS4008864 11/10/2013 0.0014 0.0005 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0007 0.0008 0.0007 0.0008 0.0007 0.0008 0.0007 0.0008 0.0007 0.0008 0.0007 0.0008 0.0007 0.0008 0.0007 0.0008 0.0007 0.0008 0.0007 0.0008 0.0008 0.0008 0.0008 0.0007 0.0008 0.0008 0.0007 0.0008 | 3 | 5.000 | 85 F10 | 1A92 | MS34008837 | 11/6/2013 | 0.0012 | 0.0006 | 0.0006 | 0.0261 | 0.0007 | 265.1180 | 31.3346 | 0.0006 |
| 3 5 000 85:10 USA 10/2013 0.0012 0.0012 0.0115 201.13 201.14 201.14 201.13 201.14 201.14 201.14 201.14 201.14 201.14 201.14 201.14 201.14 201.14 201.14 201.14 201.14 201.14 <th< td=""><td>3</td><td>5,000</td><td>85 F10</td><td>US06</td><td>MS34008838</td><td>11/6/2013</td><td>0.0037</td><td>0.0014</td><td>0.0024</td><td>1 2231</td><td>0.0041</td><td>251 5190</td><td>32 7824</td><td>0.0025</td></th<> | 3 | 5,000 | 85 F10 | US06 | MS34008838 | 11/6/2013 | 0.0037 | 0.0014 | 0.0024 | 1 2231 | 0.0041 | 251 5190 | 32 7824 | 0.0025 |
| 5 5000 5510 L02 L032 L033 L03 | 3 | 5,000 | 85 F10 | LIS FTP | MS34008842 | 11/7/2013 | 0.0641 | 0.0014 | 0.0612 | 0 1489 | 0.0041 | 264 1800 | 31 4005 | 0.0637 |
| 5 6 5 6 6 6 6 6 6 6 6 6 6 | 3 | 5,000 | 85 F10 | 1492 | MS34008843 | 11/7/2013 | 0.0041 | 0.0001 | 0.0012 | 0.1405 | 0.0015 | 265 2110 | 31 3737 | 0.0037 |
| 3 1.000 56 F10 USTP MS3008855 11/10/2013 0.001 0.01132 0.0011 0.01132 0.0011 0.01132 0.0011 0.01132 0.0011 0.0112 0.0111 0.011 | 3 | 5,000 | 85 F10 | 11506 | MS34008844 | 11/7/2013 | 0.0015 | 0.0000 | 0.0026 | 1 217/ | 0.0015 | 203.2110 | 33.0620 | 0.0013 |
| 1 1 0 | 3 | 1,000 | 85 E10 | | MS34008865 | 11/10/2013 | 0.0037 | 0.0012 | 0.0020 | 0.0611 | 0.0025 | 270 0730 | 30 6460 | 0.0027 |
| 1 1 0 85 L0 0.556 0.503 0.5030 0.5582 0.5534 0.0001 275.4653 0.0001 275.4653 0.0003 257.4653 0.0003 257.4653 0.0003 257.4653 0.0003 257.4653 0.0003 257.4653 0.0003 257.4653 0.0003 257.4653 0.0003 257.4653 0.0003 257.4653 0.0013 1.5533 0.0012 0.58510 0.0032 1.55330 0.0012 1.55330 0.0012 <th0< td=""><td>3</td><td>1,000</td><td>85 E10</td><td>1/02</td><td>MS34008866</td><td>11/10/2013</td><td>0.0140</td><td>0.0010</td><td>0.0132</td><td>0.0011</td><td>0.0105</td><td>275 2650</td><td>20 1821</td><td>0.0137</td></th0<> | 3 | 1,000 | 85 E10 | 1/02 | MS34008866 | 11/10/2013 | 0.0140 | 0.0010 | 0.0132 | 0.0011 | 0.0105 | 275 2650 | 20 1821 | 0.0137 |
| 1.000 85 L00 US FTP Mis34008874 11/12/2013 0.0017 0.0020 0.0018 0.0005 27.27.560 0.0066 0.0018 3 1.000 85 L10 US FTP Mis34008875 11/12/2013 0.0021 0.0000 0.0129 0.0005 27.57.601 3.0064 0.0001 0.0012 0.0001 0.0012 0.0001 0.0012 0.0001 27.57.001 3.0015 0.0017 0.0024 0.0017 0.0088 2.07.664 3.3.600 85 L10 US FTP Mis34008893 11/14/2013 0.0007 0.0000 0.0021 0.0284 0.0024 0.0172 26.56408 3.1.80 0.0264 0.0177 0.1034 0.0017 25.5640 3.1.80 0.0264 0.0011 0.0284 0.0012 25.5610 3.1.1114 0.0013 0.0021 0.0217 0.1034 0.0012 25.5610 3.1.000 87.510 4.984 1.12/2/2013 0.0044 0.0021 1.0224 5.5610 3.776 3.4690 0.0045 0.0022 0.0224 | 2 | 1,000 | 05 E10 | | MS2400860 | 11/10/2013 | 0.0004 | 0.0000 | 0.0000 | 0.6162 | 0.0015 | 273.2030 | 20 0070 | 0.0000 |
| 1 1 0 8 1 0 | 3 | 1,000 | 85 E10 | | MS34008807 | 11/10/2013 | 0.0019 | 0.0009 | 0.0011 | 0.0102 | 0.0027 | 277.7700 | 29.0079 | 0.0011 |
| 3 1,000 85:10 US2 Instances 11/12/2013 0.002 0.000 0.0002 25:73/40 22:0440 0.0001 3 1,000 85:10 USC IV 0.001 0.0021 0.0021 0.0071 127:53:00 30:1574 0.0184 0.0005 3 1,000 85:10 USC IV 0.0006 0.0002 0.0221 0.0005 22:53:695 32:8:695 32:8:695 32:8:695 32:8:695 32:7:566 0.0023 3 5,000 87:10 USC MS4008928 11/21/2013 0.0004 0.0002 0.0221 1.27:43 0.0048 22:8:50 31:0008 0.0022 1.27:2013 0.0005 0.0005 0.0004 22:8:50 31:0008 22:8:50 31:0008 22:8:50 31:0008 22:8:50 31:0008 22:8:50 31:0008 22:8:50 31:0008 22:8:50 31:0008 22:8:50 31:0008 22:8:50 31:0008 22:8:50 31:0008 22:8:50 31:0008 22:8:50 <td>2</td> <td>1,000</td> <td>05 L10</td> <td></td> <td>MC2400874</td> <td>11/11/2013</td> <td>0.0177</td> <td>0.0020</td> <td>0.0101</td> <td>0.0978</td> <td>0.0093</td> <td>272.3020</td> <td>20 1664</td> <td>0.0108</td> | 2 | 1,000 | 05 L10 | | MC2400874 | 11/11/2013 | 0.0177 | 0.0020 | 0.0101 | 0.0978 | 0.0093 | 272.3020 | 20 1664 | 0.0108 |
| 3 1,000 85 F10 US306 MV3306887 11/1/2/2013 0.0012 0.0012 0.0031 27.5300 30.172 3 1,000 85 F10 LAS2 MV34008892 11/1/2/2013 0.0007 0.0006 0.0001 275.660 30.1386 0.0001 3 1,000 85 F10 US5 MV34008892 11/21/2013 0.0009 0.0001 0.6687 0.0008 253.6690 31.3019 0.0000 3 5,000 87 F10 US6 MV34008928 11/21/2013 0.0024 0.0007 256.6120 31.3019 0.0000 3 5,000 87 F10 US6 MV34008928 11/21/2013 0.0025 0.0226 1.213 0.0000 0.0006 0.0004 0.0226 262.850 31.600 0.026 262.850 31.600 0.026 262.850 31.600 276.860 0.024 0.0228 262.870 31.900 31.900 31.900 31.900 31.900 31.900 31.900 31.9000 31.9000 | 2 | 1,000 | 05 E10 | LA9Z | IVI334006673 | 11/12/2013 | 0.0005 | 0.0007 | 0.0000 | 0.0159 | 0.0009 | 275.4050 | 30.1004 | 0.0000 |
| 3 1,000 85 L10 LSP MS3008881 11/14/2013 0.024 0.0071 12/3500 0.0071 12/3500 0.0071 12/3500 0.0071 12/3500 0.0071 12/3500 0.0071 12/3500 0.0071 12/3500 0.0058 12/3500 0.0058 12/3500 0.0058 12/3500 0.0058 12/3500 0.0058 12/3500 0.0058 12/3500 0.0058 12/3500 0.0058 12/3500 0.0058 0.0058 0.0058 0.0058 0.0058 0.0058 0.0058 0.0058 0.0058 0.0058 0.0058 0.0014 0.0028 0.0028 0.0028 0.0014 0.0028 0.0014 0.0028 0.0014 0.0028 0.0011 0.0018 0.00113 | 2 | 1,000 | 05 E10 | | NIS34008870 | 11/12/2013 | 0.0022 | 0.0010 | 0.0012 | 0.0021 | 0.0051 | 257.5740 | 32.0044 | 0.0015 |
| 3 1,000 85 F10 US2 IN34008822 11/14/2013 0.0007 0.0008 0.0011 2/2.6489 30.1380 0.0017 3 5,000 87 F10 USTP MS4008927 11/21/2013 0.0023 0.0006 0.0001 0.0034 0.0007 253.6890 31.5184 0.0225 3 5,000 87 F10 US06 MS34008929 11/21/2013 0.0004 0.0006 0.0000 0.0034 0.0006 256.5120 31.3100 0.0026 52.6520 31.300 0.026 52.6520 31.300 0.0026 52.6520 31.600 0.0004 0.0276 0.0286 0.0206 52.6520 31.600 31.600 87.100 US47 MS4008939 11/22/2013 0.0004 0.0028 1.0016 27.37000 30.449 0.0024 3 1,000 87.100 US47 MS4008993 12/2/2013 0.0007 0.0006 0.0001 21.6500 30.3679 0.0225 3 1,000 87.101 US65 | 3 | 1,000 | 85 E10 | USFIP | NIS34008891 | 11/14/2013 | 0.0194 | 0.0024 | 0.0177 | 0.0988 | 0.0071 | 275.3010 | 30.1574 | 0.0184 |
| 3 1,000 87:10 USG MS34088927 11/1/4/2013 0.0011 0.0087 0.0088 25.3850 32.6111 0.0011 3 5,000 87:10 USFT MS34008922 11/21/2013 0.0020 0.0021 1.2743 0.0048 25.3850 33.5184 0.0226 3 5,000 87:10 USFT MS34008929 11/22/2013 0.0040 0.0032 0.0226 262.8520 31.6060 0.0296 3 5,000 87:10 USFT MS34008991 11/22/2013 0.0014 0.0024 1.5110 0.0025 25.5703 31.4660 0.0024 3 1,000 87:10 USFT MS34008991 12/3/2013 0.0001 0.0046 0.0382 0.0315 273.5980 30.3679 0.0255 3 1,000 87:10 USFT MS34008991 12/3/2013 0.0001 0.0028 0.0017 273.5980 30.3749 0.0255 3 1,000 87:10 USFT MS34008091 | 3 | 1,000 | 85 E10 | LA9Z | IVIS34008892 | 11/14/2013 | 0.0007 | 0.0006 | 0.0002 | 0.0240 | 0.0016 | 275.6460 | 30.1386 | 0.0002 |
| 3 5_000 87±10 05±10 05±10 0.023 0.0021 0.012 0.0334 0.0002 0.0334 0.0002 0.0334 0.0002 0.0334 0.0002 0.0334 0.0002 0.0334 0.0002 0.0334 0.0002 0.0334 0.0002 0.0334 0.0002 0.0334 0.0002 0.0235 0.1330 0.0008 265.8503 3.1508 0.0008 3 5,000 87±10 US6 M534008938 11/21/21013 0.0005 0.0004 0.0235 0.1330 0.0004 263.8740 31.4960 0.0004 3 1,000 87±10 US6 M534008931 11/22/2013 0.0001 0.0006 0.0001 0.0255 0.0933 0.0116 273.5980 30.3679 0.0265 3 1,000 87±10 LA92 M534008992 12/5/2013 0.0001 0.0006 0.0001 0.0278 0.0007 27.0803 30.3490 0.0011 3 1,000 87±10 LA92 M5340089001 | 3 | 1,000 | 85 E10 | | IVIS34008893 | 11/14/2013 | 0.0019 | 0.0009 | 0.0011 | 0.6897 | 0.0058 | 253.6950 | 32.0111 | 0.0011 |
| 3 5,000 87:10 US2 M S4408223 11/21/2013 0.0004 0.0002 1.1733 0.0004 21.033 0.0007 25.8120 3.3.301 0.0000 3 5,000 87:10 USTP MS44088939 11/21/2013 0.0035 0.0025 0.0228 0.0331 0.0026 26.8320 31.6008 0.0235 0.0034 20.029 33 5,000 87:10 USTP MS4408991 11/21/21013 0.0041 0.0024 0.0146 0.0035 20.0029 32.16000 32.4490 0.0152 3 1,000 87:10 USTP MS4408991 12/3/2013 0.0001 0.0090 0.0001 0.0258 0.0939 0.0116 273.5980 36.6479 0.0001 3 1,000 87:10 USFP MS44008991 12/5/2013 0.0007 0.0011 0.388 0.0021 272.6780 36.3740 0.0256 3 1,000 87:10 USFP MS4008901 12/5/2013 0.0007 0.0011 0 | 3 | 5,000 | 87 E10 | USFIP | MS34008927 | 11/21/2013 | 0.0235 | 0.0020 | 0.0217 | 0.1031 | 0.0172 | 263.6080 | 31.5184 | 0.0226 |
| 3 5,000 87E10 US06 MM34008938 11/21/2013 0.0024 0.0285 0.133 0.0026 26.2320 3.6000 0.0226 26.2320 3.6000 0.0226 26.2320 3.6000 0.0226 26.2320 3.6000 0.0226 26.2320 3.6000 0.0226 26.2320 3.0002 26.3740 3.14660 0.0004 3 5,000 87 E10 US06 MS34008990 11/2/2/013 0.0014 0.0028 0.0146 0.0035 251.6700 32.7322 0.0029 3 1,000 87 E10 US06 MS34008991 12/2/2013 0.0027 0.0026 0.0046 0.0011 271.6101 30.6471 0.0026 3 1,000 87 E10 US06 MS34008991 12/5/2013 0.0027 0.0011 0.0258 0.0007 274.0960 3.03440 0.0011 3 1,000 87 E10 US06 MS34009001 12/5/2013 0.0021 0.0111 0.0128 0.0021 274.4080 3.06611 | 3 | 5,000 | 87 E10 | LA92 | MS34008928 | 11/21/2013 | 0.0004 | 0.0006 | 0.0000 | 0.0334 | 0.0007 | 265.6120 | 31.3019 | 0.0000 |
| 3 5,000 87 E10 US FTP MG34008939 11/21/2013 0.0000 0.0004 0.0028 262.85201 31.6008 0.0028 3 5,000 87 E10 US06 MS34008990 11/22/2013 0.0004 0.0028 1.5110 0.0035 273.0000 32.4322 0.0029 3 1,000 87 E10 US FTP MS34008991 12/5/2013 0.0000 0.0046 0.0037 271.610 30.6447 0.0000 3 1,000 87 E10 US FTP MS34008991 12/5/2013 0.0011 0.0028 0.0007 274.0960 30.344 0.0001 3 1,000 87 E10 US FTP MS34009001 12/5/2013 0.0017 0.0001 0.0002 0.0111 0.388 0.0002 274.0860 30.346 0.0201 3 1,000 87 E10 US FTP MS340090001 12/5/2013 0.0002 0.0011 0.4997 0.0021 274.0860 30.6051 0.0002 3 1,0000 | 3 | 5,000 | 87 E10 | US06 | MS34008929 | 11/21/2013 | 0.0034 | 0.0013 | 0.0022 | 1.2743 | 0.0048 | 251.8550 | 32.7566 | 0.0023 |
| 3 5,000 87 F10 LA92 MtS3400893 11/22/013 0.0005 0.0004 0.0028 1.5110 0.0035 21.5703 23.322 0.0023 3 1,000 87 F10 USGE MtS34008991 12/3/2013 0.0014 0.0024 0.0146 0.0355 27.30003 03.4491 0.0103 3 1,000 87 F10 LA92 MtS4008991 12/3/2013 0.0024 0.0225 0.0993 0.0116 27.35980 03.677 0.0265 3 1,000 87 F10 LA92 MtS4008992 12/3/2013 0.0017 0.0001 0.0288 0.0002 27.4.0980 03.344 0.0021 3 1,000 87 F10 LS96 MtS4009002 12/6/2013 0.0021 0.0219 0.1117 0.128 0.0012 274.0820 03.0344 0.0228 3 1,000 87 F10 LA92 MtS4009001 12/6/2013 0.0021 0.0219 0.0112 174.9803 0.0651 0.0020 0.021 1 | 3 | 5,000 | 87 E10 | US FTP | MS34008938 | 11/21/2013 | 0.0305 | 0.0025 | 0.0285 | 0.1330 | 0.0206 | 262.8520 | 31.6008 | 0.0296 |
| 3 5,000 87 E10 US60 MS34008940 11/22/2013 0.0014 0.0014 0.0034 0.0014 0.0035 251.6700 32,7322 0.0025 3 1,000 87 E10 LA92 MS340089971 12/3/2013 0.0070 0.0009 0.0000 0.0146 0.0037 20.0005 27.11.610 30.6647 0.0000 3 1,000 87 E10 LSF P MS34008991 12/5/2013 0.0001 0.0006 0.0001 0.028 0.0002 7.0996 30.3440 0.0011 3 1,000 87 E10 LSF P MS340089901 12/5/2013 0.0007 0.0011 0.0123 27.40820 30.334 0.0228 3 1,000 87 E10 LS92 MS34009001 12/6/2013 0.0002 0.0181 0.0012 27.5400 30.1340 0.0228 3 5,000 87 E10 LS92 MS34009001 12/9/2013 0.0026 0.0354 0.0221 25.4000 3.0325 0.0024 4.5500 | 3 | 5,000 | 87 E10 | LA92 | MS34008939 | 11/22/2013 | 0.0009 | 0.0005 | 0.0004 | 0.0279 | 0.0048 | 263.9740 | 31.4969 | 0.0004 |
| 3 1,000 87 E10 US FTP MS34008991 12/3/2013 0.0002 0.0164 0.0020 0.0000 0.0016 0.0017 0.0000 0.0116 0.0017 0.0000 0.0116 0.0017 0.0000 0.0016 0.0017 0.0000 0.0116 0.0017 0.0000 0.0116 0.0017 0.0000 0.0116 0.0017 0.0000 0.0011 0.0000 0.0011 0.0000 0.0011 0.0000 0.0011 0.0000 0.0011 0.0000 0.0011 0.0012 0.0113 0.0113 0.0113 0.0113 0.0113 | 3 | 5,000 | 87 E10 | US06 | MS34008940 | 11/22/2013 | 0.0041 | 0.0014 | 0.0028 | 1.5110 | 0.0035 | 251.6700 | 32.7322 | 0.0029 |
| 3 1,000 87 F10 LAS2 MS34008971 12/3/2013 0.0007 0.0000 0.01146 0.0017 271.1610 30.6647 0.0000 3 1,000 87 F10 LAS2 MS34008991 12/5/2013 0.0074 0.0025 0.0093 0.0116 273.5980 30.3344 0.0001 3 1,000 87 F10 LS6 MS34008993 12/5/2013 0.0027 0.0011 0.3898 0.0022 272.0780 30.4950 0.0011 3 1,000 87 F10 LS6 MS34009900 12/6/2013 0.0027 0.0011 0.4997 0.0012 274.6820 30.6561 0.0000 3 1,000 87 F10 LS6 MS34009000 12/9/2013 0.0026 0.0022 0.0304 0.0022 6.6880 3.1275 0.0024 0.334 0.0024 0.0324 0.0354 0.0024 0.344 0.0024 0.344 0.0025 0.0042 0.334 0.0225 0.0034 0.0025 0.0024 0.0021 0. | 3 | 1,000 | 87 E10 | US FTP | MS34008969 | 12/3/2013 | 0.0164 | 0.0020 | 0.0146 | 0.0362 | 0.0155 | 273.0000 | 30.4491 | 0.0152 |
| 3 1,000 87 E10 US F17 MS34008991 12/5/2013 0.0274 0.0225 0.0993 0.0116 273.5800 30.3679 0.0265 3 1,000 87 E10 US66 MS34008992 12/5/2013 0.0007 0.0011 0.3898 0.0002 274.0969 30.344 0.0001 3 1,000 87 E10 US66 MS34008901 12/6/2013 0.0027 0.0011 0.1117 0.012 274.0969 30.3134 0.0228 3 1,000 87 E10 US66 MS34009001 12/6/2013 0.0005 0.0000 0.0111 0.4997 0.0021 275.4100 30.1080 0.0002 3 5,000 87 E10 US66 MS34009010 12/9/2013 0.0088 0.0002 0.0026 247.5808 33.3925 0.0026 247.5808 33.3925 0.0026 247.5808 33.3925 0.0026 247.5808 33.3925 0.0026 247.5808 33.3925 0.0026 247.5808 33.3925 0.0021 37 | 3 | 1,000 | 87 E10 | LA92 | MS34008971 | 12/3/2013 | 0.0007 | 0.0009 | 0.0000 | 0.0146 | 0.0017 | 271.1610 | 30.6647 | 0.0000 |
| 3 1,000 87 E10 L492 M534008992 12/5/2013 0.0007 0.0001 0.0288 0.0007 274.0960 30.3344 0.0001 3 1,000 87 E10 US FTP M534008993 12/5/2013 0.0027 0.0002 0.0111 0.0122 274.0980 30.4950 0.0012 3 1,000 87 E10 US FTP M534009002 12/6/2013 0.0026 0.0000 0.0111 0.1297 0.0021 274.6401 30.0501 0.0000 3 1,000 87 E10 US FTP M534009001 12/9/2013 0.0028 0.0022 0.0334 0.0026 265.8820 31.3705 0.0002 3 5,000 87 E10 US FTP M534009011 12/9/2013 0.0003 0.0021 0.9259 0.0026 265.8820 31.3705 0.0002 4 5,000 85 E10 US FTP M534020901 12/9/2013 0.0055 0.0434 0.3925 0.0076 33.3340 0.3025 0.0143 0.0227 | 3 | 1,000 | 87 E10 | US FTP | MS34008991 | 12/5/2013 | 0.0274 | 0.0024 | 0.0255 | 0.0993 | 0.0116 | 273.5980 | 30.3679 | 0.0265 |
| 3 1,000 87 E10 US66 M534008993 12/5/2013 0.0007 0.0011 0.3898 0.0028 272.0780 30.4350 0.0011 3 1,000 87 E10 US FTP M534009002 12/6/2013 0.0024 0.0219 0.1117 0.0123 274.0802 30.3134 0.0020 3 1,000 87 E10 US6FT M534009002 12/6/2013 0.0021 0.0021 0.0121 0.75.4100 30.1080 0.0012 3 5,000 87 E10 US6F M534009010 12/9/2013 0.0085 0.0021 0.0252 0.0034 0.0026 265.8820 31.12 0.056 3 5,000 87 E10 US66 M534009011 12/9/2013 0.0035 0.0021 0.2223 0.0016 53.93406 23.1705 0.0024 4 5,000 85 E10 US6 M53409011 12/9/2014 0.0040 0.5833 0.3325 0.0026 247.5680 3.3925 0.0024 4 5,000 85 | 3 | 1,000 | 87 E10 | LA92 | MS34008992 | 12/5/2013 | 0.0001 | 0.0006 | 0.0001 | 0.0258 | 0.0007 | 274.0960 | 30.3344 | 0.0001 |
| 3 1,000 87 E10 US FTP MS34009001 12/6/2013 0.0027 0.0046 0.0111 0.0112 274.0820 3.3.134 0.0200 3 1,000 87 E10 US66 MS34009002 12/6/2013 0.0005 0.0001 0.0111 0.4997 0.0021 275.4100 30.1080 0.0012 3 5,000 87 E10 US FTP MS34009003 12/9/2013 0.0007 0.0011 0.4997 0.0022 275.4100 30.1322 0.0262 3 5,000 87 E10 US FTP MS34009010 12/9/2013 0.0008 0.0007 0.0021 0.0026 275.860 33.322 0.0026 275.860 33.325 0.0024 275.860 33.325 0.0024 275.860 33.325 0.0024 21.577 0.0022 4 5,000 85 E10 US FTP 7632502 1/14/2014 0.0026 0.0040 0.5857 0.0029 391.574 21.1968 0.0042 4 5,000 85 E10 US FTP | 3 | 1,000 | 87 E10 | US06 | MS34008993 | 12/5/2013 | 0.0017 | 0.0007 | 0.0011 | 0.3898 | 0.0028 | 272.0780 | 30.4950 | 0.0011 |
| 3 1,000 87 E10 LA92 MS34009002 12/6/2013 0.0005 0.0007 0.0011 0.0012 271.6840 30.6051 0.0001 3 1,000 87 E10 US FTP MS34009009 12/9/2013 0.0221 0.0222 0.0930 0.0011 277.470 31.022 0.021 0.0225 0.0930 0.0012 275.4100 30.1080 0.0021 0.0225 0.0930 0.0012 275.4703 31.020 0.0226 255.8820 31.2705 0.0002 0.033 0.0076 359.346 23.1705 0.0024 4.00025 255.8820 31.2705 0.0024 4.022 0.0076 359.346 23.1131 0.0564 0.0023 0.0221 0.0015 37.2344 25.577 0.0022 4.5000 85 E10 US FTP 7632502 1/14/2014 0.0024 0.0021 0.2223 0.0015 37.2344 25.577 0.0022 4.5000 85 E10 US 66 7632515 1/15/2014 0.0024 0.0023 0.0001 0.0113 36.774 <td>3</td> <td>1,000</td> <td>87 E10</td> <td>US FTP</td> <td>MS34009001</td> <td>12/6/2013</td> <td>0.0237</td> <td>0.0024</td> <td>0.0219</td> <td>0.1117</td> <td>0.0123</td> <td>274.0820</td> <td>30.3134</td> <td>0.0228</td> | 3 | 1,000 | 87 E10 | US FTP | MS34009001 | 12/6/2013 | 0.0237 | 0.0024 | 0.0219 | 0.1117 | 0.0123 | 274.0820 | 30.3134 | 0.0228 |
| 3 1,000 87 E10 US66 MS34009003 12/6/2013 0.0018 0.0007 0.0011 0.4997 0.0021 275.4100 30.1080 0.0012 3 5,000 87 E10 USFTP MS34009001 12/9/2013 0.0008 0.0007 0.0020 0.0304 0.0026 265.8820 31.2705 0.0002 3 5,000 87 E10 USG MS34009011 12/9/2013 0.0008 0.0013 0.0223 0.0262 247.5680 33.3925 0.0024 4 5,000 85 E10 USFTP 7632502 1/14/2014 0.0026 0.0005 0.0021 0.2223 0.0015 372.2304 22.577 0.0022 4 5,000 85 E10 US66 7632502 1/14/2014 0.0024 0.023 0.0011 0.4927 0.0113 362.6174 22.9108 0.0014 4 5,000 85 E10 LA92 7632515 1/15/2014 0.0024 0.0023 0.0001 0.4136.7183 22.8737 0.0 | 3 | 1,000 | 87 E10 | LA92 | MS34009002 | 12/6/2013 | 0.0005 | 0.0006 | 0.0000 | 0.0181 | 0.0010 | 271.6840 | 30.6051 | 0.0000 |
| 3 5,000 87 E10 US FTP MS34009009 12/9/2013 0.0268 0.0021 0.0252 0.0930 0.0151 267.7470 31.0322 0.0262 3 5,000 87 E10 LA92 MS34009010 12/9/2013 0.0008 0.0001 0.0020 0.0304 0.0022 267.580 33.3925 0.0002 4 5,000 85 E10 US6F T632502 1/14/2014 0.0005 0.0005 0.0021 0.2223 0.0015 372.304 22.5177 0.0022 4 5,000 85 E10 US6F T632502 1/14/2014 0.0026 0.0005 0.0011 0.5877 0.0023 9.15742 21.1968 0.0042 4 5,000 85 E10 US6F T632515 1/15/2014 0.0023 0.0001 0.1964 0.011 367.172 22.8737 0.0011 4 1,000 85 E10 US6F T632525 1/16/2014 0.0012 0.0051 0.0013 364.0772 2.2.8737 0.0001 <td>3</td> <td>1,000</td> <td>87 E10</td> <td>US06</td> <td>MS34009003</td> <td>12/6/2013</td> <td>0.0018</td> <td>0.0007</td> <td>0.0011</td> <td>0.4997</td> <td>0.0021</td> <td>275.4100</td> <td>30.1080</td> <td>0.0012</td> | 3 | 1,000 | 87 E10 | US06 | MS34009003 | 12/6/2013 | 0.0018 | 0.0007 | 0.0011 | 0.4997 | 0.0021 | 275.4100 | 30.1080 | 0.0012 |
| 3 5,000 87 E10 LA92 MS34009010 12/9/2013 0.0008 0.0007 0.0002 0.0344 0.0022 20.304 0.0022 247.5680 33.3925 0.0002 4 5,000 85 E10 US 6FTP 7632502 1/14/2014 0.0005 0.0051 0.3223 0.0015 359.3406 23.1131 0.0052 4 5,000 85 E10 US 6 7632502 1/14/2014 0.0026 0.0005 0.0021 0.2223 0.0013 372.2304 22.5577 0.0022 4 5,000 85 E10 US 6 7632502 1/14/2014 0.0023 0.0001 0.5857 0.0023 31.5742 21.1968 0.0042 4 5,000 85 E10 US FTP 7632515 1/15/2014 0.0024 0.0023 0.0011 366.1713 22.8737 0.0011 4 1,000 85 E10 US 6 7632525 1/16/2014 0.0012 0.0016 0.0273 32.4781 21.6653 0.0021 | 3 | 5,000 | 87 E10 | US FTP | MS34009009 | 12/9/2013 | 0.0268 | 0.0021 | 0.0252 | 0.0930 | 0.0151 | 267.7470 | 31.0322 | 0.0262 |
| 3 5,000 87 E10 US06 MS34009011 12/9/2013 0.0035 0.0013 0.0023 0.9259 0.0026 247.5680 33.3925 0.0024 4 5,000 85 E10 US FTP 7632502 1/14/2014 0.0005 0.0021 0.2223 0.0015 372.2304 22.5577 0.0022 4 5,000 85 E10 US FTP 7632502 1/14/2014 0.0048 0.0005 0.0040 0.5857 0.0021 372.304 22.5577 0.0022 4 5,000 85 E10 US FTP 7632515 1/15/2014 0.0042 0.0023 0.0011 0.118 362.174 22.9108 0.0501 4 5,000 85 E10 US FTP 7632515 1/15/2014 0.0047 0.0028 0.0011 0.1014 366.713 22.8737 0.0001 4 1,000 85 E10 US FTP 7632525 1/16/2014 0.0001 0.0025 0.0012 371.6965 22.780 0.0001 4 | 3 | 5,000 | 87 E10 | LA92 | MS34009010 | 12/9/2013 | 0.0008 | 0.0007 | 0.0002 | 0.0304 | 0.0026 | 265.8820 | 31.2705 | 0.0002 |
| 4 5,000 85 E10 US FTP 7632502 1/14/2014 0.0606 0.0056 0.0043 0.3925 0.0076 359.3406 23.1131 0.0565 4 5,000 85 E10 LA92 7632502 1/14/2014 0.0008 0.0001 0.2223 0.0015 372.2304 22.557 0.0022 4 5,000 85 E10 US06 7632515 1/15/2014 0.0023 0.0001 0.1964 0.0011 362.6174 22.9108 0.0001 4 5,000 85 E10 US66 7632515 1/15/2014 0.0024 0.0023 0.0001 0.1964 0.0011 366.7183 22.8737 0.0011 4 5,000 85 E10 US66 7632525 1/16/2014 0.0012 0.0036 0.0001 30.0055 0.0032 31.0027 382.4781 21.6653 0.0021 4 1,000 85 E10 US66 7632525 1/16/2014 0.0001 0.2051 0.0012 31.4652 0.3204 2.3.662 | 3 | 5,000 | 87 E10 | US06 | MS34009011 | 12/9/2013 | 0.0035 | 0.0013 | 0.0023 | 0.9259 | 0.0026 | 247.5680 | 33.3925 | 0.0024 |
| 4 5,000 85 E10 LA92 7632502 1/14/2014 0.0026 0.0005 0.0021 0.2223 0.0015 372.234 22.557 0.0022 4 5,000 85 E10 US6F 7632502 1/14/2014 0.0048 0.0040 0.5857 0.0029 391.5742 21.1968 0.0042 4 5,000 85 E10 US FTP 7632515 1/15/2014 0.0024 0.0010 0.1964 0.0014 366.7183 22.8737 0.0001 4 5,000 85 E10 US FTP 7632515 1/15/2014 0.0047 0.0028 0.0018 0.4750 0.0014 366.7183 22.8737 0.0001 4 1,000 85 E10 US FTP 7632525 1/16/2014 0.0007 0.0022 0.6176 0.0027 382.4781 21.6968 0.0002 4 1,000 85 E10 US FTP 7632541 1/17/2014 0.0002 0.6176 0.0027 382.4781 21.6968 0.0003 4 | 4 | 5,000 | 85 E10 | US FTP | 7632502 | 1/14/2014 | 0.0600 | 0.0056 | 0.0543 | 0.3925 | 0.0076 | 359.3406 | 23.1131 | 0.0565 |
| 4 5,000 85 E10 US06 7632502 1/14/2014 0.0048 0.0088 0.0040 0.5857 0.0029 391.5742 21.1968 0.0042 4 5,000 85 E10 US FTP 7632515 1/15/2014 0.0033 0.0010 0.1964 0.0011 362.6174 22.9108 0.0511 4 5,000 85 E10 US6 7632515 1/15/2014 0.0024 0.0018 0.4750 0.0011 366.7183 22.8737 0.0011 4 1,000 85 E10 US6 7632525 1/16/2014 0.0010 0.0026 0.0305 0.0012 371.6965 22.5780 0.0011 4 1,000 85 E10 US6 7632525 1/16/2014 0.0002 0.0002 0.6176 0.0027 382.4781 21.6968 0.0022 4 1,000 85 E10 US6 7632541 1/17/2014 0.0022 0.0002 0.6176 0.0027 382.4781 21.6968 0.0023 4 1, | 4 | 5,000 | 85 E10 | LA92 | 7632502 | 1/14/2014 | 0.0026 | 0.0005 | 0.0021 | 0.2223 | 0.0015 | 372.2304 | 22.5577 | 0.0022 |
| 4 5,000 85 E10 US FTP 7632515 1/15/2014 0.0533 0.0055 0.0482 0.3210 0.0118 362.6174 22.9108 0.0501 4 5,000 85 E10 LA92 7632515 1/15/2014 0.0023 0.0001 0.1964 0.0014 366.7183 22.8737 0.0001 4 1,000 85 E10 US06 7632515 1/15/2014 0.0047 0.0028 0.0018 0.4750 0.001 384.3272 21.6053 0.019 4 1,000 85 E10 US FTP 7632525 1/16/2014 0.0010 0.0055 0.0011 0.2051 0.0012 371.6965 22.5780 0.0001 4 1,000 85 E10 US FTP 7632541 1/17/2014 0.0022 0.0020 0.6166 0.0027 382.4781 21.6968 0.0022 4 1,000 85 E10 US FTP 7632541 1/17/2014 0.0022 0.0026 0.0003 0.5837 0.0027 382.4868 21.7220 </td <td>4</td> <td>5,000</td> <td>85 E10</td> <td>US06</td> <td>7632502</td> <td>1/14/2014</td> <td>0.0048</td> <td>0.0008</td> <td>0.0040</td> <td>0.5857</td> <td>0.0029</td> <td>391.5742</td> <td>21.1968</td> <td>0.0042</td> | 4 | 5,000 | 85 E10 | US06 | 7632502 | 1/14/2014 | 0.0048 | 0.0008 | 0.0040 | 0.5857 | 0.0029 | 391.5742 | 21.1968 | 0.0042 |
| 4 5,000 85 E10 LA92 7632515 1/15/2014 0.0024 0.0023 0.0001 0.1964 0.0014 366.7183 22.8737 0.0001 4 5,000 85 E10 US06 7632515 1/15/2014 0.0047 0.0028 0.0018 0.4750 0.0001 384.3272 21.6053 0.0019 4 1,000 85 E10 US FTP 7632525 1/16/2014 0.0010 0.0005 0.0001 0.2051 0.0027 382.478 21.6958 0.0011 4 1,000 85 E10 US FTP 7632541 1/17/2014 0.0017 0.0022 0.1660 0.0023 368.5639 22.7791 0.0033 4 1,000 85 E10 US06 7632541 1/17/2014 0.0022 0.0022 0.1660 0.0023 368.5639 27.7791 0.0033 4 1,000 85 E10 US06 7632541 1/17/2014 0.0022 0.0022 0.1660 0.0023 368.5639 2.7720 0.0003 | 4 | 5,000 | 85 E10 | US FTP | 7632515 | 1/15/2014 | 0.0533 | 0.0055 | 0.0482 | 0.3210 | 0.0118 | 362.6174 | 22.9108 | 0.0501 |
| 4 5,000 85 E10 US06 7632515 1/15/2014 0.0047 0.0028 0.0018 0.4750 0.0001 384.3272 21.6053 0.0019 4 1,000 85 E10 US FTP 7632525 1/16/2014 0.0010 0.0025 0.0011 0.2051 0.0012 371.6965 22.5780 0.0001 4 1,000 85 E10 US06 7632525 1/16/2014 0.0002 0.0002 0.6176 0.0027 382.4781 21.6968 0.0002 4 1,000 85 E10 US06 7632541 1/17/2014 0.0017 0.0089 0.0367 0.2855 0.0050 354.0904 23.4662 0.0382 4 1,000 85 E10 US06 7632541 1/17/2014 0.0002 0.0002 0.1660 0.0028 368.5639 22.7791 0.0003 4 1,000 87 E10 US FTP 7632641 1/28/2014 0.0022 0.0020 0.3998 0.0033 351.681 23.8088 21.7220 <td>4</td> <td>5,000</td> <td>85 E10</td> <td>LA92</td> <td>7632515</td> <td>1/15/2014</td> <td>0.0024</td> <td>0.0023</td> <td>0.0001</td> <td>0.1964</td> <td>0.0014</td> <td>366.7183</td> <td>22.8737</td> <td>0.0001</td> | 4 | 5,000 | 85 E10 | LA92 | 7632515 | 1/15/2014 | 0.0024 | 0.0023 | 0.0001 | 0.1964 | 0.0014 | 366.7183 | 22.8737 | 0.0001 |
| 4 1,000 85 E10 US FTP 7632525 1/16/2014 0.0410 0.0062 0.0369 0.3005 0.0039 354.7072 23.4233 0.0384 4 1,000 85 E10 LA92 7632525 1/16/2014 0.0001 0.0005 0.0001 0.2051 0.0012 371.6965 22.5780 0.0001 4 1,000 85 E10 US FTP 7632541 1/17/2014 0.0017 0.0089 0.0367 0.2855 0.0050 354.0904 23.4662 0.0382 4 1,000 85 E10 LA92 7632541 1/17/2014 0.0022 0.0026 0.0003 0.5837 0.0027 382.4781 21.6968 0.0033 4 1,000 85 E10 LA92 7632541 1/17/2014 0.0022 0.0026 0.0003 0.5837 0.0027 382.0868 21.720 0.0033 4 5,000 87 E10 US FTP 7632641 1/28/2014 0.0029 0.0020 0.2128 0.014 368.6685 2.8404 0.0002 4 5,000 87 E10 US FTP | 4 | 5,000 | 85 E10 | US06 | 7632515 | 1/15/2014 | 0.0047 | 0.0028 | 0.0018 | 0.4750 | 0.0001 | 384.3272 | 21.6053 | 0.0019 |
| 4 1,000 85 E10 LA92 7632525 1/16/2014 0.0001 0.0005 0.0001 0.2051 0.0012 371.6965 22.5780 0.0001 4 1,000 85 E10 US06 7632525 1/16/2014 0.0002 0.0002 0.6176 0.0027 382.4781 21.6968 0.0002 4 1,000 85 E10 US FTP 7632541 1/17/2014 0.0012 0.0032 0.6176 0.0027 382.4781 21.6968 0.0002 4 1,000 85 E10 LA92 7632541 1/17/2014 0.0002 0.0032 0.0002 0.1660 0.0028 368.5639 22.7791 0.0003 4 1,000 85 E10 US 66 7632541 1/17/2014 0.0022 0.0026 0.0003 0.5837 0.0027 382.0868 21.7220 0.0003 4 5,000 87 E10 LA92 7632641 1/28/2014 0.0002 0.0002 0.2128 0.0014 368.6685 22.8404 0.0002 | 4 | 1,000 | 85 E10 | US FTP | 7632525 | 1/16/2014 | 0.0410 | 0.0062 | 0.0369 | 0.3005 | 0.0039 | 354.7072 | 23.4233 | 0.0384 |
| 4 1,000 85 E10 US06 7632525 1/16/2014 0.0002 0.0009 0.0002 0.6176 0.0027 382.4781 21.6968 0.0002 4 1,000 85 E10 US FTP 7632541 1/17/2014 0.0417 0.0089 0.0367 0.2855 0.0003 354.0904 23.4662 0.0382 4 1,000 85 E10 LA92 7632541 1/17/2014 0.0022 0.0002 0.1660 0.0028 368.5639 22.7791 0.0003 4 1,000 85 E10 US06 7632541 1/17/2014 0.0022 0.0026 0.0003 0.5837 0.0027 382.0868 21.7220 0.0003 4 5,000 87 E10 US06 7632641 1/28/2014 0.0022 0.0020 0.2128 0.0014 388.6685 22.8404 0.0002 4 5,000 87 E10 US06 7632651 1/29/2014 0.0002 0.3065 0.0053 387.9717 21.4990 0.0002 | 4 | 1,000 | 85 E10 | LA92 | 7632525 | 1/16/2014 | 0.0001 | 0.0005 | 0.0001 | 0.2051 | 0.0012 | 371.6965 | 22.5780 | 0.0001 |
| 4 1,000 85 E10 US FTP 7632541 1/17/2014 0.0417 0.0089 0.0367 0.2855 0.0050 354.0904 23.4662 0.0382 4 1,000 85 E10 LA92 7632541 1/17/2014 0.0002 0.0032 0.0002 0.1660 0.0028 368.5639 22.7791 0.0003 4 1,000 85 E10 US06 7632541 1/17/2014 0.0022 0.0026 0.0003 0.5837 0.0027 382.0868 21.7220 0.0003 4 5,000 87 E10 US FTP 7632641 1/28/2014 0.0022 0.0020 0.2128 0.0014 368.6685 2.8404 0.0002 4 5,000 87 E10 US 6 7632641 1/28/2014 0.0002 0.3005 0.0053 387.9717 21.4990 0.0002 4 5,000 87 E10 US FTP 7632656 1/29/2014 0.0001 0.0001 0.2280 0.0011 363.4949 2.9384 0.0756 | 4 | 1,000 | 85 E10 | US06 | 7632525 | 1/16/2014 | 0.0002 | 0.0009 | 0.0002 | 0.6176 | 0.0027 | 382.4781 | 21.6968 | 0.0002 |
| 4 1,000 85 E10 LA92 7632541 1/17/2014 0.0002 0.0032 0.0002 0.1660 0.0028 368.5639 22.7791 0.0003 4 1,000 85 E10 US06 7632541 1/17/2014 0.0022 0.0003 0.5837 0.0027 382.0868 21.7220 0.0003 4 5,000 87 E10 US FTP 7632641 1/28/2014 0.0053 0.0000 0.0022 0.2128 0.0014 368.6685 22.8404 0.0002 4 5,000 87 E10 US FTP 7632641 1/28/2014 0.0002 0.0000 0.0022 0.3065 0.0053 387.9717 21.4990 0.0002 4 5,000 87 E10 US FTP 7632656 1/29/2014 0.0012 0.0004 0.0002 0.3065 0.0053 387.9717 21.4990 0.0002 4 5,000 87 E10 US FTP 7632656 1/29/2014 0.001 0.0001 0.280 0.0010 370.0977 22.7691 0.0011 4 5,000 87 E10 LA92 7632656 | 4 | 1,000 | 85 E10 | US FTP | 7632541 | 1/17/2014 | 0.0417 | 0.0089 | 0.0367 | 0.2855 | 0.0050 | 354.0904 | 23.4662 | 0.0382 |
| 4 1,000 85 E10 US06 7632541 1/17/2014 0.0022 0.0026 0.0003 0.5837 0.0027 382.0868 21.7220 0.0003 4 5,000 87 E10 US FTP 7632641 1/28/2014 0.0583 0.0059 0.0529 0.3998 0.0033 350.1681 23.8073 0.0550 4 5,000 87 E10 LA92 7632641 1/28/2014 0.0002 0.0000 0.0022 0.2128 0.0014 368.6685 22.8404 0.0002 4 5,000 87 E10 US06 7632641 1/28/2014 0.0002 0.0004 0.0002 0.3065 0.0053 387.9717 21.4990 0.0002 4 5,000 87 E10 US of 7632656 1/29/2014 0.0011 0.0000 0.0011 0.2280 0.0010 370.977 22.7691 0.0011 4 5,000 87 E10 US of 7632656 1/29/2014 0.0001 0.0006 0.0001 0.4040 0.0033 | 4 | 1,000 | 85 E10 | LA92 | 7632541 | 1/17/2014 | 0.0002 | 0.0032 | 0.0002 | 0.1660 | 0.0028 | 368.5639 | 22.7791 | 0.0003 |
| 4 5,000 87 E10 US FTP 7632641 1/28/2014 0.0583 0.0059 0.3529 0.3998 0.0033 350.1681 23.8073 0.0550 4 5,000 87 E10 LA92 7632641 1/28/2014 0.0002 0.0000 0.2128 0.0014 368.6685 22.8404 0.0002 4 5,000 87 E10 US06 7632641 1/28/2014 0.0002 0.0004 0.0002 0.3065 0.0053 387.9717 21.4990 0.0002 4 5,000 87 E10 US FTP 7632656 1/29/2014 0.00781 0.0058 0.0727 0.3770 0.0111 363.4949 22.9384 0.0756 4 5,000 87 E10 LA92 7632656 1/29/2014 0.0001 0.0000 0.0001 0.2280 0.0010 370.0977 22.7691 0.0001 4 5,000 87 E10 US FTP 7632656 1/29/2014 0.0001 0.0001 0.4040 0.0033 388.3606 21.4690< | 4 | 1,000 | 85 E10 | US06 | 7632541 | 1/17/2014 | 0.0022 | 0.0026 | 0.0003 | 0.5837 | 0.0027 | 382.0868 | 21.7220 | 0.0003 |
| 4 5,000 87 E10 LA92 7632641 1/28/2014 0.0002 0.0000 0.0002 0.2128 0.0014 368.6685 22.8404 0.0002 4 5,000 87 E10 US06 7632641 1/28/2014 0.0002 0.0004 0.0002 0.3065 0.0013 387.9717 21.4990 0.0002 4 5,000 87 E10 US FTP 7632656 1/29/2014 0.0012 0.0004 0.0002 0.3065 0.0053 387.9717 21.4990 0.0002 4 5,000 87 E10 US FTP 7632656 1/29/2014 0.0011 0.0058 0.0727 0.3770 0.0111 363.4949 22.9384 0.0756 4 5,000 87 E10 LA92 7632656 1/29/2014 0.0001 0.0000 0.0001 0.2280 0.0010 370.0977 22.7691 0.0001 4 1,000 87 E10 US FTP 7632669 1/30/2014 0.0046 0.0415 0.2844 0.0072 362.2882 <td>4</td> <td>5,000</td> <td>87 E10</td> <td>US FTP</td> <td>7632641</td> <td>1/28/2014</td> <td>0.0583</td> <td>0.0059</td> <td>0.0529</td> <td>0.3998</td> <td>0.0033</td> <td>350.1681</td> <td>23.8073</td> <td>0.0550</td> | 4 | 5,000 | 87 E10 | US FTP | 7632641 | 1/28/2014 | 0.0583 | 0.0059 | 0.0529 | 0.3998 | 0.0033 | 350.1681 | 23.8073 | 0.0550 |
| 4 5,000 87 E10 US06 7632641 1/28/2014 0.0002 0.0004 0.0002 0.3065 0.0053 387.9717 21.4990 0.0002 4 5,000 87 E10 US FTP 7632656 1/29/2014 0.0781 0.0058 0.0727 0.3770 0.0111 363.4949 22.9384 0.0756 4 5,000 87 E10 LA92 7632656 1/29/2014 0.0001 0.0000 0.0001 0.2280 0.0010 370.0977 22.7691 0.0001 4 5,000 87 E10 US 66 7632656 1/29/2014 0.0001 0.0000 0.0001 0.4040 0.0033 388.3606 21.4690 0.0001 4 1,000 87 E10 US FTP 7632669 1/30/2014 0.0458 0.0046 0.0415 0.2844 0.0072 362.2882 23.0232 0.0432 4 1,000 87 E10 LA92 7632669 1/30/2014 0.0000 0.0000 0.1965 0.0016 375.5836 <td>4</td> <td>5,000</td> <td>87 E10</td> <td>LA92</td> <td>7632641</td> <td>1/28/2014</td> <td>0.0002</td> <td>0.0000</td> <td>0.0002</td> <td>0.2128</td> <td>0.0014</td> <td>368.6685</td> <td>22.8404</td> <td>0.0002</td> | 4 | 5,000 | 87 E10 | LA92 | 7632641 | 1/28/2014 | 0.0002 | 0.0000 | 0.0002 | 0.2128 | 0.0014 | 368.6685 | 22.8404 | 0.0002 |
| 4 5,000 87 E10 US FTP 7632656 1/29/2014 0.00781 0.0058 0.0727 0.3770 0.0111 363.4949 22.9384 0.0756 4 5,000 87 E10 LA92 7632656 1/29/2014 0.0011 0.0000 0.0011 363.4949 22.9384 0.0756 4 5,000 87 E10 LA92 7632656 1/29/2014 0.0001 0.0000 0.0001 0.2280 0.0010 370.0977 22.7691 0.0001 4 5,000 87 E10 US06 7632656 1/29/2014 0.0001 0.0006 0.0001 0.4040 0.0033 388.3606 21.4690 0.0001 4 1,000 87 E10 US FTP 7632669 1/30/2014 0.0000 0.0000 0.1965 0.0016 375.5836 22.4265 0.0000 4 1,000 87 E10 LA92 7632669 1/30/2014 0.0000 0.0000 0.5255 0.0012 385.7737 21.6021 0.0000 | 4 | 5.000 | 87 E10 | US06 | 7632641 | 1/28/2014 | 0.0002 | 0.0004 | 0.0002 | 0.3065 | 0.0053 | 387.9717 | 21.4990 | 0.0002 |
| 4 5,000 87 E10 LA92 7632656 1/29/2014 0.0001 0.0000 0.0001 0.2280 0.0010 370.0977 22.7691 0.0001 4 5,000 87 E10 US06 7632656 1/29/2014 0.0001 0.0000 0.0001 0.2280 0.0010 370.0977 22.7691 0.0001 4 5,000 87 E10 US06 7632656 1/29/2014 0.0001 0.0006 0.0001 0.4040 0.0033 388.3606 21.4690 0.0001 4 1,000 87 E10 US FTP 7632669 1/30/2014 0.0458 0.0046 0.0415 0.2844 0.0072 362.2882 23.0232 0.0432 4 1,000 87 E10 LA92 7632669 1/30/2014 0.0000 0.0000 0.1965 0.0016 375.5836 22.4265 0.0000 4 1,000 87 E10 US 66 7632681 1/30/2014 0.0000 0.0010 0.5255 0.0012 385.7737 21.6021 | 4 | 5.000 | 87 E10 | US FTP | 7632656 | 1/29/2014 | 0.0781 | 0.0058 | 0.0727 | 0.3770 | 0.0111 | 363.4949 | 22.9384 | 0.0756 |
| 4 5,000 87 E10 US06 7632656 1/29/2014 0.0001 0.0006 0.0001 0.4040 0.0033 388.3606 21.4690 0.0001 4 1,000 87 E10 US FTP 7632669 1/30/2014 0.0458 0.0046 0.0415 0.2844 0.0072 362.2882 23.0232 0.0432 4 1,000 87 E10 LA92 7632669 1/30/2014 0.0000 0.0000 0.1965 0.0016 375.5836 22.4265 0.0000 4 1,000 87 E10 LA92 7632669 1/30/2014 0.0000 0.0010 0.0000 0.1965 0.0016 375.5836 22.4265 0.0000 4 1,000 87 E10 US06 7632669 1/30/2014 0.0000 0.0010 0.0000 0.5255 0.0012 385.7737 21.6021 0.0000 4 1,000 87 E10 US FTP 7632681 1/31/2014 0.0031 0.0037 3466 0.0079 366.2294 22.7697 | 4 | 5.000 | 87 E10 | LA92 | 7632656 | 1/29/2014 | 0.0001 | 0.0000 | 0.0001 | 0.2280 | 0.0010 | 370.0977 | 22.7691 | 0.0001 |
| 4 1,000 87 E10 US FTP 7632669 1/30/2014 0.0058 0.0046 0.0415 0.2844 0.0072 362.2882 23.0232 0.0432 4 1,000 87 E10 US FTP 7632669 1/30/2014 0.0000 0.0000 0.1965 0.0016 375.5836 22.4265 0.0000 4 1,000 87 E10 US06 7632669 1/30/2014 0.0000 0.0010 0.1965 0.0016 375.5836 22.4265 0.0000 4 1,000 87 E10 US06 7632669 1/30/2014 0.0000 0.0010 0.0000 0.5255 0.0012 385.7737 21.6021 0.0000 4 1,000 87 E10 US FTP 7632681 1/31/2014 0.0037 0.3466 0.0079 366.2294 22.7697 0.0402 4 1,000 87 E10 LA92 7632681 1/31/2014 0.0001 0.0001 0.1829 0.0025 367.1877 22.9616 0.00088 4 | 4 | 5.000 | 87 E10 | US06 | 7632656 | 1/29/2014 | 0.0001 | 0.0006 | 0.0001 | 0.4040 | 0.0033 | 388.3606 | 21.4690 | 0.0001 |
| 4 1,000 87 E10 LA92 7632669 1/30/2014 0.0000 0.0000 0.1965 0.0016 375.5836 22.4265 0.0000 4 1,000 87 E10 US06 7632669 1/30/2014 0.0000 0.0000 0.1965 0.0016 375.5836 22.4265 0.0000 4 1,000 87 E10 US06 7632681 1/31/2014 0.0004 0.0010 0.5255 0.0012 385.7737 21.6021 0.0000 4 1,000 87 E10 US FTP 7632681 1/31/2014 0.0037 0.3466 0.0079 366.2294 22.7697 0.0402 4 1,000 87 E10 LA92 7632681 1/31/2014 0.0001 0.0001 0.1829 0.0025 367.1877 22.9616 0.0008 4 1.000 87 E10 US06 7632681 1/31/2014 0.0001 0.0001 0.0001 0.0025 367.1877 22.9616 0.0008 4 1.000 87 E10 <td< td=""><td>4</td><td>1.000</td><td>87 E10</td><td>US FTP</td><td>7632669</td><td>1/30/2014</td><td>0.0458</td><td>0.0046</td><td>0.0415</td><td>0.2844</td><td>0.0072</td><td>362.2882</td><td>23.0232</td><td>0.0432</td></td<> | 4 | 1.000 | 87 E10 | US FTP | 7632669 | 1/30/2014 | 0.0458 | 0.0046 | 0.0415 | 0.2844 | 0.0072 | 362.2882 | 23.0232 | 0.0432 |
| 4 1,000 87 E10 US06 7632669 1/30/2014 0.0000 0.0010 0.0000 0.5255 0.0012 385.7737 21.6021 0.0000 4 1,000 87 E10 US06 7632669 1/30/2014 0.0000 0.0010 0.0000 0.5255 0.0012 385.7737 21.6021 0.0000 4 1,000 87 E10 US FTP 7632681 1/31/2014 0.0037 0.3466 0.0079 366.2294 22.7697 0.0402 4 1,000 87 E10 LA92 7632681 1/31/2014 0.0001 0.0000 0.0001 0.1829 0.0025 367.1877 22.9616 0.0008 4 1.000 87 E10 US06 7632681 1/31/2014 0.0001 0.0001 0.1829 0.0025 367.1877 22.9616 0.0008 4 1.000 87 E10 US06 7632681 1/31/2014 0.0001 0.0001 0.0001 0.0037 380 9072 21 8780 0.0001 <td>4</td> <td>1.000</td> <td>87 F10</td> <td>LA92</td> <td>7632669</td> <td>1/30/2014</td> <td>0.0000</td> <td>0.0000</td> <td>0.0000</td> <td>0.1965</td> <td>0.0016</td> <td>375.5836</td> <td>22,4265</td> <td>0.0000</td> | 4 | 1.000 | 87 F10 | LA92 | 7632669 | 1/30/2014 | 0.0000 | 0.0000 | 0.0000 | 0.1965 | 0.0016 | 375.5836 | 22,4265 | 0.0000 |
| 4 1,000 87 E10 US FTP 7632681 1/31/2014 0.0011 0.0000 0.0012 0.0012 0.0012 0.0012 0.0012 0.0012 0.0012 0.0001 0.0012 0.0012 0.0001 0.0012 0.0012 0.0001 0.0001 0.0012 0.0012 0.0012 0.0001 0.0002 0.0012 <td>4</td> <td>1.000</td> <td>87 F10</td> <td>US06</td> <td>7632669</td> <td>1/30/2014</td> <td>0.0000</td> <td>0.0010</td> <td>0.0000</td> <td>0.5255</td> <td>0.0012</td> <td>385.7737</td> <td>21,6021</td> <td>0.0000</td> | 4 | 1.000 | 87 F10 | US06 | 7632669 | 1/30/2014 | 0.0000 | 0.0010 | 0.0000 | 0.5255 | 0.0012 | 385.7737 | 21,6021 | 0.0000 |
| 4 1,000 87 E10 LA92 7632681 1/31/2014 0.0001 0.0001 0.1829 0.0025 367.1877 22.9616 0.0008 4 1.000 87 E10 LA92 7632681 1/31/2014 0.0001 0.0001 0.1829 0.0025 367.1877 22.9616 0.0008 4 1.000 87 E10 US06 7632681 1/31/2014 0.0001 0.0001 0.5198 0.0037 380.9072 21.8780 0.0001 | 4 | 1 000 | 87 F10 | US FTP | 7632681 | 1/31/2014 | 0.0435 | 0.0094 | 0.0387 | 0.3466 | 0.0079 | 366 229/ | 22,7697 | 0.0402 |
| 4 1.000 87 F10 US06 7632681 1/31/2014 0.0001 0.0001 0.0001 0.1023 0.0023 307.1077 22.3010 0.0000 | 4 | 1 000 | 87 F10 | 1007 | 7632681 | 1/31/2014 | 0 0001 | 0.000 | 0.0001 | 0 1870 | 0.0075 | 367 1877 | 22 9616 | 0.000 |
| | 4 | 1 000 | 87 F10 | 11506 | 7632681 | 1/31/2014 | 0.0001 | 0.0004 | 0.0001 | 0.5198 | 0.0037 | 380 9072 | 21,8780 | 0.0001 |

| VNumber | Altitude | Fuel | TestCycle | TestID | TestDate | THC | CH4 | NonMethane | CO | Nox | CO2 | FE | NMOG |
|---------|----------|--------|-----------|-----------------|------------|----------|----------|------------|----------|----------|----------|---------|----------|
| | (ft) | | | | | (g/mile) | (g/mile) | (g/mile) | (g/mile) | (g/mile) | (g/mile) | (mpg) | (g/mile) |
| 5 | 5,000 | 85 E10 | LA92 | 7631985 | 11/5/2013 | 0.0001 | 0.0024 | 0.0001 | 0.0917 | 0.0050 | 495.4226 | 16.9511 | 0.0001 |
| 5 | 5,000 | 85 E10 | US06 | 7631985 | 11/5/2013 | 0.0364 | 0.0148 | 0.0216 | 1.4709 | 0.0518 | 521.8467 | 15.8724 | 0.0225 |
| 5 | 5,000 | 85 E10 | US FTP | 7631996 | 11/6/2013 | 0.0224 | 0.0086 | 0.0157 | 0.2183 | 0.0108 | 467.5383 | 17.7812 | 0.0163 |
| 5 | 5,000 | 85 E10 | LA92 | 7631996 | 11/6/2013 | 0.0001 | 0.0018 | 0.0000 | 0.1228 | 0.0195 | 490.5300 | 17.1383 | 0.0000 |
| 5 | 5,000 | 85 E10 | US06 | 7631996 | 11/6/2013 | 0.0367 | 0.0139 | 0.0227 | 2.2769 | 0.0148 | 513.3744 | 16.0936 | 0.0236 |
| 5 | 1,000 | 85 E10 | US FTP | 7632108 | 11/19/2013 | 0.0280 | 0.0079 | 0.0209 | 0.1787 | 0.0126 | 482.2586 | 17.2414 | 0.0217 |
| 5 | 1,000 | 85 E10 | LA92 | 7632108 | 11/19/2013 | 0.0001 | 0.0021 | 0.0001 | 0.0851 | 0.0055 | 490.4208 | 17.1415 | 0.0001 |
| 5 | 1,000 | 85 E10 | US06 | 7632108 | 11/19/2013 | 0.0170 | 0.0073 | 0.0097 | 0.4639 | 0.0170 | 517.1492 | 16.0648 | 0.0101 |
| 5 | 1,000 | 85 E10 | US FTP | 7632126 | 11/21/2013 | 0.0226 | 0.0074 | 0.0153 | 0.2181 | 0.0087 | 484.5152 | 17.1610 | 0.0159 |
| 5 | 1,000 | 85 E10 | LA92 | 7632126 | 11/21/2013 | 0.0001 | 0.0002 | 0.0001 | 0.1275 | 0.0053 | 486.2131 | 17.2861 | 0.0001 |
| 5 | 1,000 | 85 E10 | US06 | 7632126 | 11/21/2013 | 0.0115 | 0.0044 | 0.0072 | 0.3031 | 0.0189 | 509.3711 | 16.3179 | 0.0075 |
| 5 | 1,000 | 85 E10 | US FTP | 7632427 | 1/8/2014 | 0.0250 | 0.0107 | 0.0178 | 0.2291 | 0.0056 | 482.5647 | 17.2279 | 0.0185 |
| 5 | 1,000 | 85 E10 | LA92 | 7632427 | 1/8/2014 | 0.0000 | 0.0021 | 0.0000 | 0.1690 | 0.0059 | 502.8789 | 16.7046 | 0.0000 |
| 5 | 1,000 | 85 E10 | US06 | 7632427 | 1/8/2014 | 0.0134 | 0.0068 | 0.0066 | 0.3447 | 0.0126 | 514.4750 | 16.1541 | 0.0069 |
| 5 | 5,000 | 85 E10 | US FTP | 7632456 | 1/10/2014 | 0.0267 | 0.0078 | 0.0192 | 0.2360 | 0.0041 | 464.2759 | 17.9053 | 0.0200 |
| 5 | 5,000 | 85 E10 | LA92 | 7632456 | 1/10/2014 | 0.0001 | 0.0009 | 0.0001 | 0.1413 | 0.0139 | 478.0007 | 17.6097 | 0.0001 |
| 5 | 5,000 | 85 E10 | US06 | 7632456 | 1/10/2014 | 0.0211 | 0.0084 | 0.0126 | 1.0920 | 0.0127 | 508.8532 | 16.2948 | 0.0131 |
| 5 | 5,000 | 87 E10 | US FTP | 7632579 | 1/22/2014 | 0.0240 | 0.0075 | 0.0178 | 0.1757 | 0.0089 | 461.2572 | 18.0933 | 0.0185 |
| 5 | 5,000 | 87 E10 | LA92 | 7632579 | 1/22/2014 | 0.0001 | 0.0001 | 0.0001 | 0.0840 | 0.0102 | 472.0427 | 17.9033 | 0.0001 |
| 5 | 5,000 | 87 E10 | US06 | 7632579 | 1/22/2014 | 0.0079 | 0.0034 | 0.0045 | 0.2464 | 0.0105 | 494.7013 | 16.8684 | 0.0047 |
| 5 | 5,000 | 87 E10 | US FTP | 7632589 | 1/23/2014 | 0.0311 | 0.0121 | 0.0198 | 0.2249 | 0.0184 | 478.0128 | 17.4584 | 0.0206 |
| 5 | 5,000 | 87 E10 | LA92 | 7632589 | 1/23/2014 | 0.0037 | 0.0029 | 0.0008 | 0.0837 | 0.0285 | 494.0525 | 17.0950 | 0.0008 |
| 5 | 5,000 | 87 E10 | US06 | 7632589 | 1/23/2014 | 0.0148 | 0.0054 | 0.0093 | 0.2824 | 0.0308 | 506.7147 | 16.4669 | 0.0097 |
| 5 | 1,000 | 87 E10 | US FTP | 7632625 | 1/27/2014 | 0.0255 | 0.0083 | 0.0172 | 0.2236 | 0.0062 | 489.7637 | 17.0399 | 0.0179 |
| 5 | 1,000 | 87 E10 | LA92 | 7632625 | 1/27/2014 | 0.0001 | 0.0000 | 0.0001 | 0.1059 | 0.0083 | 481.4894 | 17.5253 | 0.0001 |
| 5 | 1,000 | 87 E10 | US06 | 7632625 | 1/27/2014 | 0.0093 | 0.0038 | 0.0055 | 0.2590 | 0.0107 | 502.7363 | 16.5984 | 0.0057 |
| 5 | 1,000 | 87 E10 | US FTP | 7632778 | 2/10/2014 | 0.0267 | 0.0094 | 0.0206 | 0.1458 | 0.0127 | 487.3117 | 17.1286 | 0.0214 |
| 5 | 1,000 | 87 E10 | LA92 | 7632778 | 2/10/2014 | 0.0001 | 0.0021 | 0.0001 | 0.0762 | 0.0075 | 466.8019 | 18.0804 | 0.0001 |
| 5 | 1,000 | 87 E10 | US06 | 7632778 | 2/10/2014 | 0.0072 | 0.0048 | 0.0024 | 0.2247 | 0.0118 | 502.0875 | 16.6216 | 0.0025 |
| 6 | 5,000 | 85 E10 | US FTP | 782012140006-8 | 1/30/2014 | 0.0371 | 0.0051 | 0.0322 | 0.4570 | 0.0459 | 252.8000 | 35.0041 | 0.0335 |
| 6 | 5,000 | 85 E10 | LA92 | 782012140006-10 | 1/30/2014 | 0.0021 | 0.0017 | 0.0005 | 0.2847 | 0.0182 | 256.2000 | 34.6483 | 0.0005 |
| 6 | 5,000 | 85 E10 | US06 | 782012140006-11 | 1/30/2014 | 0.0175 | 0.0092 | 0.0086 | 5.4455 | 0.0238 | 279.7000 | 30.7861 | 0.0090 |
| 6 | 1,000 | 85 E10 | US FTP | 782012140006-13 | 2/4/2014 | 0.0298 | 0.0053 | 0.0247 | 0.4695 | 0.0330 | 261.2000 | 33.9354 | 0.0257 |
| 6 | 1,000 | 85 E10 | LA92 | 782012140006-15 | 2/4/2014 | 0.0031 | 0.0025 | 0.0007 | 0.4139 | 0.0178 | 267.9000 | 33.0739 | 0.0007 |
| 6 | 1,000 | 85 E10 | US06 | 782012140006-16 | 2/4/2014 | 0.0124 | 0.0062 | 0.0065 | 3.3692 | 0.0110 | 288.8000 | 30.1883 | 0.0067 |
| 6 | 1,000 | 85 E10 | US FTP | 782012140006-17 | 2/4/2014 | 0.0330 | 0.0051 | 0.0281 | 0.4849 | 0.0387 | 259.7000 | 34.0623 | 0.0292 |
| 6 | 1,000 | 85 E10 | LA92 | 782012140006-19 | 2/5/2014 | 0.0030 | 0.0021 | 0.0010 | 0.3073 | 0.0184 | 264.3000 | 33.5938 | 0.0010 |
| 6 | 1,000 | 85 E10 | US06 | 782012140006-20 | 2/5/2014 | 0.0127 | 0.0063 | 0.0066 | 4.6993 | 0.0209 | 286.7000 | 30.1788 | 0.0069 |
| 6 | 5,000 | 85 E10 | US FTP | 782012140009-2 | 2/7/2014 | 0.0382 | 0.0051 | 0.0333 | 0.5118 | 0.0409 | 251.1000 | 35.2706 | 0.0346 |
| 6 | 5,000 | 85 E10 | LA92 | 782012140009-4 | 2/7/2014 | 0.0027 | 0.0019 | 0.0009 | 0.4308 | 0.0205 | 261.5000 | 33.8254 | 0.0009 |
| 6 | 5,000 | 85 E10 | US06 | 782012140009-5 | 2/7/2014 | 0.0162 | 0.0086 | 0.0080 | 5.4425 | 0.0296 | 288.2000 | 29.9577 | 0.0083 |
| 6 | 5,000 | 85 E10 | US FTP | 782012140009-6 | 2/9/2014 | 0.0371 | 0.0049 | 0.0324 | 0.4415 | 0.0373 | 252.2000 | 35.1469 | 0.0337 |
| 6 | 5,000 | 85 E10 | LA92 | 782012140009-8 | 2/10/2014 | 0.0021 | 0.0016 | 0.0005 | 0.2972 | 0.0130 | 256.8000 | 34.5095 | 0.0005 |
| 6 | 5,000 | 85 E10 | US06 | 782012140009-9 | 2/10/2014 | 0.0147 | 0.0078 | 0.0071 | 5.4079 | 0.0396 | 284.9000 | 30.2690 | 0.0074 |
| 6 | 5,000 | 87 E10 | US FTP | 782012140010-4 | 2/24/2014 | 0.0396 | 0.0053 | 0.0349 | 0.4388 | 0.0347 | 244.0000 | 36.2710 | 0.0363 |
| 6 | 5,000 | 87 E10 | LA92 | 782012140010-6 | 2/25/2014 | 0.0030 | 0.0022 | 0.0011 | 0.3523 | 0.0143 | 253.5000 | 34.8830 | 0.0012 |
| 6 | 5,000 | 87 E10 | US FTP | 782012140010-8 | 2/25/2014 | 0.0417 | 0.0051 | 0.0371 | 0.4277 | 0.0394 | 250.9000 | 35.2641 | 0.0386 |
| 6 | 5,000 | 87 E10 | LA92 | 782012140010-10 | 2/25/2014 | 0.0026 | 0.0020 | 0.0008 | 0.3821 | 0.0189 | 260.0000 | 34.0736 | 0.0009 |
| 6 | 5,000 | 87 E10 | US06 | 782012140010-11 | 2/26/2014 | 0.0144 | 0.0072 | 0.0080 | 3.9369 | 0.0088 | 278.2000 | 31.2410 | 0.0083 |
| 6 | 5,000 | 87 E10 | US06 | 782012140012-1 | 2/26/2014 | 0.0135 | 0.0072 | 0.0071 | 5.0403 | 0.0162 | 279.3000 | 30.9443 | 0.0074 |
| 6 | 1,000 | 87 E10 | US FTP | 782012140010-13 | 2/26/2014 | 0.0358 | 0.0057 | 0.0308 | 0.5007 | 0.0343 | 254.2000 | 34.8364 | 0.0320 |
| 6 | 1,000 | 87 E10 | LA92 | 782012140010-15 | 2/26/2014 | 0.0046 | 0.0029 | 0.0020 | 0.3233 | 0.0194 | 261.4000 | 33.9547 | 0.0021 |
| 6 | 1,000 | 87 E10 | US FTP | 782012140010-17 | 2/28/2014 | 0.0363 | 0.0055 | 0.0314 | 0.4924 | 0.0361 | 261.5000 | 33.7784 | 0.0326 |
| 6 | 1,000 | 87 E10 | LA92 | 782012140010-19 | 2/28/2014 | 0.0024 | 0.0020 | 0.0006 | 0.3641 | 0.0142 | 266.3000 | 33.3111 | 0.0007 |
| 6 | 1,000 | 87 E10 | US06 | 782012140010-20 | 2/28/2014 | 0.0100 | 0.0050 | 0.0055 | 1.9907 | 0.0086 | 281.9000 | 31.1398 | 0.0057 |
| 6 | 1,000 | 87 E10 | US06 | 782012140013-1 | 2/28/2014 | 0.0067 | 0.0031 | 0.0039 | 2.0384 | 0.0115 | 284.1000 | 30.9155 | 0.0041 |

| (ft) (g/mile) (g/mile) <th< th=""></th<> |
|---|
| 7 5,000 85 E10 US06 MS34009190 1/24/2014 0.0529 0.0309 0.0240 1.8788 0.0215 494.6590 16.7525 0.0327 7 5,000 85 E10 US FTP MS34009189 1/29/2014 0.0376 0.0217 1.3141 0.0105 510.3080 16.7252 0.0327 7 5,000 85 E10 US FTP MS34009199 1/30/2014 0.0424 0.0164 0.0106 1.0972 0.084 510.500 16.7325 0.0176 7 5,000 85 E10 LA92 MS34009200 1/30/2014 0.0564 0.0318 0.0276 2.0844 510.500 16.7325 0.0116 7 1,000 85 E10 LA92 MS34009220 2/4/2014 0.059 1.0916 2.1881 0.0257 2.6355 0.0317 524.0010 15.726 0.0289 7 1,000 85 E10 LA92 MS34009230 2/5/2014 0.0575 0.0340 0.0277 2.6355 0.0317 52 |
| 7 5,000 85 E10 US FTP MS34009188 1/29/2014 0.0376 0.0178 0.0367 0.7347 0.0215 494.6590 16.7525 0.0382 7 5,000 85 E10 LA92 MS34009189 1/29/2014 0.0376 0.0219 0.0172 1.3141 0.0105 510.3080 16.2127 0.0176 7 5,000 85 E10 LA92 MS34009200 1/30/2014 0.0424 0.0164 0.0106 1.0972 0.0084 510.0560 16.2326 0.0117 7 5,000 85 E10 LUS6 MS34009202 1/30/2014 0.0564 0.0318 0.0266 2.1881 0.0254 518.830 15.9038 0.0277 7 1,000 85 E10 LS90 MS34009220 2/4/2014 0.0138 0.0278 2.6355 0.0317 524.0010 15.7268 0.0286 7 1,000 85 E10 LA92 MS34009232 2/5/2014 0.0257 0.340 0.0257 2.6134 0.0261 5 |
| 7 5,000 85 E10 LA92 MS34009189 1/29/2014 0.0376 0.0219 0.0172 1.3141 0.0109 510.3080 16.2127 0.0172 7 5,000 85 E10 LA92 MS34009199 1/30/2014 0.0244 0.0145 0.0289 0.6162 0.0104 495.5290 16.7305 0.0300 7 5,000 85 E10 LA92 MS34009200 1/30/2014 0.0544 0.0318 0.0266 2.1881 0.0254 518.8330 15.9038 0.0277 7 1,000 85 E10 LS06 MS34009229 2/4/2014 0.0184 0.0135 0.0059 1.0913 0.0061 523.5000 15.8181 0.0267 7 1,000 85 E10 LS0F MS34009230 2/5/2014 0.0575 0.0340 0.0410 0.8459 0.0125 15.8207 0.0267 7 1,000 85 E10 LS7F MS34009242 2/15/2014 0.0575 0.0410 0.8459 0.0123 50.905 15. |
| 7 5,000 85 E10 US FTP MS34009199 1/30/2014 0.0424 0.0145 0.0289 0.6162 0.0140 495.5290 16.7305 0.0300 7 5,000 85 E10 LA92 MS34009200 1/30/2014 0.0259 0.0164 0.0106 1.0972 0.0084 510.0560 16.2326 0.0117 7 5,000 85 E10 LS06 MS34009228 2/4/2014 0.0183 0.0266 2.1881 0.0254 518.8330 15.9038 0.0277 7 1,000 85 E10 US66 MS34009229 2/4/2014 0.0593 0.0338 0.0278 2.6355 0.0315 512.7910 16.1556 0.0426 7 1,000 85 E10 US6 MS34009231 2/5/2014 0.0593 0.0175 0.0085 1.1570 0.0040 520.8750 15.8938 0.0026 7 1,000 85 E10 US6 MS34009232 2/5/2014 0.0575 0.0340 0.0277 2.6134 0.0261 520 |
| 7 5,000 85 E10 LA92 MS34009200 1/30/2014 0.0259 0.0164 0.0106 1.0972 0.0084 510.0560 16.2326 0.0110 7 5,000 85 E10 LA92 MS340092201 1/30/2014 0.0584 0.0135 0.0059 1.0913 0.0061 523.500 15.81831 0.0075 7 1,000 85 E10 LA92 MS34009220 2/4/2014 0.0593 0.0338 0.0278 2.6355 0.0315 51.0 15.156 0.0426 7 1,000 85 E10 LA92 MS34009220 2/5/2014 0.0593 0.0186 1.1570 0.0040 52.8750 15.838 0.0085 7 1,000 85 E10 LA92 MS34009242 2/5/2014 0.0575 0.0340 0.0257 2.6134 0.0261 52.9050 15.8207 0.0267 7 1,000 85 E10 US FTP MS34009342 2/18/2014 0.0137 0.0748 0.0137 506.9760 16.3478 0.03 |
| 7 5,000 85 E10 US06 MS34009201 1/30/2014 0.0564 0.0318 0.0266 2.1881 0.0254 518.830 15.9038 0.0277 7 1,000 85 E10 LA92 MS34009228 2/4/2014 0.0135 0.0059 1.0913 0.0061 523.500 15.8181 0.0061 7 1,000 85 E10 US FTP MS34009220 2/5/2014 0.0593 0.0166 0.0410 0.8459 0.0215 512.7910 16.1556 0.0426 7 1,000 85 E10 LSPT MS34009232 2/5/2014 0.0575 0.0340 0.0257 2.6134 0.0261 520.9050 15.8207 0.0267 7 1,000 85 E10 US FTP MS34009247 2/1/2014 0.0575 0.0340 0.0277 2.6134 0.0261 528.9050 15.8207 0.0267 7 1,000 85 E10 US FTP MS34009342 2/18/2014 0.0137 0.0227 0.0133 0.0275 0.0138 <td< td=""></td<> |
| 7 1,000 85 E10 LA92 MS34009228 2/4/2014 0.0184 0.0135 0.0059 1.0913 0.0061 523.500 15.8181 0.0061 7 1,000 85 E10 US06 MS34009229 2/4/2014 0.0593 0.0338 0.0278 2.6355 0.0317 524.001 15.7268 0.0285 7 1,000 85 E10 US FTP MS34009230 2/5/2014 0.0299 0.0175 0.0085 1.1570 0.0040 520.8750 15.8938 0.0285 7 1,000 85 E10 US FTP MS34009232 2/5/2014 0.0575 0.0340 0.0257 2.6134 0.0261 520.9050 15.8207 0.0267 7 1,000 85 E10 US FTP MS34009242 2/18/2014 0.0575 0.0340 0.0277 2.6134 0.0613 50.6976 1.6339 0.0455 7 5,000 87 E10 LA92 MS34009342 2/18/2014 0.0157 0.0128 0.0173 518.7150 <td< td=""></td<> |
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| 7 1,000 85 E10 US FTP MS34009230 2/5/2014 0.0593 0.0196 0.0410 0.8459 0.0125 512.7910 16.1556 0.0426 7 1,000 85 E10 LA92 MS34009232 2/5/2014 0.0249 0.0175 0.0085 1.1570 0.0040 520.8750 15.8938 0.0085 7 1,000 85 E10 US FTP MS34009232 2/5/2014 0.0575 0.0340 0.0257 2.6134 0.0261 520.9050 15.8207 0.0267 7 1,000 85 E10 US FTP MS34009247 2/7/2014 0.0552 0.0189 0.0376 0.7048 0.0137 50.6976 16.3378 0.0391 7 5,000 87 E10 US FTP MS34009343 2/18/2014 0.0157 0.0123 0.0746 0.8079 0.0123 499.0140 16.7834 0.0445 7 5,000 87 E10 US FTP MS34009353 2/19/2014 0.0137 0.0132 0.5761 0.0138 |
| 7 1,000 85 E10 LA92 MS34009231 2/5/2014 0.0249 0.0175 0.0085 1.1570 0.0040 520.8750 15.8938 0.0085 7 1,000 85 E10 US66 MS34009232 2/5/2014 0.0575 0.0340 0.0257 2.6134 0.0261 520.9050 15.8207 0.0267 7 1,000 85 E10 US FTP MS34009247 2/7/2014 0.0552 0.0189 0.0376 0.7048 0.0137 50.69760 16.3478 0.0391 7 5,000 87 E10 US FTP MS34009342 2/18/2014 0.0157 0.0122 0.0044 0.8584 0.061 508.6550 16.303 0.0475 7 5,000 87 E10 US66 MS34009342 2/18/2014 0.0492 0.0293 0.0218 2.0795 0.0173 518.7150 15.9267 0.0227 7 5,000 87 E10 US66 MS34009354 2/19/2014 0.0492 0.0293 0.0218 2.0795 |
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| 7 1,000 85 E10 US FTP MS34009247 2/7/2014 0.0552 0.0189 0.0376 0.7048 0.0137 506.9760 16.3478 0.0391 7 5,000 87 E10 US FTP MS34009342 2/18/2014 0.0931 0.0199 0.0746 0.8079 0.0123 499.0140 16.6130 0.0775 7 5,000 87 E10 LA92 MS34009343 2/18/2014 0.0157 0.0122 0.0044 0.8584 0.0061 508.6550 16.303 0.0272 7 5,000 87 E10 US of MS34009344 2/18/2014 0.0492 0.0233 0.0218 2.0795 0.0138 494.4010 16.7834 0.0492 7 5,000 87 E10 US FTP MS34009353 2/19/2014 0.0133 0.0046 0.8261 0.018 16.4194 0.0488 7 5,000 87 E10 LA92 MS34009355 2/19/2014 0.0133 0.0030 0.8797 0.0004 516.0290 16.0790 |
| 7 5,000 87 E10 US FTP MS34009342 2/18/2014 0.0199 0.0746 0.8079 0.0123 499.0140 16.6130 0.0775 7 5,000 87 E10 LA92 MS34009343 2/18/2014 0.0157 0.0122 0.0044 0.8584 0.0061 508.6550 16.303 0.0425 7 5,000 87 E10 US06 MS34009344 2/18/2014 0.0492 0.0293 0.0218 2.0795 0.0173 518.7150 15.9267 0.0227 7 5,000 87 E10 US FTP MS34009353 2/19/2014 0.0137 0.0432 0.5761 0.0138 494.4010 16.7834 0.0449 7 5,000 87 E10 LA92 MS34009355 2/19/2014 0.0143 0.0103 0.0046 0.8261 0.018 18.982 0.0139 513.8060 16.0872 0.0196 7 1,000 87 E10 LA92 MS34009417 2/25/2014 0.0113 0.0030 0.8797 0.0004 < |
| 75,00087 E10LA92MS340093432/18/20140.01570.01220.00440.85840.0061508.655016.30390.004575,00087 E10US06MS340093442/18/20140.04920.02930.02182.07950.0173518.715015.92670.022775,00087 E10US FTPMS340093532/19/20140.05760.01570.04320.57610.0138494.401016.78340.044975,00087 E10LA92MS340093542/19/20140.01430.01030.00460.82610.0018505.124016.41940.004875,00087 E10US06MS340093552/19/20140.04300.02800.01881.89820.0139513.806016.08720.019671,00087 E10LA92MS340094172/25/20140.05310.00300.87970.0044516.029016.07090.003171,00087 E10US06MS340094282/27/20140.05290.01850.03560.76500.0120502.23016.51300.037071,00087 E10US06MS340094292/27/20140.05290.01850.02660.0120502.23016.51300.037071,00087 E10US06MS340094302/27/20140.06100.02220.04130.84380.0007513.736016.14380.004771,00087 E10US06MS34009430 |
| 7 5,000 87 E10 US06 MS34009344 2/18/2014 0.0492 0.0293 0.0218 2.0795 0.0173 518.7150 15.9267 0.0227 7 5,000 87 E10 US FTP MS34009353 2/19/2014 0.0576 0.0157 0.0432 0.5761 0.0138 494.4010 16.7834 0.0448 7 5,000 87 E10 LA92 MS34009354 2/19/2014 0.0143 0.0103 0.0046 0.8261 0.0188 505.1240 16.4194 0.0488 7 5,000 87 E10 US06 MS34009355 2/19/2014 0.0450 0.0280 0.0188 1.8982 0.0139 513.8060 16.0872 0.0196 7 1,000 87 E10 US06 MS34009417 2/25/2014 0.0531 0.0305 0.0246 2.3869 0.0259 513.6580 16.0671 0.0256 7 1,000 87 E10 US FTP MS34009428 2/27/2014 0.0529 0.0185 0.0356 0.7650 |
| 7 5,000 87 E10 US FTP MS34009353 2/19/2014 0.0576 0.0137 0.0432 0.5761 0.0138 494.401 16.7834 0.0449 7 5,000 87 E10 LA92 MS34009354 2/19/2014 0.0143 0.0103 0.0046 0.8261 0.018 505.1240 16.4194 0.0048 7 5,000 87 E10 US06 MS34009355 2/19/2014 0.0450 0.0280 0.0188 1.8982 0.0139 513.8060 16.0872 0.0196 7 1,000 87 E10 US06 MS34009417 2/25/2014 0.0131 0.0089 0.0030 0.8797 0.004 516.0290 16.0709 0.0031 7 1,000 87 E10 US06 MS34009418 2/25/2014 0.0559 0.0126 2.3869 0.0259 513.6580 16.0671 0.0256 7 1,000 87 E10 US FTP MS34009429 2/27/2014 0.0161 0.0124 0.00455 0.8438 0.0007 < |
| 7 5,000 87 E10 LA92 MS34009354 2/19/2014 0.0143 0.0103 0.0046 0.8261 0.0018 505.1240 16.4194 0.0048 7 5,000 87 E10 US06 MS34009355 2/19/2014 0.0450 0.0280 0.0188 1.8982 0.019 513.806 16.0872 0.0196 7 1,000 87 E10 LA92 MS34009417 2/25/2014 0.0131 0.0089 0.0030 0.8797 0.0004 516.0290 16.0709 0.0031 7 1,000 87 E10 US06 MS34009418 2/25/2014 0.0511 0.0305 0.0246 2.3869 0.0259 513.6580 16.0671 0.0256 7 1,000 87 E10 US FTP MS34009428 2/27/2014 0.0529 0.0185 0.0356 0.7650 0.0120 502.2330 16.133 0.0047 7 1,000 87 E10 LA92 MS34009429 2/27/2014 0.0161 0.0124 0.0045 0.8438 |
| 7 5,000 87 E10 US06 MS34009355 2/19/2014 0.0450 0.0280 0.0188 1.8982 0.0139 513.8060 16.0872 0.0196 7 1,000 87 E10 LA92 MS34009417 2/25/2014 0.0113 0.0089 0.0030 0.8797 0.0004 516.0290 16.079 0.0031 7 1,000 87 E10 US06 MS34009418 2/25/2014 0.0531 0.0305 0.0246 2.3869 0.0259 513.6580 16.0671 0.0256 7 1,000 87 E10 US FTP MS34009428 2/27/2014 0.0529 0.0185 0.0356 0.7650 0.0120 502.2330 16.5130 0.0370 7 1,000 87 E10 LA92 MS34009429 2/27/2014 0.0161 0.0124 0.0045 0.8438 0.0007 513.7360 16.1438 0.0047 7 1,000 87 E10 US 6 MS34009430 2/27/2014 0.0480 0.0282 0.0217 2.0485 <t< td=""></t<> |
| 7 1,000 87 E10 LA92 MS34009417 2/25/2014 0.0113 0.0089 0.0030 0.8797 0.0004 516.0290 16.0709 0.0031 7 1,000 87 E10 US06 MS34009418 2/25/2014 0.0531 0.0305 0.0246 2.3869 0.0259 513.6580 16.0671 0.0256 7 1,000 87 E10 US FTP MS34009428 2/27/2014 0.0529 0.0185 0.0356 0.7650 0.0120 502.2330 16.5130 0.0370 7 1,000 87 E10 LA92 MS34009429 2/27/2014 0.0161 0.0124 0.0045 0.8438 0.0007 513.7360 16.1438 0.0047 7 1,000 87 E10 US06 MS34009430 2/27/2014 0.0480 0.0282 0.0217 2.0485 0.0200 512.8320 16.1099 0.0226 7 1,000 87 E10 US FTP MS34009434 2/28/2014 0.0601 0.0202 0.0413 0.8736 |
| 7 1,000 87 E10 US06 MS34009418 2/25/2014 0.0305 0.0246 2.3869 0.0259 513.6580 16.0671 0.0256 7 1,000 87 E10 US FTP MS34009428 2/27/2014 0.0529 0.0185 0.0356 0.7650 0.0120 502.2330 16.5130 0.0370 7 1,000 87 E10 LA92 MS34009429 2/27/2014 0.0161 0.0124 0.0045 0.8438 0.0007 513.7360 16.1438 0.0047 7 1,000 87 E10 US06 MS34009430 2/27/2014 0.0480 0.0222 0.0217 2.0485 0.0200 512.8320 16.1099 0.0226 7 1,000 87 E10 US FTP MS34009434 2/28/2014 0.0601 0.0202 0.0413 0.8736 0.0115 503.4200 16.4679 0.0429 8 5,000 87 E10 US FTP 782012130059-4 12/10/2013 0.0152 0.0026 0.0127 0.1066 0.0105 |
| 7 1,000 87 E10 US FTP MS34009428 2/27/2014 0.0529 0.0185 0.0356 0.7650 0.0120 502.2330 16.5130 0.0370 7 1,000 87 E10 LA92 MS34009429 2/27/2014 0.0161 0.0124 0.0045 0.8438 0.0007 513.7360 16.1438 0.0047 7 1,000 87 E10 US06 MS34009430 2/27/2014 0.0480 0.0282 0.0217 2.0485 0.0200 512.8320 16.1099 0.0226 7 1,000 87 E10 US FTP MS34009434 2/28/2014 0.0601 0.0202 0.0413 0.8736 0.0115 503.4200 16.4679 0.0429 8 5,000 87 E10 US FTP 782012130059-4 12/10/2013 0.0122 0.0026 0.0127 0.1066 0.0105 415.4000 20.0718 0.0140 8 5,000 87 E10 LA92 782012130059-6 12/10/2013 0.0023 0.00205 0.2941 0.0083 |
| 7 1,000 87 E10 LA92 MS34009429 2/27/2014 0.0161 0.0124 0.0045 0.8438 0.0007 513.7360 16.1438 0.0047 7 1,000 87 E10 US06 MS34009430 2/27/2014 0.0480 0.0282 0.0217 2.0485 0.0200 512.8320 16.1099 0.0226 7 1,000 87 E10 US FTP MS34009434 2/28/2014 0.0601 0.0202 0.0413 0.8736 0.0115 503.4200 16.4679 0.0429 8 5,000 87 E10 US FTP 782012130059-4 12/10/2013 0.0122 0.0026 0.0127 0.1066 0.0105 415.4000 20.0718 0.0140 8 5,000 87 E10 LA92 782012130059-6 12/10/2013 0.0023 0.0020 0.00055 0.2941 0.0083 429.6030 19.4077 0.0035 8 5,000 87 E10 US06 782012130059-7 12/10/2013 0.0067 0.0031 0.0037 8.8 |
| 7 1,000 87 E10 US06 MS34009430 2/27/2014 0.0480 0.0282 0.0217 2.0485 0.0200 512.8320 16.1099 0.0226 7 1,000 87 E10 US FTP MS34009434 2/28/2014 0.0601 0.0202 0.0413 0.8736 0.0115 503.4200 16.4679 0.0429 8 5,000 87 E10 US FTP 782012130059-4 12/10/2013 0.0122 0.0012 0.1066 0.0105 415.4000 20.0718 0.0140 8 5,000 87 E10 LA92 782012130059-6 12/10/2013 0.0023 0.0020 0.0005 0.2941 0.0083 429.6030 19.4077 0.0005 8 5,000 87 E10 US06 782012130059-7 12/10/2013 0.0027 0.0037 8.8330 0.0088 424.3000 19.0713 0.0038 |
| 7 1,000 87 E10 US FTP MS34009434 2/28/2014 0.0601 0.0202 0.0413 0.8736 0.0115 503.4200 16.4679 0.0429 8 5,000 87 E10 US FTP 782012130059-4 12/10/2013 0.0152 0.0026 0.0127 0.1066 0.0105 415.4000 20.0718 0.0140 8 5,000 87 E10 LA92 782012130059-6 12/10/2013 0.0023 0.0020 0.0005 0.2941 0.0083 429.6030 19.4077 0.0005 8 5,000 87 E10 US06 782012130059-7 12/10/2013 0.0027 0.0037 8.8330 0.0088 424.3000 19.0713 0.0038 |
| 8 5,000 87 E10 US FTP 782012130059-4 12/10/2013 0.0152 0.0026 0.0127 0.1066 0.0105 415.4000 20.0718 0.0140 8 5,000 87 E10 LA92 782012130059-6 12/10/2013 0.0023 0.0020 0.0005 0.2941 0.0083 429.6030 19.4077 0.0005 8 5,000 87 E10 US06 782012130059-7 12/10/2013 0.0067 0.0031 0.0037 8.8330 0.0088 424.3000 19.0713 0.0038 |
| 8 5,000 87 E10 LA92 782012130059-6 12/10/2013 0.0023 0.0020 0.0005 0.2941 0.0083 429.6030 19.4077 0.0005 8 5,000 87 E10 US06 782012130059-7 12/10/2013 0.0067 0.0031 0.0037 8.8330 0.0088 424.3000 19.0713 0.0038 |
| 8 5,000 87 E10 US06 782012130059-7 12/10/2013 0.0067 0.0031 0.0037 8.8330 0.0088 424.3000 19.0713 0.0038 |
| |
| 8 5,000 87 E10 US FTP 782012130059-8 12/10/2013 0.0166 0.0028 0.0145 0.1224 0.0087 411.7431 20.2655 0.0159 |
| 8 5,000 87 E10 LA92 782012130059-10 12/10/2013 0.0017 0.0018 0.0001 0.2796 0.0134 427.6722 19.4989 0.0001 |
| 8 5,000 87 E10 US06 782012130059-11 12/10/2013 0.0059 0.0034 0.0026 9.4689 0.0100 422.2000 19.1149 0.0027 |
| 8 1,000 87 E10 US FTP 782012130059–13 12/11/2013 0.0122 0.0029 0.0100 0.0993 0.0079 427.1895 19.5561 0.0109 |
| 8 1,000 87 E10 LA92 782012130059-15 12/11/2013 0.0023 0.0022 0.0005 0.1698 0.0071 438.4525 19.0183 0.0005 |
| 8 1,000 87 E10 US06 782012130059-16 12/11/2013 0.0042 0.0024 0.0019 9.9875 0.0214 445.6000 18.0877 0.0019 |
| 8 1,000 87 E10 US FTP 782012130059-17 12/12/2013 0.0130 0.0029 0.0106 0.1199 0.0124 428.9594 19.4634 0.0117 |
| 8 1,000 87 E10 LA92 782012130059-19 12/12/2013 0.0019 0.0022 0.0001 0.3111 0.0158 436.8435 19.0958 0.0002 |
| 8 1,000 87 E10 US06 782012130059-20 12/12/2013 0.0033 0.0019 0.0015 6.9615 0.0487 444.4000 18.3566 0.0015 |
| 8 1,000 87 E10 US FTP 782012130062-1 12/16/2013 0.0163 0.0033 0.0135 0.1144 0.0105 423.8106 19.6931 0.0148 |
| 8 1,000 87 E10 LA92 782012130062-3 12/16/2013 0.0032 0.0025 0.0008 0.3340 0.0161 435.5563 19.1381 0.0008 |
| 8 1,000 87 E10 US06 782012130062-4 12/16/2013 0.0047 0.0023 0.0025 8.7338 0.0147 445.1000 18.2051 0.0025 |
| 8 5,000 85 E10 US FTP 782012130061-4 12/18/2013 0.0163 0.0028 0.0136 0.1095 0.0088 413.6739 20.0921 0.0150 |
| 8 5,000 85 E10 LA92 782012130061-6 12/19/2013 0.0019 0.0021 0.0002 0.4641 0.0060 426.0632 19.5031 0.0002 |
| 8 5,000 85 E10 US06 782012130061-7 12/19/2013 0.0043 0.0023 0.0021 11.0671 0.0271 427.7000 18.6785 0.0022 |
| 8 5,000 85 E10 US FTP 782012130061-8 1/3/2014 0.0170 0.0031 0.0144 0.1048 0.0086 414.1566 20.0926 0.0159 |
| 8 5,000 85 E10 LA92 782012130061-10 1/3/2014 0.0019 0.0021 0.0002 0.5369 0.0114 429.4421 19.3162 0.0002 |
| 8 5,000 85 E10 US06 782012130061-11 1/3/2014 0.0037 0.0018 0.0019 7.7974 0.0305 427.6000 18.8965 0.0020 |
| 8 5,000 85 E10 US FTP 782012140002-1 1/8/2014 0.0178 0.0033 0.0152 0.1092 0.0101 415.0000 20.0362 0.0167 |
| 8 5,000 85 E10 LA92 782012140002-3 1/8/2014 0.0014 0.0020 0.0001 0.3629 0.0080 420.2000 19.7817 0.0001 |
| 8 5,000 85 E10 US FTP 782012140003-1 1/9/2014 0.0173 0.0034 0.0143 0.1133 0.0090 419.1000 19.8451 0.0158 |
| 8 5,000 85 E10 LA92 782012140003-3 1/9/2014 0.0016 0.0019 0.0002 0.3046 0.0071 425.9000 19.5076 0.0002 |
| 8 5,000 85 E10 US06 782012140003-4 1/9/2014 0.0034 0.0022 0.0014 11.2021 0.0305 439.4000 18.2203 0.0014 |
| 8 5,000 85 E10 US06 782012140003-5 1/9/2014 0.0031 0.0018 0.0013 8.4113 0.0266 430.3000 18.7705 0.0014 |
| 8 1,000 85 E10 US FTP 782012130061-13 1/9/2014 0.0147 0.0030 0.0120 0.0988 0.0079 425.2587 19.5730 0.0132 |
| 8 1,000 85 E10 LA92 782012130061-15 1/10/2014 0.0034 0.0027 0.0009 0.7976 0.0108 435.2345 19.0768 0.0009 |
| 8 1,000 85 E10 US06 782012130061-16 1/10/2014 0.0035 0.0021 0.0015 10.1682 0.0221 452.8000 17.7393 0.0015 |

| VNumber | Altitude | Fuel | TestCycle | TestID | TestDate | THC | CH4 | NonMethane | СО | Nox | CO2 | FE | NMOG |
|---------|----------|--------|-----------|------------|-----------|----------|----------|------------|----------|----------|----------|---------|----------|
| | (ft) | | | | | (g/mile) | (g/mile) | (g/mile) | (g/mile) | (g/mile) | (g/mile) | (mpg) | (g/mile) |
| 9 | 5,000 | 87 E10 | US FTP | MS34009554 | 3/18/2014 | 0.1666 | 0.0774 | 0.0944 | 0.9827 | 0.0062 | 396.6650 | 20.8569 | 0.0982 |
| 9 | 5,000 | 87 E10 | LA92 | MS34009555 | 3/18/2014 | 0.0785 | 0.0523 | 0.0297 | 0.7138 | 0.0126 | 386.3810 | 21.4470 | 0.0309 |
| 9 | 5,000 | 87 E10 | US06 | MS34009556 | 3/18/2014 | 0.1320 | 0.0667 | 0.0699 | 1.4788 | 0.0860 | 377.9270 | 21.8466 | 0.0727 |
| 9 | 5,000 | 87 E10 | US FTP | MS34009610 | 3/24/2014 | 0.1726 | 0.0846 | 0.0938 | 0.8948 | 0.0058 | 397.9980 | 20.7936 | 0.0975 |
| 9 | 5,000 | 87 E10 | LA92 | MS34009611 | 3/24/2014 | 0.0834 | 0.0529 | 0.0341 | 0.7982 | 0.0096 | 386.0090 | 21.4595 | 0.0355 |
| 9 | 5,000 | 87 E10 | US06 | MS34009612 | 3/24/2014 | 0.1265 | 0.0645 | 0.0663 | 1.4319 | 0.0484 | 378.0430 | 21.8451 | 0.0690 |
| 9 | 1,000 | 87 E10 | US FTP | MS34009626 | 3/26/2014 | 0.1493 | 0.0781 | 0.0765 | 1.1655 | 0.0038 | 409.0740 | 20.2158 | 0.0796 |
| 9 | 1,000 | 87 E10 | LA92 | MS34009627 | 3/27/2014 | 0.0732 | 0.0465 | 0.0299 | 0.6391 | 0.0086 | 392.9030 | 21.0994 | 0.0311 |
| 9 | 1,000 | 87 E10 | US06 | MS34009628 | 3/27/2014 | 0.1112 | 0.0561 | 0.0589 | 1.2028 | 0.0433 | 382.0990 | 21.6376 | 0.0613 |
| 9 | 1,000 | 87 E10 | US FTP | MS34009633 | 3/28/2014 | 0.1472 | 0.0813 | 0.0714 | 0.7672 | 0.0054 | 410.6380 | 20.1701 | 0.0742 |
| 9 | 1,000 | 87 E10 | LA92 | MS34009634 | 3/28/2014 | 0.0915 | 0.0519 | 0.0431 | 0.7314 | 0.0098 | 392.6400 | 21.1028 | 0.0448 |
| 9 | 1,000 | 87 E10 | US06 | MS34009635 | 3/28/2014 | 0.1078 | 0.0546 | 0.0569 | 1.1986 | 0.0358 | 374.5180 | 22.0740 | 0.0592 |
| 9 | 1,000 | 87 E10 | US FTP | MS34009676 | 4/3/2014 | 0.1408 | 0.0743 | 0.0716 | 0.8343 | 0.0033 | 407.9530 | 20.2980 | 0.0744 |
| 9 | 1,000 | 87 E10 | LA92 | MS34009677 | 4/3/2014 | 0.0734 | 0.0437 | 0.0327 | 0.5551 | 0.0086 | 392.7200 | 21.1162 | 0.0340 |
| 9 | 1,000 | 87 E10 | US06 | MS34009678 | 4/3/2014 | 0.1213 | 0.0581 | 0.0671 | 1.2055 | 0.0564 | 377.7700 | 21.8822 | 0.0698 |
| 9 | 5,000 | 85 E10 | US FTP | MS34009693 | 4/10/2014 | 0.1756 | 0.0761 | 0.1047 | 1.2217 | 0.0066 | 392.3220 | 21.0473 | 0.1089 |
| 9 | 5,000 | 85 E10 | LA92 | MS34009694 | 4/11/2014 | 0.0929 | 0.0540 | 0.0426 | 0.7622 | 0.0088 | 386.3550 | 21.4237 | 0.0443 |
| 9 | 5,000 | 85 E10 | US06 | MS34009695 | 4/11/2014 | 0.1248 | 0.0631 | 0.0660 | 1.4863 | 0.0486 | 383.3630 | 21.5212 | 0.0686 |
| 9 | 5,000 | 85 E10 | LA92 | MS35004794 | 4/14/2014 | 0.0898 | 0.0538 | 0.0391 | 0.8410 | 0.0087 | 391.0130 | 21.1633 | 0.0407 |
| 9 | 5,000 | 85 E10 | US06 | MS35004795 | 4/14/2014 | 0.1143 | 0.0593 | 0.0585 | 1.4867 | 0.0430 | 385.0610 | 21.4287 | 0.0608 |
| 9 | 5,000 | 85 E10 | US FTP | MS35004800 | 4/15/2014 | 0.1659 | 0.0861 | 0.0849 | 0.9425 | 0.0053 | 398.1170 | 20.7670 | 0.0883 |
| 9 | 1,000 | 85 E10 | US FTP | MS35004853 | 4/24/2014 | 0.1533 | 0.0774 | 0.0805 | 1.1966 | 0.0054 | 413.2000 | 19.9951 | 0.0837 |
| 9 | 1,000 | 85 E10 | LA92 | MS35004854 | 4/24/2014 | 0.0784 | 0.0476 | 0.0336 | 0.7445 | 0.0091 | 401.1310 | 20.6411 | 0.0349 |
| 9 | 1,000 | 85 E10 | US06 | MS35004855 | 4/24/2014 | 0.1141 | 0.0568 | 0.0606 | 1.5964 | 0.0452 | 393.6820 | 20.9536 | 0.0630 |
| 9 | 1,000 | 85 E10 | US FTP | MS35004886 | 5/1/2014 | 0.1243 | 0.0722 | 0.0564 | 0.6353 | 0.0070 | 412.1880 | 20.0909 | 0.0587 |
| 9 | 1,000 | 85 E10 | LA92 | MS35004887 | 5/1/2014 | 0.0678 | 0.0439 | 0.0265 | 0.6429 | 0.0097 | 404.2530 | 20.4919 | 0.0275 |
| 9 | 1,000 | 85 E10 | US06 | MS35004888 | 5/1/2014 | 0.1310 | 0.0653 | 0.0696 | 3.1553 | 0.0463 | 397.2420 | 20.6382 | 0.0724 |
| 9 | 1,000 | 85 E10 | US FTP | MS35004894 | 5/2/2014 | 0.1226 | 0.0732 | 0.0537 | 0.6159 | 0.0053 | 412.0990 | 20.0970 | 0.0559 |
| 9 | 1,000 | 85 E10 | LA92 | MS35004895 | 5/2/2014 | 0.0623 | 0.0427 | 0.0222 | 0.5823 | 0.0081 | 400.2250 | 20.7033 | 0.0230 |
| 9 | 1,000 | 85 E10 | US06 | MS35004896 | 5/2/2014 | 0.1068 | 0.0541 | 0.0559 | 1.7064 | 0.0376 | 392.9020 | 20.9868 | 0.0582 |

I. Vehicle Performance Data – Core Data (85 and 87 AKI)

| Vnumber | Altitude | Fuel | Test Cycle | Date | Vehicle | Engine | Throttle | Load | Ignition Timing | Exhaust Temp - | Catalyst Temp - | Exhaust Temp - | Catalyst Temp - |
|---------|----------|---------|-----------------------------------|------------|---------|------------------|----------|-------|--------------------|----------------|-----------------|----------------|------------------|
| | | | | | (mph) | (rnm) | (%) | (%) | (deg BTDC) | (deg. C) | (deg. C) | (deg. C) | (deg. C) |
| 1 | 5,000 | 87 E10 | FTP-1 (Bag 3) | 9/11/2013 | 25.13 | 1413.5 | 18.21 | 27.73 | 18.83 | 461.4 | 587.2 | 675.7 | 744.9 |
| 1 | 5,000 | 87 E10 | LA92 | 9/11/2013 | 24.93 | 1476.0 | 19.18 | 28.58 | 16.20 | 500.9 | 637.8 | 754.2 | 830.7 |
| 1 | 5,000 | 87 E10 | US06 (2nd) | 9/11/2013 | 47.98 | 2284.5 | 27.29 | 38.94 | 19.10 | 594.2 | 747.2 | 806.4 | 877.0 |
| 1 | 5,000 | 87 E10 | FTP-2 (Bags 1 & 2) | 9/12/2013 | 19.43 | 1337.6 | 17.21 | 25.98 | 20.20 | 441.0 | 558.0 | 694.6 | 752.0 |
| 1 | 5,000 | 87 E10 | FTP-2 (Bag3) | 9/12/2013 | 25.04 | 1403.9 | 18.01 | 27.58 | 17.87 | 458.6 | 589.4 | 665.1 | 737.6 |
| 1 | 5,000 | 87 E10 | LA92 | 9/12/2013 | 24.90 | 1476.1 | 18.92 | 28.52 | 16.57 | 494.3 | 629.6 | 741.6 | 821.9 |
| 1 | 5,000 | 87 E10 | USU6 (2nd) | 9/12/2013 | 48.15 | 12270.3 | 27.12 | 38.93 | 18.33 | 592.1 | 744.9 | 814.0 690.9 | 895.1 |
| 1 | 1,000 | 87 E10 | FTP-1 (Bag 3) | 9/18/2013 | 25.29 | 1322.7 | 17 22 | 20.37 | 18.62 | 451.8 | 580.8 | 670.0 | 734.4 |
| 1 | 1.000 | 87 E10 | LA92 | 9/18/2013 | 25.13 | 1452.8 | 17.88 | 29.63 | 16.17 | 503.2 | 630.3 | 764.2 | 847.7 |
| 1 | 1,000 | 87 E10 | US06 (2nd) | 9/18/2013 | 48.41 | 2209.3 | 24.67 | 40.26 | 18.70 | 601.7 | 749.6 | 862.6 | 942.4 |
| 1 | 1,000 | 87 E10 | FTP-4 (Bags 1 & 2) | 9/19/2013 | 19.59 | 1325.4 | 16.49 | 26.85 | 19.99 | 453.8 | 562.8 | 681.8 | 747.8 |
| 1 | 1,000 | 87 E10 | FTP-2 (Bag3) | 9/19/2013 | 25.34 | 1394.7 | 17.22 | 28.98 | 18.28 | 468.7 | 586.1 | 683.4 | 695.7 |
| 1 | 1,000 | 87 E10 | LA92 | 9/19/2013 | 24.80 | 1445.4 | 18.00 | 29.59 | 15.78 | 502.5 | 631.9 | 782.7 | 860.1 |
| 1 | 5,000 | 85 E10 | FTP-1 (Bags 1 & 2) | 9/23/2013 | 19.56 | 1342.3 | 17.18 | 25.83 | 19.70 | 446.1 | 560.7 | 691.6 | 756.2 |
| 1 | 5,000 | 85 E10 | FIP-1 (Bag 3) | 9/23/2013 | 24.86 | 1397.7 | 18.18 | 28.02 | 17.30 | 467.0 | 596.0 | 702.4 | 766.9 |
| 1 | 5,000 | 85 E10 | US06 (2nd) | 9/23/2013 | 48 58 | 2293.1 | 27.64 | 38.66 | 17.55 | 608.2 | 755.4 | 815.5 | 887.0 |
| 1 | 5.000 | 85 E10 | FTP-2 (Bags 1 & 2) | 9/24/2013 | 19.57 | 1343.0 | 17.16 | 25.92 | 20.26 | 448.4 | 564.9 | 697.4 | 764.9 |
| 1 | 5,000 | 85 E10 | FTP-2 (Bag3) | 9/24/2013 | 24.41 | 1390.6 | 18.12 | 27.52 | 17.38 | 467.0 | 595.0 | 680.2 | 746.4 |
| 1 | 5,000 | 85 E10 | LA92 | 9/24/2013 | 25.11 | 1488.7 | 19.34 | 28.65 | 15.48 | 506.7 | 644.6 | 760.5 | 847.8 |
| 1 | 5,000 | 85 E10 | US06 (2nd) | 9/24/2013 | 48.66 | 2314.1 | 27.77 | 38.73 | 17.88 | 604.6 | 755.4 | 829.8 | 896.0 |
| 1 | 1,000 | 85 E10 | FTP-3 (Bags 1 & 2) | 10/1/2013 | 19.55 | 1323.6 | 16.48 | 26.76 | 20.20 | 449.5 | 561.9 | 686.1 | 754.9 |
| 1 | 1,000 | 85 E10 | FTP-3 (Bag3) | 10/1/2013 | 25.20 | 1388.9 | 17.38 | 29.28 | 17.30 | 474.3 | 594.5 | 682.2 | 752.3 |
| 1 | 1,000 | 85 E10 | LA92 | 10/1/2013 | 24.92 | 1459.8 | 18.02 | 29.55 | 15.55 | 506.8 | 639.9 | 813.1 | 862.2 |
| 1 | 1,000 | 85 E10 | FTP-4 (Bags 1 & 2) | 10/1/2013 | 40.49 | 1324.0 | 16 53 | 26.82 | 19.59 | 452.3 | 733.8 562.1 | 692.2 | 763.6 |
| 1 | 1.000 | 85 E10 | FTP-4 (Bag 3) | 10/3/2013 | 25.36 | 1397.7 | 17.38 | 29.27 | 17.23 | 475.8 | 598.7 | 708.1 | 777.3 |
| 1 | 1,000 | 85 E10 | LA92 | 10/3/2013 | 25.04 | 1460.7 | 18.12 | 29.90 | 15.38 | 507.1 | 640.0 | 807.3 | 878.5 |
| 1 | 1,000 | 85 E10 | US06 (2nd) | 10/3/2013 | 48.18 | 2214.5 | 25.30 | 41.30 | 17.17 | 608.7 | 759.2 | 876.1 | 932.5 |
| 2 | 5,000 | 87 E10 | FTP-1 (Bags 1 & 2) | 11/5/2013 | 19.22 | 1247.2 | 16.38 | 25.19 | 27.00 | 467.3 | 570.3 | 616.0 | 701.8 |
| 2 | 5,000 | 87 E10 | FTP-1(Bag 3) | 11/5/2013 | 25.79 | 1378.6 | 17.10 | 26.16 | 28.09 | 484.8 | 591.1 | 640.5 | 722.5 |
| 2 | 5,000 | 87 E10 | LA92 | 11/5/2013 | 24.58 | 1390.9 | 17.71 | 26.74 | 26.85 | 527.4 | 634.2 | 726.9 | 809.7 |
| 2 | 5,000 | 87 E10 | USU6 (2nd) | 11/5/2013 | 48.34 | 2124.8 | 25.18 | 35.21 | 29.55 | 633.2 | 746.7 | 823.5 619 7 | 915.8 |
| 2 | 5,000 | 87 E10 | FTP-2 (Bags 1 & 2) | 11/7/2013 | 25.16 | 1373.9 | 17.28 | 24.30 | 20.85 | 470.0 | 591.8 | 641.7 | 739.6 |
| 2 | 5,000 | 87 E10 | LA92 | 11/7/2013 | 24.80 | 1404.8 | 17.68 | 26.59 | 27.14 | 531.0 | 636.7 | 733.2 | 815.7 |
| 2 | 5,000 | 87 E10 | US06 (2nd) | 11/7/2013 | 48.25 | 2113.1 | 25.13 | 35.35 | 29.27 | 636.4 | 750.9 | 838.7 | 911.3 |
| 2 | 5,000 | 87 E10 | FTP-3 (Bags 1 & 2) | 11/8/2013 | 19.24 | 1254.4 | 16.37 | 25.14 | 27.00 | 467.0 | 572.2 | 616.6 | 713.6 |
| 2 | 5,000 | 87 E10 | FTP-2 (Bag 3) | 11/8/2013 | 25.06 | 1370.2 | 16.99 | 25.76 | 27.24 | 480.4 | 586.1 | 641.8 | 732.0 |
| 2 | 5,000 | 87 E10 | LA92 | 11/8/2013 | 24.84 | 1399.4 | 17.69 | 26.73 | 27.08 | 528.1 | 634.4 | 726.3 | 818.6 |
| 2 | 5,000 | 87 E10 | US06 (2nd) | 11/8/2013 | 47.95 | 2108.1 | 25.12 | 35.05 | 29.51 | 630.1 | 747.2 | 807.2 | 880.8 |
| 2 | 1,000 | 87 E10 | FTP-1 (Bags 1 & 2) | 11/10/2013 | 25.14 | 1237.8 | 15.80 | 20.33 | 20.03 | 4/1.8 | 572.9 | 632.0 | 712 4 |
| 2 | 1,000 | 87 F10 | 1492 | 11/10/2013 | 23.14 | 1386.1 | 16.55 | 27.69 | 27.10 | 528.7 | 631.3 | 725.3 | 806.5 |
| 2 | 1,000 | 87 E10 | US06 (2nd) | 11/10/2013 | 48.06 | 2059.3 | 22.29 | 36.65 | 30.18 | 628.7 | 739.4 | 843.2 | 931.4 |
| 2 | 1,000 | 87 E10 | FTP-3 (Bags 1 & 2) | 11/14/2013 | 19.30 | 1249.0 | 15.83 | 26.25 | 26.95 | 472.3 | 575.0 | 602.8 | 702.5 |
| 2 | 1,000 | 87 E10 | FTP-3 (Bag 3) | 11/14/2013 | 24.97 | 1360.2 | 16.57 | 26.99 | 27.49 | 484.5 | 586.5 | 625.0 | 711.5 |
| 2 | 1,000 | 87 E10 | FTP-4 (Bags 1 & 2) | 11/18/2013 | 19.24 | 1246.0 | 15.79 | 26.00 | 26.56 | 471.3 | 572.8 | 607.6 | 693.7 |
| 2 | 1,000 | 87 E10 | FTP-4 (Bag 3) | 11/18/2013 | 24.97 | 1356.8 | 16.48 | 26.72 | 27.40 | 483.9 | 585.4 | 633.0 | 710.4 |
| 2 | 1,000 | 87 E10 | LA92 | 11/19/2013 | 24.66 | 1382.0 | 16.68 | 27.73 | 26.95 | 523.1 | 626.2 | 719.0 | 803.8 |
| 2 | 5,000 | 85 F10 | FTP-1 (Rags 1 8 2) | 11/21/2013 | 46.29 | 2055.1 1741 1 | 16 36 | 24 09 | 26.67 | 025.7 462 Q | 565 5 | 769.7 613 0 | 675.9 702 1 |
| 2 | 5,000 | 85 E10 | FTP-1 (Bag 3) | 11/21/2013 | 24.89 | 1368.2 | 16.98 | 25.56 | 26.99 | 480.5 | 583.0 | 631.3 | 717.4 |
| 2 | 5,000 | 85 E10 | LA92 | 11/21/2013 | 24.81 | 1403.3 | 17.96 | 26.49 | 26.75 | 520.5 | 629.8 | 728.8 | 816.6 |
| 2 | 5,000 | 85 E10 | US06 (2nd) | 11/21/2013 | 48.09 | 2126.7 | 25.18 | 34.94 | 29.46 | 634.0 | 745.8 | 846.3 | 914.9 |
| 2 | 5,000 | 85 E10 | FTP-2 (Bags 1 & 2) | 11/22/2013 | 19.24 | 1250.7 | 16.36 | 24.73 | 26.70 | 466.1 | 571.5 | 607.6 | 693.9 |
| 2 | 5,000 | 85 E10 | FTP-2 (Bag 3) | 11/22/2013 | 25.00 | 1366.6 | 17.18 | 25.68 | 26.94 | 481.7 | 588.0 | 636.3 | 732.6 |
| 2 | 5,000 | 85 E10 | | 11/22/2013 | 24.73 | 1406.9 | 17.87 | 26.30 | 26.63 | 525.9 | 634.7 | 732.9 | 819.7 |
| 2 | 5,000 | 03 E10 | USUD (200) FTP-3 (Rage 1 9. 2) | 11/26/2012 | 48.37 | 1250 5 | 16.35 | 2/ 00 | 29.35 | 033.3 AG5 2 | 747.5 570 5 | 8/4.U 611 1 | - 509.7 600 7 |
| 2 | 5,000 | 85 F10 | FTP-3 (Bag 3) | 11/26/2013 | 25 12 | 1371 4 | 17 35 | 25.96 | 27.03 | 481 7 | 585.8 | 641.6 | 733.4 |
| 2 | 5,000 | 85 E10 | LA92 | 11/26/2013 | 24.78 | 1400.8 | 17.70 | 26.53 | 26.93 | 524.9 | 632.6 | 708.9 | 799.5 |
| 2 | 1,000 | 85 E10 | LA92 | 11/26/2013 | 24.67 | 1377.7 | 16.87 | 27.56 | 26.78 | 526.4 | 627.6 | 727.9 | 805.4 |
| 2 | 5,000 | 85 E10 | US06 (2nd) | 11/26/2013 | 48.28 | 2130.7 | 24.99 | 35.36 | 29.22 | 637.6 | 748.7 | 872.2 | 957.1 |
| 2 | 1,000 | 85 E10 | US06 (2nd) | 11/26/2013 | 47.93 | 2075.7 | 22.59 | 36.46 | 29.43 | 629.4 | 739.4 | 841.4 | 910.4 |
| 2 | 1,000 | 85 E10 | FTP-1 (Bags 1 & 2) | 11/27/2013 | 19.31 | 1244.3 | 15.81 | 26.13 | 26.95 | 471.0 | 571.9 | 604.5 | 684.0 |
| 2 | 1,000 | 85 E10 | FTP-1 (Bag 3) | 11/27/2013 | 25.04 | 1361.3 | 16.29 | 26.75 | 27.24 | 485.9 | 586.5 | 623.0 | 706.3 |
| 2 | 1,000 | 85 E10 | FTP-2 (Bags 1 & 2) | 12/5/2013 | 19.28 | 1250 1 | 15.85 | 26.22 | 27.01 | 4/4.2 | 5/6.3 | 636.2 | 589.6 709 E |
| 2 | 1.000 | 85 E10 | LA92 | 12/5/2013 | 24.77 | 1387 3 | 16.91 | 27.61 | 26.64 | 532.1 | 635.3 | 733.0 | 816.7 |
| 2 | 1,000 | 85 E10 | US06 (2nd) | 12/5/2013 | 48.52 | 2103.7 | 22.35 | 36.63 | 30.05 | 635.6 | 742.8 | 864.6 | 924.3 |
| 2 | 1,000 | 85 E 10 | FTP-3 (Bags 1 & 2) | 12/6/2013 | 19.61 | 1246.5 | 15.77 | 25.72 | 27.80 | 475.3 | 580.4 | 606.3 | 688.8 |
| 2 | 1,000 | 85 E10 | FTP-3 (Bag3) | 12/6/2013 | 24.93 | 1361.5 | 16.44 | 26.92 | 27.52 | 486.0 | 587.4 | 642.4 | 718.7 |
| 2 | 1,000 | 85 E10 | LA92 | 12/6/2013 | 24.77 | 1387.3 | 17.02 | 27.93 | 26.59 | 530.3 | 633.4 | 749.5 | 839.0 |
| 2 | 1,000 | 85 E10 | US06 (2nd) | 12/6/2013 | 47.92 | 2059.8 | 22.69 | 37.12 | 28.75 | 630.6 | 740.3 | 875.3 | 968.2 |

| number number number number space Space Pole Number | Vnumber | Altitudo | Fuel | Test Cycle | Date | Vehicle | Engine | Throttle | Load | Ignition | Exhaust Temp - | Catalyst Temp - | Exhaust Temp - | Catalyst Temp - |
|--|---------|----------|--------|----------------------------------|------------|----------------|------------------|----------------|----------------|----------------|----------------|-----------------|----------------|-----------------|
| s. c.v.m rum rum <thr></thr> | vnumber | Annuae | ruei | Test Cycle | Date | Speed | Speed | Position | LOau | Timing | PreCat Avg. | MidCat Avg. | PreCat Max. | MidCat Max. |
| 8 9 1 1 1 1 1 | | | | | /= /= | (mph) | (rpm) | (%) | (%) | (deg BTDC) | (deg. C) | (deg. C) | (deg. C) | (deg. C) |
| s b< b< b< b< b< <td>3</td> <td>5,000</td> <td>85 E10</td> <td>FTP-1 (Bags 1 & 2)</td> <td>11/5/2013</td> <td>19.75</td> <td>1282.9</td> <td>18.69</td> <td>26.73</td> <td>22.39</td> <td>477.2</td> <td>581.5</td> <td>651.0</td> <td>726.8</td> | 3 | 5,000 | 85 E10 | FTP-1 (Bags 1 & 2) | 11/5/2013 | 19.75 | 1282.9 | 18.69 | 26.73 | 22.39 | 477.2 | 581.5 | 651.0 | 726.8 |
| 3 1.000 PC10 P | 3 | 5,000 | 85 E10 | FTP-2 (Bags 1 & 2) | 11/6/2013 | 19.77 | 12/3.9 | 18.74 | 26.81 | 21.78 | 468.3 | 574.0 | 658.7 | 730.1 |
| 3 1.000 64:10 1.042 1.042,001 2.5.42 1.924 1.988 2.1.44 69.81 27.1.4 998.81 30.1.4 66.81 77.5.8 83.00 30.00 30.1.000 85.10 777.100 1.988 23.52 1.802 77.51 23.14 66.40 77.51 83.00 30.00 66.40 77.21 77.24 77.82 77.81 77.81 83.00 30.00 77.81 83.00 30.00 77.81 83.00 30.00 66.40 77.24 77.82.4 77.82 77.81 77.82.4 77.82 77.82 77.82 77.82 77.82 77.82 77.82.4 77.82 77.82 77.82 77.82 77.82 77.82 77.82 77.82 77.82 77.82 77.82 77.82 77.82 77.82 77.82 77.82 77.82 77.82 77.82 77.83 77.83 77.83 77.83 77.83 77.83 77.83 77.83 77.83 77.83 77.73 77.83 | 3 | 1,000 | 85 E10 | FTP-1 (Bag 3) | 11/10/2013 | 25 58 | 1390.0 | 18.02 | 20.00 | 21.38 | 405.5 | 592.8 | 659.3 | 723.0 |
| 5 1.000 69110 1000 2514 661.8 775.4 888.0 980.0 3 1.000 6110 TP 2/leg.1 111/1/200 25.5 188.2 16.2 21.9 <t< td=""><td>3</td><td>1,000</td><td>85 E10</td><td>LA92</td><td>11/10/2013</td><td>25.42</td><td>1422.8</td><td>18.98</td><td>28.88</td><td>22.74</td><td>532.4</td><td>647.5</td><td>727.4</td><td>798.8</td></t<> | 3 | 1,000 | 85 E10 | LA92 | 11/10/2013 | 25.42 | 1422.8 | 18.98 | 28.88 | 22.74 | 532.4 | 647.5 | 727.4 | 798.8 |
| 3 1.000 SETID TPT-2[leg1: 4.2 11/17/2013 29.8 1987 1878 27.05 23.14 49.25 99.55 64.8 77.14 5 1.000 Kriti Lok9 11/17/2013 25.29 188.0 24.06 54.01 12.10 47.17 84.0 44.01 5 1.000 Kriti Lok9 11/17/2013 45.0 24.00 42.01 43.0 44.0 44.0 5 Lok0 Kriti Lik1/42012 45.0 14.01 45.0 27.1 | 3 | 1,000 | 85 E10 | US06 (2nd) | 11/10/2013 | 48.98 | 2153.2 | 24.39 | 39.01 | 23.14 | 661.8 | 775.8 | 838.0 | 909.0 |
| 3 1.000 BSEID 117/2001 25.90 1882 1876 2877 21.44 99.22 99.56 98.34 772.1 3 1.000 BSEID USSE10.11/12/2013 45.69 28.83 23.1 667.4 775.7 788.4 998.4 3 1.000 BSEID TOPALISHING 35.90 27.13 1.000 BSEID 777.4 498.1 3 1.000 BSEID TOPALISHING 35.90 477.2 1.800 BSEID 1.800 27.14 1.800 27.14 1.800 1.80 | 3 | 1,000 | 85 E10 | FTP-2 (Bags 1 & 2) | 11/11/2013 | 19.68 | 1263.7 | 18.02 | 27.05 | 23.19 | | | | |
| 3 1.000 65120 1.002 1.11/2/031 4.60 24851 2486 2476 777 578.3 6440 772.4 7786 3 5.000 7107 717 1101011 1101/2001 4486 2186 2287 | 3 | 1,000 | 85 E10 | FTP-2 (Bag3) | 11/12/2013 | 25.59 | 1388.2 | 18.78 | 28.73 | 23.14 | 493.2 | 599.5 | 663.8 | 729.1 |
| 1 1.000 6513 1.005 1.001 1.00 | 3 | 1,000 | 85 E10 | LA92 | 11/12/2013 | 25.29 | 1419.7 | 18.90 | 28.85 | 22.65 | 530.0 | 644.4 | 722.4 | 792.4 |
| s 1.000 65:10 171-64 12/23 16/23 16/24 12/23 16/24 12/23 16/24 16 | 3 | 1,000 | 85 E10 | US06 (2nd) | 11/12/2013 | 48.69 | 2146.1 | 24.08 | 36.93 | 23.21 | 647.4 | 775.7 | 858.4 | 930.4 |
| 3 1.000 64.101 1.000 64.101 1.000 64.101 1.000 64.101 1.000 1.0100 1.0100 1.0100 | 3 | 1,000 | 85 E10 | FTP-4 (Bags 1 & 2) | 11/14/2013 | 19.68 | 12/2.3 | 18.1/ | 27.40 | 22.54 | 480.6 | 584.7 | /82.4 | 849.1 |
| 3 1.000 65 101 1.095 16rd 1.017/2013 49.19 2.366.4 25.24 35.80 77.10 | 3 | 1,000 | 85 E10 | FTP-3 (Bag 3) | 11/14/2013 | 25.43 | 1380.2 | 18.70 | 28.50 | 23.09 | 532.0 | 554.5 6/8 2 | 373.3 727 A | 554.5 794.0 |
| 3 500 9710 971-1 971-3 984.1 972-3 984.1 972-3 3 500 8710 771-1 100 107-1 100-4 1102 107-1 100-4 100-1 < | 3 | 1.000 | 85 E10 | US06 (2nd) | 11/14/2013 | 49.19 | 2146.4 | 23.74 | 35.89 | 24.72 | | | | |
| 3 5.000 97120 1772 (lbsg1 & 20) 1172/2003 27/3 12/6 14/6 15/8 27/7 22/40 <t< td=""><td>3</td><td>5,000</td><td>87 E10</td><td>FTP-1 (Bags 1 & 2)</td><td>11/21/2013</td><td>19.66</td><td>1264.8</td><td>18.69</td><td>26.29</td><td>22.17</td><td>470.7</td><td>574.3</td><td>649.4</td><td>722.4</td></t<> | 3 | 5,000 | 87 E10 | FTP-1 (Bags 1 & 2) | 11/21/2013 | 19.66 | 1264.8 | 18.69 | 26.29 | 22.17 | 470.7 | 574.3 | 649.4 | 722.4 |
| 3 5,000 37100 1710 | 3 | 5,000 | 87 E10 | FTP-2 (Bags 1 & 2) | 11/21/2013 | 19.71 | 1266.2 | 18.65 | 26.06 | 21.93 | | | | |
| 3 5,000 7710 L02 11/2/2013 25.10 7710 25.20 7710 25.20 7710 25.20 7710 25.20 7810 5800 78100 78100 78100 | 3 | 5,000 | 87 E10 | FTP-1 (Bag 3) | 11/21/2013 | 27.03 | 1416.0 | 19.58 | 27.81 | 22.78 | | | | |
| 3 5,000 87100 USO(2nd) 11/2/2003 2855 1302 24.13 24.43 638.6 779.7 819.5 819.5 3 5,000 87100 USO(2nd) 11/2/2013 25.5 130.8 27.32 22.33 582.1 664.0 7715.7 819.5 819.5 3 1,000 87100 USO(2nd) 11/2/2013 25.6 137.2 24.21 447.6 840.4 540.0 644.8 770.6 887.2 3 1,000 87100 UAG2 12/2/2013 25.61 1371.4 88.63 25.00 52.0 480.6 590.6 633.7 770.3 3 1,000 87100 UAG2 12/2/2013 25.20 15.07 12.40.0 12.40 11.41.20 12.48.8 24.01 462.7 711.0 700.5 733.5 3 1.000 871.0 USG2(2nd) 12.29 14.12.0 14.8.8 25.10 45.6 673.7 773.3 739.3 730.9< | 3 | 5,000 | 87 E10 | LA92 | 11/21/2013 | 25.19 | 1424.8 | 19.78 | 27.77 | 22.40 | | | | |
| 3 5,000 87100 197-2 (bg g) 11/2/2013 25.5 192.0 27.18 22.61 48.4 30.21 696.1 77.15 3 5,000 87100 1050 (2nd) 11/2/2013 45.96 22.19 25.15 34.47 24.89 641.2 77.96 80.77 888.3 3 1,000 87100 17.91 168.8 12.70 18.63 22.12 22.12 42.12 47.16 53.02 663.4 (79.0) 780.5 3 1,000 87100 17.97 18.02 22.11 12.12 18.83 28.30 52.10 462.2 50.05 77.0 60.09 70.05 3 1.000 87100 17.92 10.92 12.42 14.16.2 18.89 28.31 23.30 50.64 60.77 78.00 92.12 78.11 23.12 78.11 23.12 78.11 23.12 78.11 23.12 78.11 23.12 78.11 23.12 78.11 78.11 | 3 | 5,000 | 87 E10 | US06 (2nd) | 11/21/2013 | 48.83 | 2203.7 | 26.12 | 34.41 | 24.93 | 639.6 | 759.7 | 819.5 | 899.0 |
| 3 0.000 0.7100 1024/013 21.1 10.85 21.4 24.81 50.40 64.90 77.90 78.90 3 1.000 0.710 1710 1710 1710 1710 1710 1710 1710 17111 1711 1711 | 3 | 5,000 | 87 E10 | FTP-2 (Bag 3) | 11/22/2013 | 25.55 | 1392.6 | 19.49 | 27.18 | 22.61 | 483.4 | 592.1 | 646.1 | 715.5 |
| 5 1.000 0710 1791.08821 1.21/2013 1.200 1710 1791.0 1892.1 1.21/2013 125.0 1170.2 16.00 173.0 190.0 640.6 640.6 640.6 640.6 640.6 640.6 640.8 970.0 970.5 3 1.000 7710 1792.1 122.1 1172.2 162.1 1172.2 162.1 1172.2 162.1 1172.2 162.1 1172.2 1172.1 127.0 127.1 127.0 127.1 | 3 | 5,000 | 87 E10 | LA92 | 11/22/2013 | 25.17 | 1438.3 2211.0 | 19.83 | 27.32 | 22.33 | 528.1 | 544.0 759.6 | 729.0 | 795.4 |
| 3 1.000 271:0 1.27.2013 25.30 1.378.2 18.65 28.20 23.57 48.36 590.6 633.4 6990.5 3 1.000 871:0 179-2(8:g) 1.27/2013 125.71 1412.9 18.82 82.90 23.00 552.2 669.1 722.4 3 1.000 871:0 179.2(8:g) 1.27/2013 25.53 120.0 171.2 82.9 40.0 422.9 582.8 665.7 707.3 3 1.000 871:0 1.07(2011) 12/2013 128.51 124.0 94.1 132.2 669.8 662.3 70.5 70.7 840.0 922.0 3 1.000 871:0 179.2(8:g) 12/2013 125.51 126.7 136.00 92.31 126.2 70.5 70.7 32.50 566.5 51.6 61.2 70.0 3 1.000 871.0 156.0 71.6 92.3 124.2 45.0 13.6 72.5 72.5 72.5 72.5 72.5< | 3 | 1.000 | 87 E10 | FTP-1 (Bags 1 & 2) | 12/3/2013 | 19.68 | 1270.0 | 18.06 | 27.26 | 23.21 | 477.6 | 580.2 | 648.8 | 720.6 |
| 3 1.000 871:0 1.402 12/1/2013 12/2013 12/2013 12/204 131 270 23.10 77.1 582.2 693.1 732.4 3 1.000 871:0 TP2 (Bay 3) 12/1/2013 25.2 187.1 28.2 24.01 482.9 592.8 663.7 707.3 3 1.000 871:0 TP2 (Bay 3) 12/5/2013 42.8 183.3 23.30 552.4 662.3 718.2 780.1 3 1.000 871:0 TP2 (Bag 3) 12/5/2013 42.8 185.0 717.7 32.5 664.5 661.2 730.5 3 1.000 871:0 TP3 (Bag 3) 12/6/2013 25.31 1415.6 148.9 24.22 442.0 586.5 667.6 700.7 700.2 3 1.000 871:0 11/6/2013 25.31 1415.6 11.8 82.16 165.0 772.2 44.0 1.00 84.3 12.25 1.00 772.1 74.4 572. | 3 | 1,000 | 87 E10 | FTP-1 (Bag 3) | 12/3/2013 | 25.30 | 1378.2 | 18.63 | 28.20 | 23.57 | 483.6 | 590.6 | 633.4 | 699.0 |
| 3 1,000 8710 17P-2 (Bag) 12/2/2013 12864 1811 27.00 23.12 497.1 582.2 653.1 772.4 3 1,000 8710 17P-2 (Bag) 12/2/2013 25.3 146.2 18.89 23.3 23.0 252.4 642.9 71.8.2 799.1 3 1,000 8710 17P-2 (Bag) 12/2/2013 25.2 13.60 27.17 23.26 649.8 570.7 840.0 23.0 3 1,000 8710 17P-2 (Bag) 12/2/2013 25.1 1322.0 15.60 28.71 23.26 442.0 482.0 585.5 573.8 70.9< | 3 | 1,000 | 87 E10 | LA92 | 12/3/2013 | 25.21 | 1412.9 | 18.88 | 28.59 | 23.09 | 527.0 | 640.9 | 710.9 | 780.5 |
| 3 1,000 87:10 125/2013 25:63 1390.2 18:71 28:29 24.01 48:29 55:28 66:57 707.3 3 1,000 97:10 US06 (2nd) 125/2013 15:82 128:33 23:30 58:84 642.9 718.2 7783.1 3 1,000 97:10 US06 (2nd) 125/2013 15:81 126/2013 23:81 64:82 77.7 840.0 95:85 65:83 709.0 97:10 17:96 (2nd) 126/2013 15:31 13:82 92:33 124:42.0 58:85 65:33 709.9 84:5 97:25 77:2 77:2 77:31 77:35 77:31 77:35 77:31 77:35 77:35 77:34 80:34 77:32 72:22:43 - | 3 | 1,000 | 87 E10 | FTP-2 (Bags 1 & 2) | 12/5/2013 | 19.71 | 1266.4 | 18.11 | 27.60 | 23.12 | 477.1 | 582.2 | 659.1 | 732.4 |
| 3 1,000 87±10 U.62 1/2/5/013 82.29 141.62 18.80 28.31 23.30 25.24 64.29 71.2. 789.1 3 1,000 87±10 FFP-2 (logs) 1.42/5/013 19.75 126.7 18.00 27.17 23.26 69.88 770.7 840.0 92.30 3 1,000 87±10 FFP-2 (logs) 1.42/5/013 25.31 1415.6 18.89 28.38 22.33 644.9 77.2. 65.29 779.2 3 5.000 87±10 FFP-3 (logs) 1.42/7/013 21.37 12.36.1 12.36 655.3 784.9 849.5 912.9 3 5.000 87±10 L4.22 12/9/2/013 25.13 1425.6 19.39 27.72 22.41 576.1 641.3 72.7.6 883.4 3 1.000 85±10 FFF-1 (logs) 1.42/1/1/2/103 1.99.9 1337.3 17.99 30.44 65.31 45.1 74.6 644.3 70.7 76.4 73.00 74.5 88 | 3 | 1,000 | 87 E10 | FTP-2 (Bag 3) | 12/5/2013 | 25.63 | 1390.2 | 18.71 | 28.29 | 24.01 | 482.9 | 592.8 | 636.7 | 707.3 |
| 3 1,000 87:10 TP-2 (Bag 1.8.2) 12/52/013 3.7.5 128.20 48.85 128.25 127.2 128.26 47.66 58.16 661.2 730.5 3 1,000 87:10 FFP-2 (Bag 1.8.2) 12/5/2013 25.31 1128.20 128.29 28.29 42.20 488.5 687.5 778.9 989.5 979.7 3 1,000 87:10 FFP-3 (Bag 1.8.2) 12/5/2013 12.37 1266.3 18.89 28.81 22.33 644.9 725.9 789.3 984.5 912.9 3 5.000 87:10 FFP-3 (Bag 1.8.2) 12/9/2013 25.37 1386.7 19.69 77.2 22.44 52.61 641.3 77.6 883.4 3 5.000 87:10 FFP-1 (Bag 1.8.2) 11/9/2013 48.50 23.87 47.7 782.7 784.7 884.1 3 5.000 85:10 FFP-1 (Bag 1.8.2) 1/9/2014 24.69 124.7 565.5 660.3 22.9.4 880.0 | 3 | 1,000 | 87 E10 | LA92 | 12/5/2013 | 25.29 | 1416.2 | 18.89 | 28.33 | 23.30 | 528.4 | 642.9 | 718.2 | 789.1 |
| 3 1.000 87:10 171-2 (1883) 12/02 (1893) 12/02 (1 | 3 | 1,000 | 87 E10 | US06 (2nd) | 12/5/2013 | 48.85 | 2135.3 | 24.40 | 39.41 | 23.52 | 659.8 | 770.7 | 840.0 | 923.0 |
| 3 1,000 67 FL0 1/16/2013 25.01 185.00 11.0000 11.0000 11.0000 11.0000< | 3 | 1,000 | 87 E10 | FTP-2 (Bags 1 & 2) | 12/6/2013 | 19.75 | 1267.2 | 18.09 | 27.17 | 23.26 | 4/6.6 | 581.6 | 661.2 | 730.5 |
| 3 1,000 87 E10 US06[2nd] 12/6/2013 42/7 2137 300 67 E10 US06[2nd] 12/6/2013 42/7 2137 300 67 E10 FTP-3 [Bag 3] 12/6/2013 42/7 13663 18/7 26.64 21.76 472.4 577.2 652.9 723.1 3 5,000 87 E10 LV32 12/9/2013 25.13 1425.6 19.93 27.72 22.44 577.2 653.5 752.1 794.7 884.1 3 5,000 85 E10 FTP-1 (Bag 18.2) 11/1/0/2014 19.99 1337.3 17.99 30.44 26.03 1.491.8 522.0 617.5 745.3 800.9 4 5,000 85 E10 FTP-1 (Bag 31.8.2) 1/14/2014 25.99 1343.5 1.197 26.55 660.3 22.94 806.9 4 5,000 85 E10 FTP-2 (Bag 31.8.2) 1/15/2014 25.42 151.6 20.43 38.84 1.197 26.55 760.73 882.9 99.9 < | 3 | 1,000 | 87 E10 | FTP-2 (Bag 5) | 12/6/2013 | 25.01 | 1392.0 | 18.09 | 28.29 | 24.22 | 482.0 529.3 | 644.9 | 725.9 | 709.0 |
| $ \begin{array}{c c c c c c c c c c c c c c c c c c c $ | 3 | 1.000 | 87 E10 | US06 (2nd) | 12/6/2013 | 48.74 | 2137.6 | 24.17 | 38.84 | 23.61 | 655.3 | 768.9 | 849.5 | 912.9 |
| $ \begin{array}{c c c c c c c c c c c c c c c c c c c $ | 3 | 5,000 | 87 E10 | FTP-3 (Bags 1 & 2) | 12/9/2013 | 19.67 | 1266.3 | 18.79 | 26.64 | 21.76 | 472.4 | 577.2 | 652.9 | 729.1 |
| 3 5,000 87t10 LA92 12/9/2013 25.13 1425.6 19.93 27.72 22.41 52.61. 64.13 72.76. 88.41 3 1,000 85t10 FTP-1 [Bags 1 & 2] 11/10/2103 19.79 1280.3 18.02 26.85 23.71 475.7 578.7 654.4 730.0 4 5,000 85t10 FTP-1 [Bags 1 & 2] 1/14/2014 25.99 152.5 20.59 13.42 27.03 552.0 667.5 565.5 660.3 28.94 886.0 4 5,000 85t10 FTP-2 [Bags 1 & 2] 1/14/2014 25.42 1565.5 26.59 13.87 24.77 556.5 660.3 28.94 886.0 4 5,000 85t10 FTP-2 [Bag 3] 1/15/2014 26.82 11.92 24.71 556.5 660.3 28.94 880.0 4 5,000 85t10 FTP-2 [Bag 3] 1/15/2014 26.82 15.10 14.02 776.7 778.4 38.0 28.93< | 3 | 5,000 | 87 E10 | FTP-3 (Bag 3) | 12/9/2013 | 25.37 | 1386.7 | 19.60 | 27.52 | 22.43 | | | | |
| 3 5,000 87 E10 US06 [2nd] 129/2013 48.90 2185.3 26.08 24.45 635.5 752.1 794.7 884.1 3 1,000 85 E10 FTP-1(Bags 18.2) 1/14/2014 19.99 1337.3 17.99 30.44 26.83 491.8 592.0 672.3 772.7 4 5,000 85 E10 FTP-1(Bag 18.2) 1/14/2014 26.99 1525.5 20.59 31.49 27.03 552.0 617.5 745.3 800.9 4 5,000 85 E10 FTP-1(Bag 18.2) 1/14/2014 25.42 1566.5 22.63 31.41 27.03 522.0 617.5 745.3 800.9 4 5,000 85 E10 FTP-2(Bag 18.2) 1/15/2014 25.42 151.8 30.02 26.56 490.7 585.6 689.4 742.8 4 5,000 85 E10 FTP-2(Bag 18.2) 1/15/2014 49.77 24.06 36.98 41.79 25.99 687.5 776.9 89.9.9 <td< td=""><td>3</td><td>5,000</td><td>87 E10</td><td>LA92</td><td>12/9/2013</td><td>25.13</td><td>1425.6</td><td>19.93</td><td>27.72</td><td>22.41</td><td>526.1</td><td>641.3</td><td>727.6</td><td>803.4</td></td<> | 3 | 5,000 | 87 E10 | LA92 | 12/9/2013 | 25.13 | 1425.6 | 19.93 | 27.72 | 22.41 | 526.1 | 641.3 | 727.6 | 803.4 |
| 3 1,000 8510 FTP-1 (Bags 18.2) 11/1/2/103 19.99 1337.3 17.99 30.44 26.31 4475.7 578.7 654.4 730.0 4 5,000 85100 FTP-1 (Bags 18.2) 1/14/2014 26.99 1525.5 20.59 31.49 27.03 522.0 617.5 745.3 800.9 4 5,000 85100 US6(2nd) 1/14/2014 25.42 1566.5 22.63 31.77 24.77 565.5 660.3 829.4 868.0 4 5,000 85101 US6(2nd) 1/14/2014 40.67 256.1 36.81 41.97 26.61 685.5 778.0 892.2 954.9 4 5,000 85101 US6(2nd) 1/15/2014 25.44 1558.7 22.29 31.50 24.83 561.1 654.2 818.0 853.6 4 5,000 85101 UFP-2 (Bag3 18.2) 1/15/2014 25.44 1558.7 26.59 687.5 777.6 980.9 942.3 | 3 | 5,000 | 87 E10 | US06 (2nd) | 12/9/2013 | 48.90 | 2185.3 | 26.08 | 34.65 | 24.96 | 635.5 | 752.1 | 794.7 | 884.1 |
| 4 5,000 8510 FIP-1[1683] 1/14/2014 19.99 135.73 17.99 30.44 26.11 491.8 592.0 612.3 72.7 4 5,000 8510 LA92 1/14/2014 25.42 1556.5 22.63 31.77 24.77 555.5 660.3 829.4 868.0 4 5,000 8510 LFP-12(883) 1/15/2014 25.42 1556.5 26.61 685.5 778.0 892.2 954.9 4 5,000 8510 FFP-2(883) 1/15/2014 25.42 151.8 20.00 134.0.5 17.80 30.02 26.55 490.7 585.6 689.4 742.8 4 5,000 8510 FFP-2(883) 1/15/2014 25.44 158.87 22.29 31.50 24.83 551.1 654.2 818.0 683.5 4 1,000 8510 FFP-3(8831 & 2) 1/16/2014 42.67 14.0.9 26.59 687.5 776.9 890.9 942.3 4 1,000 8510 FFP-1(883) 1/16/2014 42.75 156.4 < | 3 | 1,000 | 85 E10 | FTP-1 (Bags 1 & 2) | 11/10/2103 | 19.79 | 1280.3 | 18.02 | 26.85 | 23.71 | 475.7 | 578.7 | 654.4 | 730.0 |
| 4 5,000 85E10 FIF-1(Beg 3) 1/14/2014 25.92 152.3 20.33 31.77 24.73 55.5 660.3 829.4 866.0 4 5,000 85E10 US06(2nd) 1/14/2014 49.57 256.1 36.81 41.97 26.61 685.5 F78.0 892.2 954.9 4 5,000 85E10 FTP-2(Bags 18.2) 1/15/2014 26.82 1511.8 20.40 31.22 26.59 581.9 613.2 720.0 779.6 4 5,000 85E10 FTP-2(Bags 18.2) 1/15/2014 25.44 158.7 72.29 51.5 776.9 890.9 942.3 4 1,000 85E10 FTP-1(Bag 3) 1/16/2014 25.74 150.46 18.63 31.91 26.54 40.7 56.4 656.0 852.3 881.9 4 1,000 85E10 LV32 1/16/2014 25.74 156.4 156.4 656.0 852.3 881.9 4 1,000 | 4 | 5,000 | 85 E10 | FTP-1 (Bags 1 & 2) | 1/14/2014 | 19.99 | 1337.3 | 17.99 | 30.44 | 26.31 | 491.8 | 592.0 | 6/2.3 | /32.7 |
| J. Job J. Job J. J | 4 | 5,000 | 85 E10 | FTP-1 (Bag 3) | 1/14/2014 | 26.99 | 1525.5 | 20.59 | 31.49 | 27.03 | 522.0 | 660.3 | 745.3 879.4 | 800.9 |
| 4 5,000 85 E10 FTP-2 (Bag3) 1/15/2014 20.00 1340.5 17.80 30.02 26.56 490.7 585.6 689.4 742.8 4 5,000 85 E10 FTP-2 (Bag3) 1/15/2014 26.82 1511.8 20.40 31.22 26.99 518.9 613.2 770.0 779.6 4 5,000 85 E10 US6 (2nd) 1/15/2014 49.77 2540.6 36.98 41.79 26.59 687.5 776.9 890.9 942.3 4 1,000 85 E10 FTP-1 (Bag 3) 1/16/2014 25.74 1504.6 18.63 31.91 26.54 450.3 610.7 706.9 751.4 4 1,000 85 E10 FTP-1 (Bag 3) 1/16/2014 25.04 18.63 31.91 26.54 4.04 25.95 688.3 777.7 907.7 949.6 4 1,000 85 E10 FTP-2 (Bag3) 1/17/2014 26.91 18.31 31.88 27.04 520.6 610.3 | 4 | 5,000 | 85 E10 | US06 (2nd) | 1/14/2014 | 49.67 | 2561.3 | 36.81 | 41.97 | 26.61 | 685.5 | 778.0 | 892.2 | 954.9 |
| 4 5,000 85 E10 FTP-2 (Bag]3 1/15/2014 26.82 1511.8 20.40 31.22 26.99 518.9 613.2 720.0 779.6 4 5,000 85 E10 LM92 1/15/2014 25.44 1558.7 22.99 31.50 24.83 561.1 654.2 818.0 853.6 4 1,000 85 E10 FTP-3 (Bags 1 & 2) 1/16/2014 49.77 2540.6 36.98 41.79 26.59 687.5 776.9 890.9 942.3 4 1,000 85 E10 FTP-1 (Bag 3) 1/16/2014 26.75 1504.6 186.3 31.91 26.94 520.3 610.7 706.9 751.4 4 1,000 85 E10 US6(2nd) 1/16/2014 50.19 2447.3 32.66 44.04 25.95 688.3 777.7 907.7 949.6 4 1,000 85 E10 US6(2nd) 1/17/2014 25.47 1546.2 18.81 31.81 27.44 520.6 610.3 < | 4 | 5,000 | 85 E10 | FTP-2 (Bags 1 & 2) | 1/15/2014 | 20.00 | 1340.5 | 17.80 | 30.02 | 26.56 | 490.7 | 585.6 | 689.4 | 742.8 |
| 4 5,000 85 E10 LA92 1/15/2014 25.44 1558.7 22.29 31.50 24.83 561.1 654.2 818.0 853.6 4 1,000 85 E10 FTP-3(Bags 1 & 2) 1/16/2014 19.97 258.06 36.98 41.79 26.59 687.5 776.9 890.9 942.3 4 1,000 85 E10 FTP-3(Bags 1 & 2) 1/16/2014 26.75 1504.6 18.63 31.91 26.94 520.3 610.7 706.9 751.4 4 1,000 85 E10 LVS02 (Lndt 52.44 1541.8 19.92 32.65 24.71 565.4 656.0 852.3 881.9 4 1,000 85 E10 LVS02 (Lndt 52.14 1541.8 19.92 32.65 24.71 565.4 656.0 852.3 881.9 4 1,000 85 E10 LVS02 (Lndt 1/17/2014 20.01 1337.0 16.37 30.17 26.41 493.7 584.5 678.4 736.7 | 4 | 5,000 | 85 E10 | FTP-2 (Bag3) | 1/15/2014 | 26.82 | 1511.8 | 20.40 | 31.22 | 26.99 | 518.9 | 613.2 | 720.0 | 779.6 |
| 4 5,000 85 E10 US06 (2nd) 1/15/2014 49.77 2540.6 36.88 41.79 26.59 687.5 776.9 890.9 942.3 4 1,000 85 E10 FTP-3 (Bags 1 & 2) 1/16/2014 26.75 1504.6 30.49 26.39 492.9 584.4 668.1 725.6 4 1,000 85 E10 LA92 1/16/2014 25.47 1504.6 18.63 31.91 26.59 688.3 777.7 907.7 949.6 4 1,000 85 E10 FTP-4 (Bags 1 & 2) 1/17/2014 20.01 1337.0 16.37 30.17 26.41 493.7 584.5 678.4 736.7 4 1,000 85 E10 FTP-2 (Bag3) 1/17/2014 20.01 1337.0 16.37 138.8 27.04 520.6 610.3 739.3 787.8 4 1,000 85 E10 FTP-2 (Bag3) 1/17/2014 20.01 1330.7 14.15 26.16 684.6 7774.2 903.8 936.7 <td>4</td> <td>5,000</td> <td>85 E10</td> <td>LA92</td> <td>1/15/2014</td> <td>25.44</td> <td>1558.7</td> <td>22.29</td> <td>31.50</td> <td>24.83</td> <td>561.1</td> <td>654.2</td> <td>818.0</td> <td>853.6</td> | 4 | 5,000 | 85 E10 | LA92 | 1/15/2014 | 25.44 | 1558.7 | 22.29 | 31.50 | 24.83 | 561.1 | 654.2 | 818.0 | 853.6 |
| 4 1,000 85 E10 FTP-3 (Bags 1, 8, 2) 1/16/2014 19.94 1333.5 16.63 30.49 26.39 492.9 584.4 668.1 725.6 4 1,000 85 E10 FTP-1 (Bag 3) 1/16/2014 26.74 1564.8 31.91 26.59 520.3 610.7 706.9 751.4 4 1,000 85 E10 US06 (2nd) 1/16/2014 50.19 2447.3 32.66 44.04 25.95 688.3 777.7 907.7 999.6 4 1,000 85 E10 US06 (2nd) 1/17/2014 20.01 1337.0 16.37 30.17 26.41 493.7 584.5 678.4 736.7 4 1,000 85 E10 UA92 1/17/2014 25.47 1546.2 18.86 32.10 25.21 562.9 651.1 809.0 855.0 4 1,000 85 E10 US06 (2nd) 1/17/2014 25.47 1546.2 18.86 32.10 25.21 562.9 651.1 809.0 855.0 4 1,000 85 E10 US06 (2nd) 1/12/2014 <t< td=""><td>4</td><td>5,000</td><td>85 E10</td><td>US06 (2nd)</td><td>1/15/2014</td><td>49.77</td><td>2540.6</td><td>36.98</td><td>41.79</td><td>26.59</td><td>687.5</td><td>776.9</td><td>890.9</td><td>942.3</td></t<> | 4 | 5,000 | 85 E10 | US06 (2nd) | 1/15/2014 | 49.77 | 2540.6 | 36.98 | 41.79 | 26.59 | 687.5 | 776.9 | 890.9 | 942.3 |
| 4 1,000 85 E 10 111-1 (Hag 3) 1/16/2014 26.75 150.4.6 18.63 1.91 26.94 520.3 651.0 706.9 751.4 4 1,000 85 E 10 USO6 (2nd) 1/16/2014 25.14 1541.8 19.92 32.65 24.71 565.4 656.0 852.3 881.9 4 1,000 85 E 10 USO6 (2nd) 1/16/2014 20.01 1337.0 16.37 30.17 26.41 493.7 584.5 678.4 736.7 4 1,000 85 E 10 UFP-2 (Bag3) 1/17/2014 25.91 18.31 31.88 27.04 520.6 610.3 739.3 787.8 4 1,000 85 E 10 USO (2nd) 1/17/2014 25.03 243.0 25.16 684.6 774.2 903.8 936.7 4 5,000 87 E 10 FTP-1 (Bag 3) 1/28/2014 25.55 1564.7 22.60 31.55 25.20 557.9 653.1 804.6 850.8 | 4 | 1,000 | 85 E10 | FTP-3 (Bags 1 & 2) | 1/16/2014 | 19.94 | 1333.5 | 16.63 | 30.49 | 26.39 | 492.9 | 584.4 | 668.1 | 725.6 |
| 4 1,000 851.0 US62 1/10/2014 52.14 1341.0 135.2 24.03 24.11 2050.4 6050.1 7050.4 < | 4 | 1,000 | 85 E10 | FIP-1 (Bag 3) | 1/16/2014 | 26.75 | 1504.6 | 18.63 | 31.91 | 26.94 | 520.3 | 610.7 | /06.9 | /51.4 |
| 4 1,000 85:10 FTP-4 (Bag3) 1/17/2014 20.01 1337.0 16.37 30.17 26.03 77.77 30.77 4 1,000 85:10 FTP-4 (Bag3) 1/17/2014 20.01 1337.0 16.37 30.17 26.41 493.7 584.5 678.4 736.7 4 1,000 85:10 LA92 1/17/2014 25.47 1546.2 18.86 32.10 25.21 562.9 651.1 809.0 855.0 4 1,000 85:10 LS06 (2nd) 1/17/2014 25.47 1546.2 18.86 32.10 25.21 562.9 651.1 809.0 855.0 4 5,000 87:10 FTP-1 (Bag3) 1/28/2014 26.84 1523.7 20.60 30.66 27.32 517.5 613.5 740.7 777.1 4 5,000 87:10 FTP-2 (Bag3) 1/28/2014 25.55 1564.7 22.61 31.55 25.20 557.9 653.1 804.6 850.8 4 5,000 87:10 FTP-2 (Bag3) 1/29/2014 25.42 38.04 <td>4</td> <td>1,000</td> <td>85 F10</td> <td>US06 (2nd)</td> <td>1/16/2014</td> <td>23.44 50.19</td> <td>2447 3</td> <td>32.66</td> <td>44 04</td> <td>24.71</td> <td>688 3</td> <td>777.7</td> <td>907.7</td> <td>949 6</td> | 4 | 1,000 | 85 F10 | US06 (2nd) | 1/16/2014 | 23.44 50.19 | 2447 3 | 32.66 | 44 04 | 24.71 | 688 3 | 777.7 | 907.7 | 949 6 |
| 4 1,000 85 E10 FIP-2 (Bag3) 1/17/2014 26.91 1499.6 18.31 31.88 27.04 520.6 610.3 739.3 787.8 4 1,000 85 E10 LA92 1/17/2014 25.47 1546.2 18.86 32.10 25.21 562.9 651.1 809.0 855.0 4 1,000 85 E10 LSO6 (2nd) 1/17/2014 50.03 2430.6 31.70 44.15 26.16 684.6 774.2 903.8 936.7 4 5,000 87 E10 FTP-1 (Bag3 18.2) 1/28/2014 26.84 1523.7 20.60 30.66 27.32 517.5 613.5 740.7 778.0 4 5,000 87 E10 FTP-1 (Bag3 14.2) 1/28/2014 25.55 1564.7 22.61 31.55 25.20 557.9 653.1 804.6 850.8 4 5,000 87 E10 FTP-2 (Bag3 18.2) 1/29/2014 26.86 1518.8 20.44 31.08 27.33 517.7 612.2< | 4 | 1,000 | 85 E10 | FTP-4 (Bags 1 & 2) | 1/17/2014 | 20.01 | 1337.0 | 16.37 | 30.17 | 26.41 | 493.7 | 584.5 | 678.4 | 736.7 |
| 4 1,000 85 E10 LA92 1/17/2014 25.47 1546.2 18.86 32.10 25.21 562.9 651.1 809.0 855.0 4 1,000 85 E10 US06 (2nd) 1/17/2014 50.03 2430.6 31.70 44.15 26.16 684.6 774.2 903.8 936.7 4 5,000 87 E10 FTP-1 (Bags 18.2) 1/28/2014 29.64 152.7 20.60 30.66 27.32 517.5 613.5 740.7 778.0 4 5,000 87 E10 LA92 1/28/2014 25.55 1564.7 22.61 31.55 25.20 557.9 653.1 804.6 850.8 4 5,000 87 E10 US06 (2nd) 1/28/2014 50.18 2542.7 38.04 42.11 26.64 690.1 782.5 889.0 949.4 4 5,000 87 E10 US06 (2nd) 1/29/2014 59.88 20.44 31.08 27.33 517.7 612.2 753.5 793.5 </td <td>4</td> <td>1,000</td> <td>85 E10</td> <td>FTP-2 (Bag3)</td> <td>1/17/2014</td> <td>26.91</td> <td>1499.6</td> <td>18.31</td> <td>31.88</td> <td>27.04</td> <td>520.6</td> <td>610.3</td> <td>739.3</td> <td>787.8</td> | 4 | 1,000 | 85 E10 | FTP-2 (Bag3) | 1/17/2014 | 26.91 | 1499.6 | 18.31 | 31.88 | 27.04 | 520.6 | 610.3 | 739.3 | 787.8 |
| 4 1,000 85 E10 US06 (2nd) 1/17/2014 50.03 2430.6 31.70 44.15 26.16 684.6 774.2 903.8 936.7 4 5,000 87 E10 FTP-1 (Bags 1 & 2) 1/28/2014 19.96 1349.7 17.65 28.82 26.03 486.9 583.0 677.7 747.1 4 5,000 87 E10 FTP-1 (Bag 3) 1/28/2014 26.84 1523.7 20.60 30.66 27.32 517.5 613.5 740.7 778.0 4 5,000 87 E10 LA92 1/28/2014 25.55 1564.7 22.61 31.55 25.20 557.9 653.1 804.6 850.8 4 5,000 87 E10 US06 (2nd) 1/28/2014 25.42 38.04 42.11 26.64 690.1 782.5 889.0 949.4 4 5,000 87 E10 FTP-2 (Bags 1 & 2) 1/29/2014 25.49 156.7 22.08 31.46 25.25 558.0 650.7 832.9 | 4 | 1,000 | 85 E10 | LA92 | 1/17/2014 | 25.47 | 1546.2 | 18.86 | 32.10 | 25.21 | 562.9 | 651.1 | 809.0 | 855.0 |
| 4 5,000 87 E10 FTP-1 (Bags 1 & 2) 1/28/2014 19.96 1349.7 17.65 28.82 26.03 486.9 583.0 677.7 747.1 4 5,000 87 E10 FTP-1 (Bag 3) 1/28/2014 26.84 1523.7 20.60 30.66 27.32 517.5 613.5 740.7 778.0 4 5,000 87 E10 LA92 1/28/2014 25.55 1564.7 22.61 31.55 25.20 557.9 653.1 804.6 850.8 4 5,000 87 E10 US06 (2nd) 1/28/2014 50.18 2542.7 38.04 42.11 26.64 690.1 782.5 889.0 949.4 4 5,000 87 E10 FTP-2 (Bag3) 1/29/2014 25.49 1562.7 22.08 31.46 25.25 558.0 650.7 832.9 857.7 4 5,000 87 E10 US06 (2nd) 1/29/2014 25.49 1562.7 22.08 31.46 25.25 558.0 650.7 | 4 | 1,000 | 85 E10 | US06 (2nd) | 1/17/2014 | 50.03 | 2430.6 | 31.70 | 44.15 | 26.16 | 684.6 | 774.2 | 903.8 | 936.7 |
| 4 5,000 87 E10 FTP-1 (Bag 3) 1/28/2014 26.84 1523.7 20.60 30.66 27.32 517.5 613.5 740.7 778.0 4 5,000 87 E10 LA92 1/28/2014 25.55 1564.7 22.61 31.55 25.20 557.9 653.1 804.6 850.8 4 5,000 87 E10 US06 (2nd) 1/28/2014 50.18 2542.7 38.04 42.11 26.64 690.1 782.5 889.0 949.4 4 5,000 87 E10 FTP-2 (Bags 1 & 2) 1/29/2014 19.98 1337.9 18.01 30.50 26.50 489.9 586.2 680.8 741.3 4 5,000 87 E10 FTP-2 (Bags) 1/29/2014 26.86 1518.8 20.44 31.08 27.33 517.7 612.2 753.5 793.5 4 5,000 87 E10 LA92 1/29/2014 25.49 1562.7 22.08 31.46 25.25 558.0 650.7 832.9 857.7 4 5,000 87 E10 US06 (2nd) 1/29/201 | 4 | 5,000 | 87 E10 | FTP-1 (Bags 1 & 2) | 1/28/2014 | 19.96 | 1349.7 | 17.65 | 28.82 | 26.03 | 486.9 | 583.0 | 677.7 | 747.1 |
| 4 5,000 67 E10 LA92 1/28/2014 25.55 1564.7 22.61 31.55 25.20 557.9 653.1 804.6 850.8 4 5,000 87 E10 US06 (2nd) 1/28/2014 50.18 2542.7 38.04 42.11 26.64 690.1 782.5 889.0 949.4 4 5,000 87 E10 FTP-2 (Bag3 1 & 2) 1/29/2014 19.98 1337.9 18.01 30.50 26.50 489.9 586.2 680.8 741.3 4 5,000 87 E10 FTP-2 (Bag3) 1/29/2014 26.86 1518.8 20.44 31.08 27.33 517.7 612.2 753.5 793.5 4 5,000 87 E10 US06 (2nd) 1/29/2014 25.49 1562.7 22.08 31.46 25.25 558.0 650.7 832.9 857.7 4 5,000 87 E10 US06 (2nd) 1/29/2014 20.05 1337.7 16.54 31.34 26.57 494.8 585.9 | 4 | 5,000 | 87 E10 | FTP-1 (Bag 3) | 1/28/2014 | 26.84 | 1523.7 | 20.60 | 30.66 | 27.32 | 517.5 | 613.5 | 740.7 | 778.0 |
| + - | 4 | 5,000 | 87 E10 | | 1/28/2014 | 25.55 50.19 | 1564.7 | 22.61 | 31.55 | 25.20 | 557.9 | 653.1 792 F | 804.6 | 850.8 |
| 4 5,000 87 E10 FTP-2 (Bag3) 1/29/2014 26.86 1518.8 20.44 31.08 27.33 517.7 612.2 753.5 793.5 4 5,000 87 E10 LA92 1/29/2014 25.49 1562.7 22.08 31.46 25.25 558.0 650.7 832.9 857.7 4 5,000 87 E10 US06 (2nd) 1/29/2014 25.49 1562.7 22.08 31.46 25.25 558.0 650.7 832.9 857.7 4 5,000 87 E10 US06 (2nd) 1/29/2014 49.98 2543.8 37.45 41.60 27.14 686.2 77.7 875.2 936.2 4 1,000 87 E10 FTP-1 (Bags 1 & 2) 1/30/2014 20.05 1337.7 16.54 31.34 26.57 494.8 585.9 676.9 725.9 4 1,000 87 E10 FTP-1 (Bags 1 & 2) 1/30/2014 20.05 1337.7 16.54 31.34 26.57 494.8 585.9 | 4 4 | 5,000 | 87 F10 | 0300 (200) FTP-2 (Rags 1 & 2) | 1/29/2014 | 20.18 10 08 | 2042.7 1337 Q | 38.04 18.01 | 42.11 | 20.04 26.50 | 780 0 090.1 | 782.5 586.7 | 0.500 680 8 | 949.4 741 २ |
| 4 5,000 87 E10 LA92 1/29/2014 25.49 1562.7 22.08 31.46 25.25 558.0 650.7 832.9 857.7 4 5,000 87 E10 US06 (2nd) 1/29/2014 49.98 254.38 37.45 41.60 27.14 686.2 775.7 875.2 936.2 4 1,000 87 E10 FTP-1 (Bags 1 & 2) 1/30/2014 20.05 1337.7 16.54 31.34 26.57 494.8 585.9 676.9 725.9 4 1,000 87 E10 FTP-1 (Bag 3) 1/30/2014 27.06 18.00 32.09 27.31 519.2 609.8 713.6 762.7 4 1,000 87 E10 LA92 1/30/2014 25.57 1551.4 19.05 32.49 24.82 560.8 649.5 817.5 874.0 4 1,000 87 E10 LA92 1/30/2014 25.00 243.40 30.86 43.94 27.04 679.4 768.5 895.6 937.9 <td>4</td> <td>5.000</td> <td>87 E10</td> <td>FTP-2 (Bag3)</td> <td>1/29/2014</td> <td>26.86</td> <td>1518.8</td> <td>20.44</td> <td>31.08</td> <td>27.33</td> <td>517.7</td> <td>612.2</td> <td>753.5</td> <td>793.5</td> | 4 | 5.000 | 87 E10 | FTP-2 (Bag3) | 1/29/2014 | 26.86 | 1518.8 | 20.44 | 31.08 | 27.33 | 517.7 | 612.2 | 753.5 | 793.5 |
| 4 5,000 87 E10 US06 (2nd) 1/29/2014 49.98 2543.8 37.45 41.60 27.14 686.2 775.7 875.2 936.2 4 1,000 87 E10 FTP-1 (Bags 1 & 2) 1/30/2014 20.05 1337.7 16.54 31.34 26.57 494.8 585.9 676.9 725.9 4 1,000 87 E10 FTP-1 (Bag 3) 1/30/2014 27.06 1500.6 18.00 32.09 27.31 519.2 609.8 713.6 762.7 4 1,000 87 E10 LA92 1/30/2014 25.57 1551.4 19.05 32.49 24.82 560.8 649.5 817.5 874.0 4 1,000 87 E10 US06 (2nd) 1/30/2014 50.00 2434.0 30.86 43.94 27.04 679.4 768.5 895.6 937.9 4 1,000 87 E10 FTP-2 (Bags 1 & 2) 1/31/2014 20.06 1334.4 16.63 31.59 26.50 489.4 580.5 | 4 | 5,000 | 87 E10 | LA92 | 1/29/2014 | 25.49 | 1562.7 | 22.08 | 31.46 | 25.25 | 558.0 | 650.7 | 832.9 | 857.7 |
| 4 1,000 87 E10 FTP-1 (Bags 1 & 2) 1/30/2014 20.05 1337.7 16.54 31.34 26.57 494.8 585.9 676.9 725.9 4 1,000 87 E10 FTP-1 (Bags 3) 1/30/2014 27.06 1500.6 18.00 32.09 27.31 519.2 609.8 713.6 762.7 4 1,000 87 E10 LA92 1/30/2014 25.57 155.4 19.05 32.49 24.82 560.8 649.5 817.5 874.0 4 1,000 87 E10 US06 (2nd) 1/30/2014 50.00 2434.0 30.86 43.94 27.04 679.4 768.5 895.6 937.9 4 1,000 87 E10 FTP-2 (Bags 1 & 2) 1/31/2014 20.06 1334.4 16.63 31.59 26.50 489.4 580.5 670.1 726.8 4 1,000 87 E10 FTP-2 (Bags 1 1/31/2014 26.91 1514.9 17.52 32.15 27.52 512.8 603.6 6 | 4 | 5,000 | 87 E10 | US06 (2nd) | 1/29/2014 | 49.98 | 2543.8 | 37.45 | 41.60 | 27.14 | 686.2 | 775.7 | 875.2 | 936.2 |
| 4 1,000 87 E10 FTP-1 (Bag 3) 1/30/2014 27.06 1500.6 18.00 32.09 27.31 519.2 609.8 713.6 762.7 4 1,000 87 E10 LA92 1/30/2014 25.57 1551.4 19.05 32.49 24.82 560.8 649.5 817.5 874.0 4 1,000 87 E10 US06 (2nd) 1/30/2014 50.00 2434.0 30.86 43.94 27.04 679.4 768.5 895.6 937.9 4 1,000 87 E10 FTP-2 (Bags 1 & 2) 1/31/2014 20.06 1334.4 16.63 31.59 26.50 489.4 580.5 670.1 726.8 4 1,000 87 E10 FTP-2 (Bag 3) 1/31/2014 26.91 1514.9 17.52 32.15 27.52 512.8 603.6 690.0 739.2 4 1,000 87 E10 LA92 1/31/2014 25.56 1544.7 19.06 32.43 25.09 559.2 648.5 <t< td=""><td>4</td><td>1,000</td><td>87 E10</td><td>FTP-1 (Bags 1 & 2)</td><td>1/30/2014</td><td>20.05</td><td>1337.7</td><td>16.54</td><td>31.34</td><td>26.57</td><td>494.8</td><td>585.9</td><td>676.9</td><td>725.9</td></t<> | 4 | 1,000 | 87 E10 | FTP-1 (Bags 1 & 2) | 1/30/2014 | 20.05 | 1337.7 | 16.54 | 31.34 | 26.57 | 494.8 | 585.9 | 676.9 | 725.9 |
| 4 1,000 87 E10 LA92 1/30/2014 25.57 1551.4 19.05 32.49 24.82 560.8 649.5 817.5 874.0 4 1,000 87 E10 US06 (2nd) 1/30/2014 50.00 2434.0 30.86 43.94 27.04 679.4 768.5 895.6 937.9 4 1,000 87 E10 FTP-2 (Bags 1 & 2) 1/31/2014 20.06 1334.4 16.63 31.59 26.50 489.4 580.5 670.1 726.8 4 1,000 87 E10 FTP-2 (Bags 3) 1/31/2014 26.91 1514.9 17.52 32.15 27.52 512.8 603.6 690.0 739.2 4 1,000 87 E10 LA92 1/31/2014 25.56 1544.7 19.06 32.43 25.09 559.2 648.5 849.9 881.4 4 1,000 87 E10 US06 (2nd) 1/31/2014 49.99 2419.4 31.40 43.77 27.05 678.5 766.7 | 4 | 1,000 | 87 E10 | FTP-1 (Bag 3) | 1/30/2014 | 27.06 | 1500.6 | 18.00 | 32.09 | 27.31 | 519.2 | 609.8 | 713.6 | 762.7 |
| 4 1,000 87 E10 US06 (2nd) 1/30/2014 50.00 2434.0 30.86 43.94 27.04 679.4 768.5 895.6 937.9 4 1,000 87 E10 FTP-2 (Bags 1 & 2) 1/31/2014 20.06 1334.4 16.63 31.59 26.50 489.4 580.5 670.1 726.8 4 1,000 87 E10 FTP-2 (Bag3) 1/31/2014 26.91 1514.9 17.52 32.15 27.52 512.8 603.6 690.0 739.2 4 1,000 87 E10 LA92 1/31/2014 25.56 1544.7 19.06 32.43 25.09 559.2 648.5 849.9 881.4 4 1,000 87 E10 US06 (2nd) 1/31/2014 49.99 2419.4 31.40 43.77 27.05 678.5 766.7 885.8 929.7 | 4 | 1,000 | 87 E10 | LA92 | 1/30/2014 | 25.57 | 1551.4 | 19.05 | 32.49 | 24.82 | 560.8 | 649.5 | 817.5 | 874.0 |
| 4 1,000 87 E10 FTP-2 (BagS 1 & 2) 1/31/2014 20.0b 1334.4 16.63 31.59 26.50 489.4 580.5 670.1 726.8 4 1,000 87 E10 FTP-2 (Bag3) 1/31/2014 26.91 1514.9 17.52 32.15 27.52 512.8 603.6 690.0 739.2 4 1,000 87 E10 LA92 1/31/2014 25.56 1544.7 19.06 32.43 25.09 559.2 648.5 849.9 881.4 4 1,000 87 E10 US06 (2nd) 1/31/2014 49.99 2419.4 31.40 43.77 27.05 678.5 766.7 885.8 929.7 | 4 | 1,000 | 87 E10 | US06 (2nd) | 1/30/2014 | 50.00 | 2434.0 | 30.86 | 43.94 | 27.04 | 679.4 | 768.5 | 895.6 | 937.9 |
| 4 1,000 67 E10 F17-2 (56gs) 1/31/2014 20.51 17.32 32.15 27.32 512.6 003.0 690.0 739.2 4 1,000 87 E10 LA92 1/31/2014 25.56 1544.7 19.06 32.43 25.09 559.2 648.5 849.9 881.4 4 1,000 87 E10 US06 (2nd) 1/31/2014 49.99 2419.4 31.40 43.77 27.05 678.5 766.7 885.8 929.7 | 4 | 1,000 | 87 E10 | FTP-2 (Bags 1 & 2) | 1/31/2014 | 20.06 | 1514.0 | 10.03 | 31.59 22 1E | 26.50 | 489.4 | 580.5 | 600.0 | 720.8 |
| 4 1,000 87 E10 US06 (2nd) 1/31/2014 49.99 2419.4 31.40 43.77 27.05 678.5 766.7 885.8 929.7 | 4 | 1.000 | 87 F10 | LA92 | 1/31/2014 | 25.51 | 1544.9 | 19.06 | 32.13 | 25.09 | 559.2 | 648 5 | 849.9 | 881.4 |
| | 4 | 1,000 | 87 E10 | US06 (2nd) | 1/31/2014 | 49.99 | 2419.4 | 31.40 | 43.77 | 27.05 | 678.5 | 766.7 | 885.8 | 929.7 |

| Vnumber | Altitudo | Fuel | Test Cycle | Date | Vehicle | Engine | Throttle | heal | Ignition | Exhaust Temp - | Catalyst Temp - | Exhaust Temp - | Catalyst Temp - |
|-------------|----------|--------------------|-----------------------------------|-------------|----------------------|------------------|--------------|----------------|----------------|----------------|-----------------|----------------|-----------------|
| vitatiliber | Annua | ruei | rest cycle | Date | Speed | Speed | Position | LUau | Timing | PreCat Avg. | MidCat Avg. | PreCat Max. | MidCat Max. |
| | F 000 | 0F F10 | FTD 1 (Dags 1 9 2) | 11/6/2012 | (mph) | (rpm) | (%) 16.72 | (%) | (deg BTDC) | (deg. C) | (deg. C) | (deg. C) | (deg. C) |
| 5 | 5,000 | 85 E 10 85 E 10 | FTP-1 (Bags 1 & 2) | 11/6/2013 | 27.9/ | 1209.2 | 18.73 | 26.50 | 23.41 | | | | |
| 5 | 5,000 | 85 E10 | LA92 | 11/6/2013 | 25.21 | 1194.7 | 18.70 | 31.56 | 19.16 | | | | |
| 5 | 5,000 | 85 E10 | US06 (2nd) | 11/6/2013 | 49.42 | 1712.6 | 23.79 | 47.34 | 18.18 | | | | |
| 5 | 1,000 | 85 E10 | FTP-4 (Bags 1 & 2) | 11/21/2013 | 19.82 | 1158.0 | 15.80 | 27.41 | 22.47 | 397.3 | 517.5 | 513.4 | 624.1 |
| 5 | 1,000 | 85 E10 | FTP-2 (Bag3) | 11/21/2013 | 26.76 | 1200.9 | 16.58 | 30.12 | 20.97 | 393.1 | 513.8 | 545.5 | 630.9 |
| 5 | 1,000 | 85 E10 | LA92 | 11/21/2013 | 25.28 | 1192.2 | 17.13 | 31.94 | 18.97 | 469.2 | 597.7 | 652.2 | 736.1 |
| 5 | 1,000 | 85 E10 | US06 (2nd) | 11/21/2013 | 49.50 | 1/08.3 | 21.67 | 48.37 | 17.91 | 588.4 | /19.3 | /66.6 | 8/5.4 |
| 5 | 1,000 | 85 E10 | FTP-2 (Bag3) | 1/9/2014 | 26.91 | 1196.1 | 16.69 | 30.45 | 20.53 | 398.8 | 524.1 | 543.3 | 627.6 |
| 5 | 5,000 | 85 E10 | LA92 | 1/9/2014 | 25.25 | 1203.7 | 18.63 | 31.60 | 19.50 | 469.7 | 601.0 | 640.8 | 783.7 |
| 5 | 1,000 | 85 E10 | LA92 | 1/9/2014 | 25.08 | 1191.2 | 17.15 | 32.42 | 19.28 | 471.1 | 600.3 | 659.2 | 759.5 |
| 5 | 5,000 | 85 E10 | US06 (2nd) | 1/9/2014 | 49.42 | 1708.8 | 24.44 | 48.18 | 17.89 | 592.4 | 727.6 | 753.6 | 888.8 |
| 5 | 1,000 | 85 E10 | US06 (2nd) | 1/9/2014 | 49.32 | 1702.3 | 22.21 | 49.08 | 18.44 | 585.6 | 716.3 | 767.7 | 905.1 |
| 5 | 5,000 | 85 E10 | FTP-2 (Bags 1 & 2) | 1/10/2014 | 19.90 | 1175.1 | 16.90 | 26.81 | 23.17 | 394.8 | 515.6 | 514.3 | 608.6 |
| 5 | 5,000 | 87 F10 | FTP-2 (Bdg3) | 1/10/2014 | 20.82 | 1204.5 | 16.19 | 29.70 | 20.84 | 390.2 | 515.8 | 50.4 | 598.2 |
| 5 | 5,000 | 87 E10 | FTP-1 (Bag 3) | 1/22/2014 | 26.79 | 1203.7 | 17.91 | 29.54 | 23.33 | 390.8 | 518.3 | 530.2 | 641.3 |
| 5 | 5,000 | 87 E10 | LA92 | 1/22/2014 | 25.34 | 1200.0 | 18.53 | 31.19 | 19.62 | 458.9 | 594.8 | 620.3 | 757.5 |
| 5 | 5,000 | 87 E10 | US06 (2nd) | 1/22/2014 | 49.56 | 1709.6 | 23.68 | 47.32 | 19.46 | 569.5 | 711.2 | 722.2 | 856.2 |
| 5 | 5,000 | 87 E10 | FTP-2 (Bags 1 & 2) | 1/23/2014 | 19.87 | 1172.6 | 16.89 | 26.50 | 23.37 | | | | |
| 5 | 5,000 | 87 E10 | FTP-2 (Bag3) | 1/23/2014 | 26.77 | 1207.1 | 18.36 | 29.66 | 21.67 | 391.0 | 527.2 | 548.8 | 687.6 |
| 5 | 5,000 | 87 E10 | LA92 | 1/23/2014 | 25.25 | 1204.1 | 18.91 | 31.16 | 19.31 | 464.2 | 706 5 | 635.6 722.7 | 766.0 |
| 5 | 1.000 | 87 E10 | FTP-1 (Bags 1 & 2) | 1/23/2014 | 19.52 | 1166.6 | 16.11 | 29.02 | 22.15 | 399.4 | 518.0 | 522.7 | 668.0 |
| 5 | 1,000 | 87 E10 | FTP-1 (Bag 3) | 1/27/2014 | 26.90 | 1200.6 | 16.65 | 30.39 | 21.95 | 392.6 | 515.8 | 528.3 | 616.8 |
| 5 | 1,000 | 87 E10 | LA92 | 1/27/2014 | 25.33 | 1201.8 | 16.86 | 31.65 | 20.13 | 462.2 | 590.4 | 643.2 | 737.1 |
| 5 | 1,000 | 87 E10 | US06 (2nd) | 1/27/2014 | 49.43 | 1715.4 | 21.32 | 47.42 | 19.28 | 575.7 | 703.9 | 724.0 | 831.8 |
| 5 | 1,000 | 87 E10 | FTP-2 (Bags 1 & 2) | 2/10/2014 | 19.86 | 1160.7 | 16.00 | 28.43 | 22.90 | 397.4 | 515.4 | 519.2 | 646.6 |
| 5 | 1,000 | 87 E10 | FTP-2 (Bag3) | 2/10/2014 | 26.70 | 1199.6 | 16.57 | 30.09 | 22.03 | 383.3 | 495.4 | 513.6 | 592.4 |
| 5 | 1,000 | 87 E10 | LA92 LISO6 (2nd) | 2/10/2014 | 25.16 //g g5 | 1716.6 | 21 1/ | 30.85 | 21.02 19.59 | 447.3 | 569.2 698 5 | 623.9 | 704.2 |
| 6 | 5,000 | 85 E10 | LA92 | 1/7/2014 | 24.59 | 1677.0 | 27.07 | 38.40 | 13.93 | 465.0 | 598.5 | 625.3 | 706.3 |
| 6 | 5,000 | 85 E10 | FTP-2 (Bags 1 & 2) | 1/30/2014 | 19.60 | 1573.9 | 21.43 | 34.30 | 18.54 | 411.3 | 531.3 | 525.6 | 623.2 |
| 6 | 5,000 | 85 E10 | FTP-2 (Bag3) | 1/30/2014 | 25.43 | 1639.0 | 23.57 | 35.86 | 20.91 | 405.5 | 531.7 | 523.4 | 605.2 |
| 6 | 5,000 | 85 E10 | LA92 | 1/30/2014 | 24.49 | 1665.3 | 25.28 | 37.55 | 16.48 | 459.2 | 589.8 | 620.1 | 703.4 |
| 6 | 5,000 | 85 E10 | US06 (2nd) | 1/30/2014 | 48.02 | 2329.6 | 41.51 | 57.30 | 14.27 | 623.7 | 758.6 | 771.7 | 838.6 |
| 6 | 1,000 | 85 F10 | FTP-1 (Bag 3) | 2/4/2014 | 25.69 | 1570.5 | 21.98 | 37 32 | 21 22 | 412.6 | 527.0 | 531.0 | 607.8 |
| 6 | 1,000 | 85 E10 | LA92 | 2/4/2014 | 24.52 | 1676.1 | 23.68 | 39.13 | 17.32 | 461.0 | 589.5 | 628.9 | 709.3 |
| 6 | 1,000 | 85 E10 | US06 (2nd) | 2/4/2014 | 48.42 | 2293.3 | 36.89 | 59.99 | 14.58 | 632.1 | 768.2 | 790.0 | 844.0 |
| 6 | 1,000 | 85 E10 | FTP-2 (Bags 1 & 2) | 2/5/2014 | 19.64 | 1569.9 | 19.83 | 35.19 | 18.69 | 411.8 | 528.9 | 528.5 | 619.7 |
| 6 | 1,000 | 85 E10 | FTP-2 (Bag3) | 2/5/2014 | 25.79 | 1640.0 | 21.67 | 36.56 | 21.34 | 400.2 | 525.2 | 521.8 | 605.0 |
| 6 | 1,000 | 85 E10 | LA92 | 2/5/2014 | 24.53 | 1663.4 | 23.26 | 38.27 | 17.48 | 453.6 | 582.1 | 616.9 | 699.8 |
| 6 | 1,000 | 85 E10 | USU6 (2nd) | 2/5/2014 | 48.33 | 2286.7 | 36.68 | 22 60 | 14.53 | 629.7 | 761.7 | 756.6 | 612.0 |
| 6 | 5,000 | 85 E10 | FTP-2 (Bag31 & 2) | 2/7/2014 | 25.60 | 1645.6 | 23.50 | 35.71 | 19.47 | 407.1 | 535.5 | 530.8 | 609.2 |
| 6 | 5,000 | 85 E10 | US06 (2nd) | 2/7/2014 | 48.10 | 2320.4 | 41.95 | 60.10 | 12.14 | 632.1 | 769.4 | 768.3 | 832.1 |
| 6 | 5,000 | 85 E10 | FTP-2 (Bags 1 & 2) | 2/10/2014 | 19.57 | 1575.9 | 21.20 | 34.39 | 18.71 | 408.9 | 526.8 | 525.4 | 615.8 |
| 6 | 5,000 | 85 E10 | FTP-2 (Bag3) | 2/10/2014 | 25.57 | 1660.2 | 23.33 | 35.76 | 20.10 | 405.5 | 532.4 | 520.2 | 606.7 |
| 6 | 5,000 | 85 E10 | LA92 | 2/10/2014 | 24.59 | 1667.5 | 26.61 | 37.92 | 15.41 | 461.2 | 592.5 | 637.5 | 709.9 |
| 6 | 5,000 | 85 E10 | USUb (2nd) FTP-1 (Bage 1 8. 2) | 2/10/2014 | 48.29 | 2351.1 1570 0 | 41.8/ | 58.0/ 33 51 | 13.85 17.87 | 627.1 | /63.5 | /61.2 | 835.6 |
| 6 | 5.000 | 87 E10 | FTP-1 (Bag 3) | 2/25/2014 | 25.64 | 1646 2 | 23.33 | 35.37 | 19.26 | | | | |
| 6 | 5,000 | 87 E10 | LA92 | 2/25/2014 | 24.89 | 1680.6 | 26.90 | 37.87 | 14.48 | 464.6 | 598.1 | 643.5 | 721.1 |
| 6 | 5,000 | 87 E10 | FTP-2 (Bags 1 & 2) | 2/26/2014 | 19.58 | 1572.2 | 21.17 | 34.04 | 17.05 | 410.3 | 528.4 | 522.4 | 611.3 |
| 6 | 5,000 | 87 E10 | FTP-2 (Bag3) | 2/26/2014 | 25.44 | 1642.7 | 23.71 | 35.12 | 18.92 | 406.4 | 535.2 | 525.4 | 612.8 |
| 6 | 5,000 | 87 E10 | LA92 | 2/26/2014 | 24.71 | 1677.6 | 26.38 | 37.73 | 14.70 | 462.3 | 596.4 | 632.9 | 712.5 |
| 6 | 5,000 | 87 E10 | USU6 (2nd) | 2/26/2014 | 48.18 | 2363.7 | 40.94 | 57.01 | 14.11 | 622.3 | 759.5 | /51.0 754 E | 834.0 |
| 6 | 1.000 | 87 F10 | FTP-3 (Bags 1 & 2) | 2/27/2014 | 40.52 19.61 | 2349.7 1577 6 | 19 76 | 35.54 | 18.96 | | | | 030.4 |
| 6 | 1,000 | 87 E10 | FTP-3 (Bag 3) | 2/27/2014 | 25.53 | 1667.5 | 21.81 | 36.28 | 20.61 | | | | |
| 6 | 1,000 | 87 E10 | LA92 | 2/27/2014 | 24.73 | 1677.1 | 23.78 | 38.75 | 15.58 | 457.9 | 589.5 | 618.0 | 707.9 |
| 6 | 1,000 | 87 E10 | FTP-5 (Bags 1 & 2) | 2/28/2014 | 19.68 | 1575.1 | 19.95 | 35.33 | 17.62 | 415.4 | 536.4 | 535.3 | 625.5 |
| 6 | 1,000 | 87 E10 | FTP-5 (Bag3) | 2/28/2014 | 25.61 | 1655.8 | 22.20 | 36.79 | 20.82 | 408.8 | 534.9 | 529.6 | 615.8 |
| 6 | 1,000 | 87 E10 | | 2/28/2014 | 24.69 | 1678.8 | 23.89 | 39.02 | 15.63 | 464.7 | 597.2 | 646.6 | 723.2 |
| 6 | 1,000 | 87 E10 | USUB (2nd) | 2/28/2014 | 48.31 <u>48.7</u> | 22/9.3 | 37.73 | 60.80 | 14.13 | 632.9 | 767.1 | 776.0 | 832.4 851 5 |
| | 1,000 | 0, 110 | 5500 (211u) | -1 -01 -014 | -10.17 | -201.I | 50.55 | 00.21 | 17.37 | 030.7 | 704.3 | 770.0 | 0.01.0 |

| | | Freed | Test Curls | Data | Vehicle | Engine | Throttle | 1 | Ignition | Exhaust Temp - | Catalyst Temp - | Exhaust Temp - | Catalyst Temp - |
|---------|----------|------------------|-----------------------------------|------------|-----------------|-----------------|----------|----------------|----------------|-------------------------|-----------------|----------------|------------------|
| vnumber | Altitude | Fuel | lest Cycle | Date | Speed | Speed | Position | Load | Timing | PreCat Avg. | MidCat Avg. | PreCat Max. | MidCat Max. |
| | | | | | (mph) | (rpm) | (%) | (%) | (deg BTDC) | (deg. C) | (deg. C) | (deg. C) | (deg. C) |
| 7 | 5,000 | 85 E10 | FTP-1 (Bags 1 & 2) | 1/29/2014 | 19.30 | 999.1 | 16.78 | 21.92 | 25.61 | 411.1 | 538.1 | 545.6 | 676.6 |
| 7 | 5,000 | 85 E10 | FTP-1 (Bag 3) | 1/29/2014 | 25.21 | 1114.6 | 17.34 | 22.80 | 25.98 | 422.6 | 559.2 | 539.3 | 681.9 |
| / 7 | 5,000 | 85 E10 | LA92 | 1/29/2014 | 24.87 | 1133.5 | 1/./2 | 23.55 | 25.29 | 484.1 | 634.9 | 644.1 | 770.9 |
| 7 | 5,000 | 85 E10 | USUB (2110) FTP-2 (Bags 1 & 2) | 1/29/2014 | 49.13 | 1/3/.3 000 3 | 16 73 | 21.97 | 27.57 | /12.8 | 740.7 5/0.9 | 724.7 550.4 | 677.4 |
| 7 | 5,000 | 85 E10 | FTP-2 (Bag3) | 1/30/2014 | 25.15 | 1104.3 | 17.38 | 22.76 | 25.92 | 421.5 | 561.6 | 555.3 | 675.8 |
| 7 | 5,000 | 85 E10 | LA92 | 1/30/2014 | 25.10 | 1135.7 | 17.76 | 23.67 | 25.16 | 484.0 | 634.9 | 641.6 | 768.7 |
| 7 | 5,000 | 85 E10 | US06 (2nd) | 1/30/2014 | 48.45 | 1717.3 | 22.72 | 31.65 | 27.42 | 607.9 | 749.1 | 734.0 | 866.3 |
| 7 | 1,000 | 85 E10 | FTP-1 (Bags 1 & 2) | 2/4/2014 | 19.34 | 997.6 | 16.29 | 22.51 | 25.26 | 420.4 | 545.4 | 564.8 | 678.8 |
| 7 | 1,000 | 85 E10 | FTP-1 (Bag 3) | 2/4/2014 | 25.20 | 1104.0 | 16.85 | 23.35 | 25.89 | 427.0 | 560.6 | 560.2 | 683.8 |
| 7 | 1,000 | 85 E10 | LA92 | 2/4/2014 | 24.91 | 1127.7 | 17.20 | 24.37 | 24.60 | 491.3 | 631.9 | 666.9 | 785.0 |
| 7 | 1,000 | 85 E10 | US06 (2nd) | 2/4/2014 | 48.81 | 1701.1 | 21.86 | 32.82 | 26.59 | 613.9 | 742.4 | 774.9 | 869.2 |
| 7 | 1,000 | 85 E10 | FTP-2 (Bags 1 & 2) | 2/5/2014 | 19.31 | 999.8 | 16.37 | 22.88 | 25.49 | 426.0 | 552.1 | 5/1.2 | 679.2 |
| 7 | 1,000 | 85 F10 | ΓΙΡ-2 (Bag5) ΙΔ92 | 2/5/2014 | 23.39 | 1110.8 | 17.13 | 23.40 | 23.60 | 429.4 479.4 | 619.6 | 545.4 647.8 | 778.6 |
| 7 | 1,000 | 85 E10 | US06 (2nd) | 2/5/2014 | 48.82 | 1701.2 | 21.54 | 32.69 | 26.83 | 614.6 | 744.5 | 780.9 | 859.6 |
| 7 | 1,000 | 85 E10 | FTP-3 (Bags 1 & 2) | 2/7/2014 | 19.26 | 995.5 | 16.31 | 22.77 | 25.45 | 419.7 | 542.0 | 561.9 | 679.5 |
| 7 | 1,000 | 85 E10 | FTP-3 (Bag3) | 2/7/2014 | 25.17 | 1101.5 | 16.86 | 18.82 | 25.95 | 424.6 | 554.2 | 554.6 | 671.5 |
| 7 | 5,000 | 87 E10 | FTP-1 (Bags 1 & 2) | 2/18/2014 | 19.29 | 1006.5 | 16.82 | 22.39 | 25.66 | 413.6 | 541.9 | 549.0 | 684.0 |
| 7 | 5,000 | 87 E10 | FTP-1 (Bag 3) | 2/18/2014 | 25.10 | 1112.6 | 17.37 | 22.80 | 26.71 | 420.3 | 558.2 | 541.8 | 681.9 |
| 7 | 5,000 | 87 E10 | LA92 | 2/18/2014 | 24.85 | 1139.3 | 17.70 | 23.56 | 25.62 | 482.8 | 633.8 | 640.3 | 769.8 |
| 7 | 5,000 | 87 E10 | US06 (2nd) | 2/18/2014 | 48.83 | 1740.8 | 22.33 | 31.53 | 27.88 | 608.8 | 748.4 | 731.9 | 862.4 |
| / | 5,000 | 87 E10 | FTP-2 (Bags 1 & 2) | 2/19/2014 | 19.30 | 1001.3 | 16.83 | 22.21 | 25.25 | 413.4 | 543.3 | 554.7 | 6//./ |
| 7 | 5,000 | 87 E10 | FTP-2 (Bag 3) | 2/19/2014 | 25.21 | 1104.9 | 17.39 | 22.69 | 26.07 | 420.3 | 558.Z | 548.4 | 6/3.6 762.0 |
| 7 | 5,000 | 87 E10 | LA92 | 2/19/2014 | 24.01 //8.8/ | 1732.2 | 22.45 | 23.50 | 23.21 | 611.8 | 751 1 | 730.3 | 863.6 |
| 7 | 1,000 | 87 F10 | FTP-1 (Bags 1 & 2) | 2/15/2014 | 19 30 | 994.9 | 16 34 | 22 74 | 27.32 | 418.4 | 543.3 | 560.4 | 685.6 |
| 7 | 1,000 | 87 E10 | FTP-1 (Bag 3) | 2/25/2014 | 25.16 | 1098.2 | 16.81 | 23.41 | 25.79 | 426.1 | 557.4 | 556.4 | 675.2 |
| 7 | 1,000 | 87 E10 | LA92 | 2/25/2014 | 24.85 | 1126.8 | 17.06 | 24.12 | 25.20 | 485.2 | 628.1 | 635.4 | 764.6 |
| 7 | 1,000 | 87 E10 | US06 (2nd) | 2/25/2014 | 48.93 | 1702.5 | 21.36 | 32.65 | 26.90 | 609.1 | 737.9 | 745.2 | 846.5 |
| 7 | 1,000 | 87 E10 | FTP-2 (Bags 1 & 2) | 2/27/2014 | 19.35 | 995.7 | 16.31 | 22.81 | 25.52 | 418.4 | 541.6 | 555.1 | 668.6 |
| 7 | 1,000 | 87 E10 | FTP-2 (Bag 3) | 2/27/2014 | 25.17 | 1103.3 | 16.87 | 23.06 | 25.89 | 424.0 | 552.7 | 544.7 | 671.6 |
| 7 | 1,000 | 87 E10 | LA92 | 2/27/2014 | 24.85 | 1125.3 | 17.16 | 24.20 | 25.10 | 478.7 | 616.9 | 635.4 | 767.5 |
| / | 1,000 | 87 E10 | US06 (2nd) | 2/2//2014 | 48.89 | 1/06.1 | 21.19 | 32.52 | 27.09 | 608.8 | /39.6 | /42.5 | 846.8 |
| 7 | 1,000 | 87 E10 | FTP-2 (Bags 1 & 2) | 2/28/2014 | 19.34 25.17 | 990.9 1105 9 | 16.27 | 22.07 | 25.30 | 415.1 | 553.0 | 507.0 | 666.0 |
| 8 | 1,000 | 87 E10 | FTP-4 (Bag3) | 12/13/2014 | 25.51 | 1297.2 | 17.15 | 34.26 | 22.29 | | | | |
| 8 | 1,000 | 85 E10 | US06 (2nd) | 1/10/2013 | 48.50 | 1909.1 | 23.96 | 45.83 | 15.73 | 711.1 | 857.1 | 901.5 | 975.0 |
| 8 | 5,000 | 87 E10 | FTP-1 (Bags 1 & 2) | 12/10/2013 | 19.64 | 1259.0 | 17.17 | 31.66 | 23.84 | 524.8 | 632.2 | 710.0 | 822.9 |
| 8 | 5,000 | 87 E10 | FTP-1 (Bag 3) | 12/10/2013 | 25.47 | 1319.8 | 17.88 | 32.15 | 22.52 | 532.6 | 656.5 | 705.5 | 817.2 |
| 8 | 5,000 | 87 E10 | LA92 | 12/10/2013 | 24.65 | 1358.5 | 18.58 | 32.85 | 21.00 | 560.0 | 694.6 | 797.2 | 924.1 |
| 8 | 5,000 | 87 E10 | US06 (2nd) | 12/10/2013 | 48.59 | 1959.3 | 25.28 | 41.74 | 19.10 | 676.6 | 824.1 | 854.7 | 935.4 |
| 8 | 5,000 | 87 E10 | FTP-2 (Bags 1 & 2) | 12/11/2013 | 19.64 | 1257.2 | 17.16 | 31.75 | 23.77 | 521.6 | 626.3 | 704.4 | 814.0 |
| 8 | 5,000 | 87 E10 | FTP-2 (Bag3) | 12/11/2013 | 25.40 | 1314.4 | 17.79 | 32.07 | 23.50 | 533.3 | 600.2 | 701.8 | 812.4 924.6 |
| 8 | 5,000 | 87 E10 | LA92 | 12/11/2013 | 24.03 48.53 | 1966.0 | 25.15 | 41 45 | 18 58 | 682.7 | 879.4 | 798.0 891.2 | 924.0 |
| 8 | 1,000 | 87 E10 | FTP-3 (Bags 1 & 2) | 12/12/2013 | 19.61 | 1240.4 | 16.58 | 33.88 | 23.41 | | | | |
| 8 | 1,000 | 87 E10 | FTP-3 (Bag 3) | 12/12/2013 | 25.48 | 1299.4 | 17.14 | 34.25 | 22.95 | 542.7 | 651.9 | 717.6 | 814.3 |
| 8 | 1,000 | 87 E10 | LA92 | 12/12/2013 | 24.68 | 1331.5 | 17.67 | 35.47 | 20.32 | 571.1 | 690.1 | 829.7 | 945.7 |
| 8 | 1,000 | 87 E10 | US06 (2nd) | 12/12/2013 | 48.45 | 1902.8 | 23.64 | 45.17 | 17.20 | 697.7 | 841.7 | 906.6 | 966.4 |
| 8 | 1,000 | 87 E10 | FTP-4 (Bags 1 & 2) | 12/13/2013 | 19.71 | 1254.3 | 16.59 | 33.95 | 23.74 | 535.8 | 632.0 | 707.4 | 810.3 |
| 8 | 1,000 | 87 E10 | LA92 | 12/13/2013 | 24.76 | 1329.7 | 17.70 | 35.49 | 20.18 | 571.6 | 693.8 | 831.9 | 947.0 |
| 8 | 1,000 | 8/E10 | US06 (2nd) | 12/13/2013 | 48.50 | 1917.7 | 23.44 | 45.12 | 18.04 | 522.2 | | | |
| 0 8 | 1,000 | 07 E10 87 F10 | FTP-5 (Bags 1 & 2) | 12/17/2013 | 25 52 | 1200.4 | 10.02 | 34.20 | 23.4U 22 Q/ | 532.3 5 <u>4</u> 1 8 | 651.6 | 701.8 | 810 G |
| 8 | 1.000 | 87 E10 | LA92 | 12/17/2013 | 24.74 | 1325.2 | 17.69 | 35.56 | 20.31 | 570.3 | 694.2 | 826.0 | 940.2 |
| 8 | 1,000 | 87 E10 | US06 (2nd) | 12/17/2013 | 48.51 | 1913.1 | 23.70 | 45.12 | 16.96 | 704.0 | 849.4 | 890.2 | 967.6 |
| 8 | 5,000 | 85 E10 | FTP-1 (Bags 1 & 2) | 12/19/2013 | 19.61 | 1260.6 | 17.22 | 31.55 | 24.07 | 522.5 | 629.3 | 700.3 | 815.1 |
| 8 | 5,000 | 85 E10 | FTP-1 (Bag 3) | 12/19/2013 | 25.43 | 1318.3 | 17.90 | 31.89 | 23.15 | 536.5 | 658.3 | 703.8 | 814.1 |
| 8 | 5,000 | 85 E10 | LA92 | 12/19/2013 | 24.64 | 1361.2 | 18.58 | 32.67 | 20.31 | 563.4 | 699.4 | 811.8 | 925.9 |
| 8 | 5,000 | 85 E10 | US06 (2nd) | 12/19/2013 | 48.51 | 1976.4 | 25.70 | 41.60 | 17.57 | 689.1 | 839.0 | 881.9 | 939.2 |
| 8 | 5,000 | 85 E10 | FTP-2 (Bags 1 & 2) | 1/3/2014 | 19.62 | 1264.4 | 17.20 | 32.02 | 24.27 | 523.4 | 631.8 | 702.6 | 820.7 |
| 8 | 5,000 | 85 E10 | FTP-2 (Bag3) | 1/3/2014 | 25.51 | 1319.4 | 1/.// | 32.20 | 23.35 | 534.4 | 655.3 | /01.0 | 813.7 |
| 0 8 | 5,000 | 63 E10 | US06(2nd) | 1/3/2014 | 24.0U 48.43 | 1978 3 | 25.61 | 32.88 41 96 | 20.54 | 504.3 688 0 | 703.5 R3R 1 | 881 2 | 933.2 939.9 |
| 8 | 5.000 | 85 E10 | FTP-1 (Bags 1 & 2) | 1/8/2014 | 19.56 | 1262 3 | 17.20 | 32.05 | 24.25 | 523.2 | 631.1 | 703.4 | 815.3 |
| 8 | 5,000 | 85 E10 | FTP-1 (Bag 3) | 1/8/2014 | 25.42 | 1315.5 | 17.83 | 32.05 | 22.07 | 531.0 | 655.7 | 717.6 | 827.2 |
| 8 | 5,000 | 85 E10 | LA92 | 1/8/2014 | 24.52 | 1350.5 | 18.47 | 32.80 | 20.67 | 559.7 | 693.2 | 820.6 | 929.1 |
| 8 | 5,000 | 85 E10 | FTP-2 (Bags 1 & 2) | 1/9/2014 | 19.55 | 1262.0 | 17.23 | 32.09 | 23.90 | 523.3 | 630.9 | 723.5 | 840.1 |
| 8 | 5,000 | 85 E10 | FTP-2 (Bag3) | 1/9/2014 | 25.35 | 1313.7 | 17.89 | 32.42 | 22.32 | 534.4 | 658.6 | 715.3 | 834.1 |
| 8 | 5,000 | 85 E10 | LA92 | 1/9/2014 | 24.51 | 1356.6 | 18.55 | 32.61 | 20.23 | 560.6 | 695.9 | 802.1 | 918.7 o 5 |
| 8 | 5,000 | 85 E10 | US06 (2nd) | 1/9/2014 | 48.44 | 1982.6 | 25.62 | 41.35 | 17.37 | 690.0 | 839.8 | 859.1 | 935.6 |
| 8 | 5,000 | 85 E10 | USU6 (2nd) | 1/9/2014 | 48.31 | 2014.6 | 26.15 | 41.99 | 16.65 | 696.6 | 849.4 | 8/1.4 | 938.5 |
| 0 2 | 1,000 | 85 F10 | FTP-1 (Rag 2) | 1/10/2014 | 25 // | 1241.3 | 17 15 | 34.00 | 23.30 22.08 | 52.4 541 A | 659.0 | 710.1 | 805.1 |
| 8 | 1,000 | 85 E10 | LA92 | 1/10/2014 | 24.62 | 1324.9 | 17.72 | 35.54 | 19.69 | 570.1 | 693.0 | 859.7 | 961.6 |

m. Vehicle Emissions Data – Response Drift Data (Tier 2 Emissions Test Fuel)

| VNumber | Altitude | Fuel | TestCycle 🗵 | TestID | TestDate | THC | CH4 | NonMethane | СО | Nox | CO2 | FE | NMOG |
|---------|----------------|--------|-------------|----------------|------------|----------|----------|------------|----------|----------|----------|---------|----------|
| | (ft) | | | | | (g/mile) | (g/mile) | (g/mile) | (g/mile) | (g/mile) | (g/mile) | (mpg) | (g/mile) |
| 1 | Site Elevation | Tier 2 | US FTP | MS34008520 | 8/28/2013 | 0.0288 | 0.0051 | 0.02407 | 0.2474 | 0.0121 | 237.5300 | 37.3996 | 0.0250 |
| 1 | Site Elevation | Tier 2 | US FTP | MS35004296 | 9/5/2013 | 0.0302 | 0.0045 | 0.02595 | 0.3012 | 0.0113 | 237.4640 | 37.4235 | 0.0270 |
| 1 | Site Elevation | Tier 2 | US FTP | MS35004355 | 10/5/2013 | 0.0333 | 0.0038 | 0.0297 | 0.2195 | 0.0114 | 239.2380 | 37.1650 | 0.0309 |
| 1 | Site Elevation | Tier 2 | US FTP | MS35004362 | 10/6/2013 | 0.0271 | 0.0041 | 0.0232 | 0.2118 | 0.0075 | 239.2620 | 37.1662 | 0.0242 |
| 2 | Site Elevation | Tier 2 | US FTP | MS34008749 | 10/22/2013 | 0.0099 | 0.0022 | 0.0081 | 0.3080 | 0.0008 | 285.4260 | 31.1533 | 0.0085 |
| 2 | Site Elevation | Tier 2 | US FTP | MS34008755 | 10/23/2013 | 0.0108 | 0.0023 | 0.0088 | 0.2942 | 0.0011 | 287.6000 | 30.9203 | 0.0092 |
| 2 | Site Elevation | Tier 2 | US FTP | MS34008761 | 10/24/2013 | 0.0137 | 0.0030 | 0.0109 | 0.3687 | 0.0014 | 286.5500 | 31.0197 | 0.0113 |
| 2 | Site Elevation | Tier 2 | US FTP | MS34008767 | 10/25/2013 | 0.0260 | 0.0042 | 0.0221 | 0.4157 | 0.0020 | 294.5060 | 30.1720 | 0.0230 |
| 2 | Site Elevation | Tier 2 | US FTP | MS34008788 | 10/29/2013 | 0.0221 | 0.0048 | 0.0176 | 0.3460 | 0.0026 | 289.0940 | 30.7483 | 0.0183 |
| 2 | Site Elevation | Tier 2 | US FTP | MS35004581 | 12/15/2013 | 0.0424 | 0.0054 | 0.0374 | 0.8782 | 0.0071 | 289.2470 | 30.6369 | 0.0389 |
| 2 | Site Elevation | Tier 2 | US FTP | MS34009057 | 12/18/2013 | 0.0109 | 0.0022 | 0.0091 | 0.1891 | 0.0014 | 286.4870 | 31.0581 | 0.0095 |
| 2 | Site Elevation | Tier 2 | US FTP | MS34009065 | 12/18/2013 | 0.0115 | 0.0026 | 0.0092 | 0.2200 | 0.0012 | 288.6490 | 30.8204 | 0.0095 |
| 3 | Site Elevation | Tier 2 | US FTP | MS34008748 | 10/22/2013 | 0.0185 | 0.0028 | 0.0162 | 0.1038 | 0.0105 | 288.0750 | 30.8988 | 0.0168 |
| 3 | Site Elevation | Tier 2 | US FTP | MS34008754 | 10/23/2013 | 0.0188 | 0.0034 | 0.0156 | 0.1268 | 0.0172 | 279.4540 | 31.8470 | 0.0163 |
| 3 | Site Elevation | Tier 2 | US FTP | MS34008760 | 10/24/2013 | 0.0189 | 0.0027 | 0.0164 | 0.1326 | 0.0130 | 282.2470 | 31.5311 | 0.0171 |
| 3 | Site Elevation | Tier 2 | US FTP | MS34008766 | 10/25/2013 | 0.0187 | 0.0027 | 0.0162 | 0.1007 | 0.0145 | 283.2170 | 31.4289 | 0.0168 |
| 3 | Site Elevation | Tier 2 | US FTP | MS34008787 | 10/29/2013 | 0.0184 | 0.0032 | 0.0154 | 0.0954 | 0.0134 | 283.9690 | 31.3468 | 0.0161 |
| 3 | Site Elevation | Tier 2 | US FTP | MS35004569 | 12/12/2013 | 0.0231 | 0.0030 | 0.0208 | 0.1246 | 0.0108 | 286.7010 | 31.0416 | 0.0216 |
| 3 | Site Elevation | Tier 2 | US FTP | MS35004580 | 12/15/2013 | 0.0182 | 0.0025 | 0.0159 | 0.0812 | 0.0148 | 283.6020 | 31.3898 | 0.0166 |
| 3 | Site Elevation | Tier 2 | US FTP | MS34009056 | 12/17/2013 | 0.0189 | 0.0028 | 0.0164 | 0.0940 | 0.0151 | 281.9670 | 31.5692 | 0.0170 |
| 4 | Site Elevation | Tier 2 | US FTP | 7230770 | 12/19/2013 | 0.0484 | 0.0053 | 0.0430 | 0.5265 | 0.0051 | 349.8270 | 25.2852 | 0.0447 |
| 4 | Site Elevation | Tier 2 | US FTP | 7230781 | 12/20/2013 | 0.0489 | 0.0048 | 0.0441 | 0.4543 | 0.0076 | 351.4745 | 25.1750 | 0.0459 |
| 4 | Site Elevation | Tier 2 | US FTP | 8343813 | 2/13/2014 | 0.0392 | 0.0047 | 0.0345 | 0.4367 | 0.0041 | 357.6537 | 24.7447 | 0.0359 |
| 4 | Site Elevation | Tier 2 | US FTP | 8343875 | 2/18/2014 | 0.0214 | 0.0037 | 0.0178 | 0.3055 | 0.0029 | 354.8835 | 24.9567 | 0.0185 |
| 5 | Site Elevation | Tier 2 | US FTP | 4843735 | 10/16/2013 | 0.0225 | 0.0066 | 0.0163 | 0.3106 | 0.0072 | 500.6258 | 17.7673 | 0.0170 |
| 5 | Site Elevation | Tier 2 | US FTP | 3239554 | 10/23/2013 | 0.0243 | 0.0064 | 0.0178 | 0.3509 | 0.0080 | 498.9165 | 17.8260 | 0.0185 |
| 6 | Site Elevation | Tier 2 | US FTP | 782012130047-3 | 9/12/2013 | 0.0365 | 0.0043 | 0.0327 | 0.5369 | 0.0368 | 273.3000 | 32.4272 | 0.0340 |
| 6 | Site Elevation | Tier 2 | US FTP | 782012130047-4 | 9/13/2013 | 0.0376 | 0.0042 | 0.0339 | 0.5599 | 0.0380 | 276.4000 | 32.0716 | 0.0352 |
| 6 | Site Elevation | Tier 2 | US FTP | 782012140016-4 | 3/6/2014 | 0.0356 | 0.0045 | 0.0314 | 0.5307 | 0.0357 | 262.6000 | 33.6424 | 0.0327 |
| 6 | Site Elevation | Tier 2 | US FTP | 782012140016-5 | 3/7/2014 | 0.0406 | 0.0052 | 0.0360 | 0.6896 | 0.0388 | 285.3000 | 31.0250 | 0.0374 |
| 7 | Site Elevation | Tier 2 | US FTP | MS34009141 | 1/16/2014 | 0.0639 | 0.0223 | 0.0431 | 1.2326 | 0.0186 | 517.9910 | 17.0237 | 0.0448 |
| 7 | Site Elevation | Tier 2 | US FTP | MS34009167 | 1/23/2014 | 0.0765 | 0.0233 | 0.0548 | 1.2920 | 0.0188 | 525.2120 | 16.7863 | 0.0570 |
| 7 | Site Elevation | Tier 2 | US FTP | MS34009468 | 3/5/2014 | 0.0477 | 0.0172 | 0.0317 | 0.8203 | 0.0118 | 518.7340 | 17.0222 | 0.0329 |
| 7 | Site Elevation | Tier 2 | US FTP | MS34009480 | 3/5/2014 | 0.0618 | 0.0194 | 0.0439 | 1.0676 | 0.0123 | 524.0750 | 16.8353 | 0.0456 |
| 7 | Site Elevation | Tier 2 | US FTP | MS34009495 | 3/7/2014 | 0.0557 | 0.0200 | 0.0370 | 0.9562 | 0.0155 | 520.7020 | 16.9503 | 0.0385 |
| 8 | Site Elevation | Tier 2 | US FTP | 782012130032-5 | 9/12/2013 | 0.0150 | 0.0030 | 0.0128 | 0.1908 | 0.0192 | 454.4000 | 19.5530 | 0.0133 |
| 8 | Site Elevation | Tier 2 | US FTP | 782012130032-6 | 9/13/2013 | 0.0145 | 0.0017 | 0.0130 | 0.1995 | 0.0161 | 454.9000 | 19.5094 | 0.0135 |
| 8 | Site Elevation | Tier 2 | US FTP | 782012140008-2 | 1/30/2014 | 0.0158 | 0.0034 | 0.0134 | 0.1817 | 0.0161 | 456.8000 | 19.4288 | 0.0139 |
| 9 | Site Elevation | Tier 2 | US FTP | MS34009289 | 2/12/2014 | 0.1386 | 0.0676 | 0.0755 | 1.4995 | 0.0074 | 420.5780 | 20.9142 | 0.0785 |
| 9 | Site Elevation | Tier 2 | US FTP | MS34009341 | 2/18/2014 | 0.1494 | 0.0708 | 0.0832 | 1.5224 | 0.0064 | 423.2250 | 20.7809 | 0.0865 |
| 9 | Site Elevation | Tier 2 | US FTP | MS35004934 | 5/7/2014 | 0.1786 | 0.0820 | 0.1014 | 1.5956 | 0.0082 | 425.4140 | 20.7415 | 0.1055 |
| 9 | Site Elevation | Tier 2 | US FTP | MS35004963 | 5/12/2014 | 0.1552 | 0.0724 | 0.0870 | 1.4761 | 0.0062 | 421.8280 | 20.9295 | 0.0905 |

| Vnumber | Altitude | Fuel | Test | Date | Vehicle Speed | Engine Speed | Throttle Position | Load | lgnition Timing | Exhaust Temp - PreCat Avg. | Catalyst Temp - MidCat Avg. | Exhaust Temp - PreCat Max. | Catalyst Temp - MidCat Max. |
|---------|----------|--------|-------------------------------------|------------|------------------|-----------------|----------------------|-------|--------------------|-------------------------------|--------------------------------|-------------------------------|--------------------------------|
| | | | | | (mph) | (rpm) | (%) | (%) | (deg BTDC) | (deg. C) | (deg. C) | (deg. C) | (deg. C) |
| 1 | Site | Tier 2 | FTP-3 (Bags 1 & 2) | 8/28/2013 | 19.54 | 1317.4 | 16.49 | 26.88 | 20.29 | 452.6 | 565.2 | 666.5 | 719.1 |
| 1 | Site | Tier 2 | FTP-3 (Bag 3) | 8/28/2013 | 25.41 | 1390.5 | 17.32 | 29.05 | 18.98 | 468.4 | 587.6 | 666.1 | 734.3 |
| 1 | Site | Tier 2 | FTP-4 (BagS 1 & 2) | 9/5/2013 | 25.47 | 1308.2 | 17.26 | 20.82 | 19.62 | 455.5 | 582.3 | 664.2 | 721.1 |
| 1 | Site | Tier 2 | FTP-1 (Bags 1 & 2) | 10/5/2013 | 19.56 | 1323.8 | 16.51 | 27.00 | 20.45 | 456.4 | 566.1 | 674.4 | 751.6 |
| 1 | Site | Tier 2 | FTP-1 (Bag 3) | 10/5/2013 | 25.38 | 1384.1 | 17.34 | 29.21 | 19.43 | 466.8 | 583.6 | 651.8 | 722.1 |
| 1 | Site | Tier 2 | FTP-2 (Bag3) | 10/6/2013 | 25.36 | 1378.7 | 17.38 | 29.17 | 19.69 | | | | |
| 2 | Site | Tier 2 | FTP-1 (Bags 1 & 2) | 10/22/2013 | 19.28 | 1249.1 | 15.84 | 25.70 | 26.96 | 477.6 | 579.6 | 610.7 | 691.9 |
| 2 | Site | Tier 2 | FTP-2 (Bags 1 & 2) | 10/23/2013 | 19.27 | 1248.4 | 15.81 | 25.61 | 27.00 | 476.8 | 577.2 | 613.5 | 696.4 |
| 2 | Site | Tier 2 | FTP-2 (Bag3) | 10/23/2013 | 24.96 | 1354.7 | 16.35 | 26.54 | 27.55 | 488.7 | 589.7 | 636.3 | /18./ |
| 2 | Site | Tier 2 | FTP-1 (Bag 3) | 10/24/2013 | 25.06 | 1365.9 | 15.65 | 25.75 | 20.95 | 476.0 | 591 7 | 653.2 | 726.9 |
| 2 | Site | Tier 2 | FTP-3 (Bag 3) | 10/24/2013 | 25.12 | 1362.1 | 16.38 | 26.54 | 27.81 | 488.0 | 589.9 | 629.7 | 712.5 |
| 2 | Site | Tier 2 | FTP-4 (Bags 1 & 2) | 10/25/2013 | 19.58 | 1241.4 | 15.91 | 26.69 | 27.64 | 480.9 | 583.8 | 623.3 | 704.0 |
| 2 | Site | Tier 2 | FTP-4 (Bag3) | 10/25/2013 | 25.04 | 1363.2 | 16.46 | 27.16 | 27.77 | 490.2 | 591.7 | 635.8 | 701.5 |
| 2 | Site | Tier 2 | FTP-5 (Bags 1 & 2) | 10/29/2013 | 19.29 | 1247.1 | 15.79 | 25.89 | 26.98 | 478.1 | 578.7 | 615.3 | 695.9 |
| 2 | Site | Tier 2 | FTP-4 (Bag3) | 10/29/2013 | 25.00 | 1361.5 | 16.33 | 26.65 | 27.68 | 490.9 | 592.1 | 638.8 | 713.0 |
| 2 | Site | Tior 2 | FTP-2 (Bags 1 & 2) | 12/15/2013 | 19.28 | 1253.3 | 15.91 | 27.14 | 26.67 | 4/8.5 | 579.1 | 616.4 | 586.7 |
| 2 | Site | Tier 2 | FTP-3 (Bags 1 & 2) | 12/13/2013 | 19 33 | 1246.6 | 15.45 | 26.84 | 28.01 | 432.2 | 579.8 | 611 7 | 692.1 |
| 2 | Site | Tier 2 | FTP-4 (Bags 1 & 2) | 12/18/2013 | 19.32 | 1249.9 | 15.86 | 25.89 | 27.15 | 477.2 | 578.9 | 608.4 | 687.7 |
| 2 | Site | Tier 2 | FTP-3 (Bag 3) | 12/18/2013 | 25.08 | 1363.8 | 16.43 | 26.84 | 27.57 | 492.1 | 593.2 | 627.0 | 707.8 |
| 2 | Site | Tier 2 | FTP-4 (Bag 3) | 12/18/2013 | 25.12 | 1367.4 | 16.40 | 26.70 | 27.85 | 491.4 | 592.6 | 621.1 | 707.9 |
| 3 | Site | Tier 2 | FTP-2 (Bags 1 & 2) | 10/23/2013 | 19.81 | 1274.7 | 17.89 | 25.80 | 24.13 | | | | |
| 3 | Site | Tier 2 | FTP-2 (Bag3) | 10/23/2013 | 25.47 | 1391.9 | 18.74 | 28.63 | 24.66 | 486.7 | 596.0 | 639.6 | 710.7 |
| 3 | Site | Tier 2 | FTP-3 (Bags 1 & 2) | 10/24/2013 | 19.78 | 1277.7 | 18.13 | 27.64 | 23.77 | 481.2 | 584.4 | 657.4 | 729.9 |
| 3 | Site | Tier 2 | FTP-3 (Bag 3) FTP-4 (Bags 1 & 2) | 10/24/2013 | 25.41 | 1381.9 | 18.00 | 28.57 | 24.49 | 487.9 | 596.6 | 667.2 | 708.7 |
| 3 | Site | Tier 2 | FTP-4 (Bag3) | 10/25/2013 | 25.54 | 1386.3 | 18.67 | 27.40 | 23.05 | 401.1 | | | |
| 3 | Site | Tier 2 | FTP-5 (Bags 1 & 2) | 10/29/2013 | 19.66 | 1271.3 | 18.04 | 27.51 | 23.52 | 479.9 | 582.6 | 664.4 | 737.3 |
| 3 | Site | Tier 2 | FTP-5 (Bag3) | 10/29/2013 | 25.38 | 1388.2 | 18.64 | 28.46 | 24.43 | 486.7 | 594.7 | 634.8 | 708.9 |
| 3 | Site | Tier 2 | FTP-1 (Bags 1 & 2) | 12/12/2013 | 19.81 | 1272.6 | 18.17 | 27.55 | 23.55 | 480.4 | 581.5 | 655.6 | 726.5 |
| 3 | Site | Tier 2 | FTP-1 (Bag 3) | 12/12/2013 | 25.48 | 1387.9 | 18.81 | 28.73 | 24.37 | 487.7 | 594.3 | 630.3 | 701.6 |
| 3 | Site | Tier 2 | FTP-2 (Bags 1 & 2) | 12/15/2013 | 19.93 | 1281.3 | 18.17 | 27.42 | 23.84 | 479.6 | 580.3 | 653.9 | 730.2 |
| 3 | Site | Tier 2 | FTP-2 (Bag3) | 12/15/2013 | 25.64 | 1392.7 | 18.79 | 28.88 | 24.35 | 485.9 | 594.1 | 631.8 | 707.2 |
| 3 | Site | Tier 2 | FTP-3 (Bags 1 & 2) | 12/17/2013 | 25.07 | 1276.3 | 18.13 | 27.34 | 23.86 | 480.1 | 582.0 | 630.5 | 728.7 |
| 4 | Site | Tier 2 | FTP-3 (Bags 1 & 2) | 2/12/2014 | 19.94 | 1347.7 | 16.21 | 30.96 | 27.20 | 492.6 | 581.6 | 655.4 | 731.8 |
| 4 | Site | Tier 2 | FTP-3 (Bag 3) | 2/12/2014 | 26.89 | 1515.4 | 17.48 | 31.70 | 28.84 | 515.2 | 608.8 | 682.4 | 727.1 |
| 4 | Site | Tier 2 | FTP-4 (Bags 1 & 2) | 2/13/2014 | 19.99 | 1336.3 | 16.35 | 31.25 | 26.95 | 492.7 | 582.4 | 668.6 | 722.1 |
| 4 | Site | Tier 2 | FTP-4 (Bag3) | 2/13/2014 | 26.77 | 1506.3 | 17.38 | 31.49 | 28.57 | 512.1 | 606.4 | 684.7 | 734.3 |
| 5 | Site | Tier 2 | FTP-3 (Bags 1 & 2) | 10/23/2013 | 19.94 | 1164.4 | 16.00 | 28.44 | 22.53 | | | | |
| 5 | Site | Tier 2 | FTP-3 (Bag 3) | 2/18/2014 | 29.72 | 1225.1 | 16.14 | 27.01 | 21.27 | 402.2 | 525.2 | | |
| 5 | Site | Tier 2 | FTP-4 (Bag3 1 & 2) | 2/18/2014 | 26.70 | 1199.6 | 15.82 | 30.06 | 22.78 | 403.3 | 531.0 | 513.9 | 623.9 |
| 6 | Site | Tier 2 | FTP-1 (Bags 1 & 2) | 9/12/2013 | 19.59 | 1558.3 | 20.06 | 35.58 | 17.69 | 424.5 | 552.0 | 551.6 | 642.4 |
| 6 | Site | Tier 2 | FTP-1 (Bag 3) | 9/12/2013 | 25.68 | 1630.5 | 22.51 | 37.07 | 18.34 | 418.6 | 556.3 | 544.3 | 638.5 |
| 6 | Site | Tier 2 | FTP-2 (Bags 1 & 2) | 9/13/2013 | 19.51 | 1553.6 | 20.18 | 35.57 | 18.07 | 422.9 | 547.5 | 550.1 | 641.0 |
| 6 | Site | Tier 2 | FTP-2 (Bag3) | 9/13/2013 | 25.74 | 1630.2 | 21.92 | 37.35 | 18.95 | 417.7 | 552.1 | 541.9 | 642.0 |
| 6 | Site | Tier 2 | FTP-1 (Bags 1 & 2) | 3/6/2014 | 19.55 | 1579.8 | 19.57 | 34.41 | 18.45 | 411.4 | 534.5 | 529.9 | 617.9 |
| 6 | Site | Tier 2 | FIP-1 (Bag 3) | 3/6/2014 | 25.63 | 1649.9 | 21.04 | 36.44 | 20.19 | 407.3 | 534.3 | 527.5 | 615.2 |
| 6 | Site | Tier 2 | FTP-2 (Bag3 1 & 2) | 3/8/2014 | 25.48 | 1627 3 | 20.37 | 38.23 | 17.44 | | | | |
| 7 | Site | Tier 2 | FTP-1 (Bags 1 & 2) | 1/16/2014 | 19.36 | 994.2 | 16.28 | 22.42 | 25.07 | 423.8 | 544.2 | 563.3 | 661.4 |
| 7 | Site | Tier 2 | FTP-1 (Bag 3) | 1/16/2014 | 25.26 | 1109.1 | 16.89 | 23.33 | 25.84 | 432.4 | 559.2 | 548.3 | 678.3 |
| 7 | Site | Tier 2 | LA92 | 1/16/2014 | 24.85 | 1125.2 | 17.20 | 24.08 | 25.01 | 494.0 | 632.5 | 639.0 | 766.5 |
| 7 | Site | Tier 2 | US06 (2nd) | 1/16/2014 | 49.32 | 1717.1 | 20.85 | 32.33 | 27.85 | 611.5 | 740.6 | 718.2 | 834.7 |
| 7 | Site | Tier 2 | FTP-2 (Bags 1 & 2) | 1/23/2014 | 19.39 | 998.1 | 16.37 | 22.76 | 25.33 | 423.7 | 546.1 | 575.0 | 680.6 |
| / | Site | Tier 2 | FTP-2 (Bag3) | 1/23/2014 | 25.21 | 1109.2 | 16.91 | 23.11 | 25.83 | 429.6 | 556.9 | 549.2 | 6/9.8 |
| 7 | Site | Tier 2 | LA92 LIS06 (2nd) | 1/23/2014 | 24.95 48.90 | 1710.6 | 20.81 | 24.04 | 25.00 | 490.2 | 739 5 | 723 5 | 838 5 |
| 7 | Site | Tier 2 | FTP-1 (Bags 1 & 2) | 3/5/2014 | 19.28 | 994.3 | 16.29 | 22.53 | 25.50 | 419.6 | 543.6 | 557.0 | 668.6 |
| 7 | Site | Tier 2 | FTP-2 (Bags 1 & 2) | 3/5/2014 | 19.31 | 995.9 | 16.30 | 22.50 | 25.48 | 421.2 | 543.6 | 549.7 | 670.0 |
| 7 | Site | Tier 2 | FTP-1 (Bag 3) | 3/5/2014 | 25.19 | 1103.5 | 16.89 | 23.06 | 26.22 | 426.4 | 558.3 | 540.4 | 671.9 |
| 7 | Site | Tier 2 | FTP-2 (Bag3) | 3/5/2014 | 25.17 | 1105.6 | 16.88 | 23.22 | 26.00 | 425.7 | 555.1 | 540.3 | 670.6 |
| 7 | Site | Tier 2 | FTP-3 (Bags 1 & 2) | 3/7/2014 | 19.31 | 996.5 | 16.31 | 22.68 | 25.60 | 420.7 | 544.5 | 553.8 | 663.2 |
| 8 | Site | Tier 2 | FTP-1 (Bags 1 & 2) | 9/12/2013 | 19.68 | 1252.8 | 16.85 | 34.20 | 22.56 | | | | |
| 8 | Site | Tior 2 | FIP-1 (Bag 3) | 9/12/2013 | 25.26 | 1302.7 | 17.37 | 34.53 | 22.39 | | | | |
| ð Q | Site | Tier 2 | FTP-2 (Bags 1 & 2) | 9/13/2013 | 25 22 | 1302.6 | 17 27 | 34.21 | 22.90 | | | | |
| 8 | Site | Tier 2 | FTP-2 (Bags 1 & 2) | 1/30/2014 | 19.56 | 1251.1 | 16.69 | 34.49 | 22.44 | 540.7 | 646.0 | 703.8 | 808.6 |
| 8 | Site | Tier 2 | FTP-2 (Bag3) | 1/30/2014 | 25.34 | 1312.9 | 17.25 | 34.75 | 20.80 | 546.1 | 667.2 | 720.5 | 822.6 |
| 8 | Site | Tier 2 | FTP-2 (Bags 1 & 2) | 1/31/2014 | 19.55 | 1249.4 | 16.66 | 33.95 | 22.61 | | | | |
| 8 | Site | Tier 2 | FTP-2 (Bag3) | 1/31/2014 | 25.09 | 1297.5 | 17.15 | 34.20 | 21.44 | 542.2 | 659.9 | 707.4 | 659.9 |

n. Vehicle Performance Data – Response Drift Data (Tier 2 Emissions Test Fuel)